Mechanical behaviour of polymeric foam core at various orientation angles

M.R.M.Rejab¹, M.S.M.Sani¹, M.M.Noor¹,K.Kadirgama¹, M.M.Rahman¹, & A.Alias²

¹Universiti Malaysia Pahang, 26300 Kuantan, Pahang, Malaysia. ²Universiti Teknologi Malaysia, 81310 Skudai, Johor, Malaysia.

Abstract

Polymeric foam is widely used as core materials in various applications such as cushioning, padding, insulating, structural use and buoyancy. This is because of its ability to provide high bending stiffness tied with lightweight in composite sandwich construction. The purpose of this paper is to present the behaviour of polyurethane (PU) foam, which is fabricated in various orientation angles. There were five different orientation angles have been studied i.e. 0°, 30°, 45°, 60° and 90°. Three mechanical tests were performed under tension, compression and shear loads to investigate the polyurethane foam behaviour. Electron microscope was used to capture the microstructure of the specimens before and after the tests. Comparisons have been made between different orientation angles in fracture modes and mechanical properties. Deformation and failure occur during foam crushing are discussed according to experimental evidence. Since the main application of foam materials are for energy absorption, foam response under considerable compression has been studied intensively. At angle of 90°, it permits more localised failure with high energy absorption and in contrary, 0° which posses the lowest of energy absorption. Energy absorption for PU foam material tends to increase when the orientation of angle is increased.

Keywords: polyurethane foam, cell orientation angles, fracture mode

1 Introduction

Foam materials have a cellular structure with a three dimensional array of cells and they are being used increasingly in engineering. Their microscopic cellular structure determines their superior performance as an energy absorbing materials and as a core material in sandwich panels. However, their mechanical behaviours are complex due to their cellular structure. More materials tests are required to determine their mechanical properties for structural design and numerical simulation purposes. Currently, the standard tests on mechanical properties of foam core materials include uniaxial tension test (ASTM C297), uniaxial compressive (ASTM D365) and shear (ASTM C273) tests.

In order to understand the mechanical behaviours of foam materials in the general loading case, experimental and theoretical studies have been conducted for a variety of loading paths. Yield and failure surface of various foams have been presented based on experimental results and constitutive models [1,2,3]. Microscopic mechanics of cellular materials has been introduced by Ashby and Gibson (1997) to relate microscopic behaviour to cell-wall properties and geometric constructions of the foam [4]. The most common foam materials used in all applications except aerospace are polyurethane, polystyrenes, polyvinyl chlorides and polyphenolics, which are in group of expanded polymeric foams. Recently, rigid polyurethane foam is becoming famous foam core materials because of it's meritoriously properties [5,6]. This rigid polyurethane foam is used as sample for this research.

The aims of this study are to obtain the effect of foam properties in various orientations and its behaviour in the energy absorption point of view. The reliable techniques of manufacturing this foam core were used and the experimental data have been analysed to determine their mechanical properties for structural design and numerical simulation purposes

2 Material Preparation

In this study, rigid polyurethane (PUR) foam was used as the specimen. Two chemical components are used to fabricate the foam. Component A is called polyol blend (RF 0597/3A) and component B is called isocyanate (RF0597/3B). The chemicals were supplied by Asia Polyurethane Manufacturing (APM), Singapore. The foam was manufactured to get slab stock foam by using injection foaming process in special *in-situ* mould [7]. The PUR chemicals used were based on ratio 50% of component A and component B, respectively. This ratio was chosen because of the ratio gave uniform and consistency microstructure for this structural foam. The samples were prepared from slab stock foam into cubes with dimensions of 25mm x 25mm x 25mm as shown in Figure 1. The foam weight was determined by using electronic weighting scale. The density of foam, ρ was measured according to standard ASTM D1622-98.



Figure 1: Specimen dimension and measuring of foam weight.

Sample (°)	Weight (g)	Height (mm)	Length (mm)	Width (mm)	Volume $(mm^3) \times 10^3$	Density, $p (kg/m^3)$
0	1.0056	25.09	24.91	25.11	15.69	64.07
30	1.0094	25.04	25.12	25.04	15.75	64.09
45	1.0135	25.13	25.10	25.12	15.84	63.96
60	1.0084	25.14	25.05	25.09	15.80	63.82
90	1.0117	25.06	25.11	25.07	15.78	64.13
					Ave:	64.01

Table 1 shows the density of PUR was measured. Based on the table, the average apparent density of the PUR foam was 64.01 ± 0.2 kg/m³.

Table 1: Density of PUR foam was measured.

3 Experimental work

In this study, three types of tests have been considered and experimental tests were accomplished to collect the appropriate data for this PUR foam.

