# ANALYSIS AND COUNTERMEASURE TO IMPROVE OVERALL EQUIPMENT EFFECTIVENESS (OEE) ON CHASSIS LINE AT TAN CHONG INDUSTRY 

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ANALYSIS AND COUNTERMEASURE TO IMPROVE OVERALL EQUIPMENT EFFECTIVENESS (OEE) ON CHASSIS LINE AT TAN CHONG INDUSTRY

NUR SYAHIRAH BINTI ISMAIL

Thesis submitted in fulfilment of the requirements for the award of the degree of B.Eng. (Hons.) Manufacturing Engineering

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#### Abstract

Overall Equipment Effectiveness (OEE) is a powerful metric of manufacturing performance incorporating measures of the utilization, yield and efficiency of a given process, machine or manufacturing line. When associated with the reasons for performance loss, OEE provides the means to compare and priorities improvement efforts. This project assesses the current condition of Chassis-Final Assembly lines of Nissan Tan Chong Motor Assemblies Sdn Bhd, a company of car manufacturer in order to reduce unplanned downtime due to line stoppages to maximize the productivity. Before obtaining the data to calculate the existing OEE value, the product or process that have the highest downtime rate need to be identified at Chassis-Final Assembly Department. The methods used to analyze these various causes were control chart to find the out of control point, Pareto Analysis to find the critical problem, Ishikawa diagram to find causes affecting the problem, and 5 W 1 H to proposed the recommendation. After knowing the causes of various activities that leads to high downtime rate, then recommendations for OEE improvements are $84.35 \%$ and $84.31 \%$ for A, and B shift respectively. From the existing to world class ranking OEE there are improved by $4.51 \%$ and $4.71 \%$ for A, and B shift respectively, that could be used by Nissan Tan Chong Motor Assemblies Sdn Bhd were ready to be made.


#### Abstract

ABSTRAK

Keberkesanan keseluruhan Equipment (OEE) adalah metrik kuat pembuatan langkahlangkah prestasi pemerbadanan penggunaan, hasil dan kecekapan proses, mesin atau pembuatan garis diberikan. Apabila dikaitkan dengan sebab-sebab bagi kehilangan prestasi, OEE menyediakan cara-cara untuk membandingkan dan usaha keutamaan penambahbaikan. Projek ini menilai keadaan semasa garis Perhimpunan Chassis-Final Nissan Tan Chong Motor Assemblies Sdn Bhd, sebuah syarikat pengeluar kereta untuk mengurangkan tidak dirancang kerugian masa ke atas penamatan baris kerja untuk memaksimumkan produktiviti. Sebelum mendapatkan data untuk mengira nilai