3.1 Compression Test

Compression test was conducted in an INSTRON 100kN series 4206 testing machine according to standards ASTM D1621-1987. The specimens were 25mm thick, and other dimensions were same, 25mm by 25mm. As shown in Figure 2, the specimen was placed between the platens of the machine and was deformed at a quasi-static loading rate 1mm per minute, which gives an engineering strain rate of $6.7 \times 10^{-4} s^{-1}$.



Figure 2: Compression test setup.

3.2 Tension test

The foam tension test was conducted on an INSTRON 100kN series 4206 testing machine to the relevant standard ASTM C297-1961. The specimens were 25mm thick and the other dimensions were 25mm by 25mm. The blocks of the foam were bonded to aluminium blocks using Araldite glue. The curing time was 3 hours at 40°C. The testing rig is designed to allow for both forward and lateral

deflections which eliminate bending effect (Figure 3). The stiffness of the testing machine was compensated for by replacing the foam with an aluminium block. The crosshead speed was 1mm per minute, which gives an engineering strain rate of $6.7 \times 10^{-4} \text{ s}^{-1}$.



Figure 3: Tension test setup.

3.3 Shear test

The foam shear test is defined in ASTM standard C273-1961. There are two versions of the test, namely tensile and compression loading. The compression version was used. The specimen geometry was 25mm thick with the other dimensions being 240mm by 50mm. It was then tested on the INSTRON 100kN series 4206 testing machine.



Figure 4: Shear test setup.

The load line should act through the opposite corners of the foam specimen. The foam was bonded to the platens using Araldite glue (Figure 4). The bonding between rigid and the foam was important because if not failure would occur at the bonding of the foam and the platen. If this occurs so the shear data was not accurately.

4 **Results and Discussions**

In this study, three type of tests have been considered and experimental tests were accomplished to collect the appropriate data for this PUR foam.



5 different orientation angles.

Figure 5 shows the compression test of foam that have been done to ascertain the mechanical behaviours. This is to determine the energy absorption and maximum compression strength for every sample. Based on the graph, the PUR 90 degree sample gives the largest value of core compression modulus which is 1.65 MPa, where as the maximum compression stress is 0.159 MPa with 0.09 of strain. The lowest core compression modulus is 0.627 MPa that is for the orientation of 0 degree with maximum compression stress value at 0.10 MPa. Other samples including 30, 45 and 60 degrees indicates core compressive strength of 0.068 MPa, 0.074 MPa and 0.125 MPa with the amount of strain valued at 0.099, 0.93 and 0.98, respectively.



Figure 6: Compression yield stress at various orientation angles

Figure 6 shows the compression yield stress of PUR foam in various orientations. From the figure, it is clearly shown that the value of compression yield stress increases with the increase of PUR foam angle in polynomial relation. Minor increment occurred in the range of 0 degree and 45 degree. The increment of yield stress value is about 0.06 MPa or about 9%.

A sudden rise is noticed in values of the yield stress. This occurred between the range of 45 degree and 60 degree. The value increased by 0.051 MPa or 68%. The highest and lowest value of yield stress is about 0.159 MPa and 0.062 MPa

which happened for 90 degree and 0 degree respectively. The eqn (1) is derived in the graph as shown below:

$$\sigma_{cy} = 1^{-05} \theta^2 + 6^{-05} \theta + 0.0591 \text{ (MPa)}, 0^\circ < \theta < 90^\circ$$
(1)



Figure 7: Tension stress-strain curves for 5 different orientation angles.

Figure 7 shows the tensile test of foam that has been done to ascertain the mechanical behaviours. This is to determine the maximum tension strength for every sample. Based from above figure, the PUR 90 degree sample gives the largest value of core tensile modulus which is 3.53 MPa. Whereas the maximum tension stress resulted of 0.323 MPa with 0.09 of strain. The lowest core tension modulus is 0.567 MPa that is for the orientation of 30 degree. Other samples including 0, 45 and 60 degrees indicates core compressive strength of 0.15 MPa, 0.176 MPa and 0.202 MPa with the amount of strain valued at 0.21, 0.22 and 0.17, respectively.



Figure 8: Tension yield stress at various orientation angles

Figure 8 shows the tension yield stress of PUR foam in various orientations. It shows that the value of tension yield stress PUR foam increases with the increase

of PUR foam angle. The graph is a polynomial type of graph. From the lowest angle, the yield stress increase up to 0.323 MPa to fail at the highest angle of PUR foam specimen (90 degree). The graph shows a uniform increment in the angle range of 0 degree and 60 degree with 14% of increment. The value of yield stress increased rapidly in the angle range of 60 degree and 90 degree. The increase of yield stress value is 0.121 MPa or in a percentage is 60% before failing. While the difference between highest and lowest value is 0.188 MPa for 90 degree and 0 degree. The eqn (2) is derived from the graph as shown below:

$$\sigma_{t} = 3^{-05} \theta^2 - 0.0005 \theta + 0.1363 \text{ (MPa)}, \ 0^\circ < \theta < 90^\circ \tag{2}$$



Figure 9 shows the shear test of foam which has been done to ascertain the mechanical foam behaviours which widely used as a core for the sandwich structure. These mechanical behaviours should be known to determine the maximum shear strength for each sample. Based on the above graph, the PUR 90 degree sample gives the largest value of core shear modulus that is 1.32 MPa. This is because most of the direction force that has been loaded is absorbed by the 90 degree cell of structure foam. The maximum shear is 0.123 MPa with 0.031 of strain. Whereas the lowest cores shear modulus is 0.95 MPa occurred during the orientation of 0 degree. This is because of the forces applied could not be bear by the cell structure. Whereas the cores shear modulus for the sample 30, 45 and 60 degrees are 1.07 MPa, 1.16 MPa and 1.98 MPa accordingly with the core shear strength of 0.110 MPa, 0.114 MPa and 0.121 MPa, respectively.

Figure 10 shows the shear yield stress of PUR foam in various orientations. It shows that the value of shear yield stress increases with the increase of PUR foam angle in a linear relation. From the lowest angle, the yield stress increase up to 0.106 MPa before failure occurred at the highest angle of PUR foam specimen with 0.123 MPa.

The value of yield stress increased rapidly in the angle range of 45 degree and 60 degree. The increase of yield stress value is 0.007 MPa or in a percentage is 6% before failing. While the difference between highest and lowest value is



0.017 MPa for 90 degree and 0 degree. The eqn (3) is derived from the graph as shown below:

Figure 10: Shear yield stress at various orientation angles

angle (Ø)

The PUR foam that has undergone by compression test had been analysed using Stereo Microscope with magnification 10X and 20X. The microstructures of closed cell of PUR are shown as in Figure 11. Microscopic structure of sample was taken using by Stereo Microscope with calibration 0.31646 μ m/Pixel (magnification 20X).





Figure 11: Shear yield stress at various orientation angles

Figure 11 shows that the plateau range of crushable foam in compression, caused by cell-wall collapse. The cell-wall for all samples were collapse in compression could be one of cell-wall buckling, cell wall breaking and the formation of foam hinges in the cell wall, or their combinations. From the microstructure analysis, the characteristic cell-wall size and cell wall thickness is decrease. The average of the cell-wall size was move between 10 μ m and 15 μ m and the cell-wall thickness still between 1 μ m to 10 μ m. It also shows that the crash of diameter of the cell respectively is equal.

5 Conclusion

In conclusion, the purpose of this project is to study the effect of orientation of the fabrication of foam core under several mechanical tests such as compression, tension and shear tests. In this study, several mechanical behaviour of PUR foam which relate to orientation have been determined. From the analyses that have been done to the foam structure, it can be concluded that the PU foam is good in bearing the compression load and also has a good absorbing value. PUR foam under compression test has been studied intensively to determine the energy absorption for each type of conditions. For 90 degree, it permits more localised failure with high energy absorption, unlike 0 degree which posses the lowest of energy absorption. Energy absorption for PUR foam material tends to increase when the orientation of angle is increased. Therefore, the higher foam angle orientation gives higher stiffness and energy absorption.

Acknowledgement

The financial support by Universiti Malaysia Pahang is grateful acknowledged.

References

- Avalle, M., Belingardi, G. and Montanini, R., Characterization of polymeric structural foams under compressive impact loading by means of energyabsorption diagram. *International Journal of Impact Engineering*, 25, pp. 455-472, (2001).
- [2] Li, Q.M., Mines, R.A.W. and Birch, R.S., The crush behaviour of Rohacell-51WF structural foam. *International Journal of Solids and Structures*, 37, pp. 6321 – 6341, 2000.
- [3] Triantafillou, T.C., Zhang, J., Shercliff, T.L., Gibson, J.L. and Ashby, M.F., Failure surface for cellular materials under multiaxial loading-II Comparison of model with experimental. *International Journal of Mechanical Science*, **31**, pp. 665 – 678, 1989.
- [4] Gibson, J.L. and Ashby, M.F., *Cellular Solids*. Cambridge University Press, 1997.
- [5] Alias, A. and Mines, R.A.W., Experimental results and techniques on the crush behaviour of structural foam. *Proc. of the 3rd International Symposium* on *Impact Engineering*, Singapore, pp. 379 – 384, 1998.
- [6] Mines, R.A.W., Li, Q.M., Alias, A., Birch, R.S. and Close, J.A., On the measurement of the crush behaviour of structural foams. *Proc of the 11th International Conference on Experimental Mechanics*, Oxford, 1998.
- [7] Rejab, M.R.M., Alias, A. and Ismail, Y.S. *In-situ* technique in manufacturing structural sandwich beams. *Proc. of Research Seminar on Materials and Constructions*, UTM Skudai, October 2002.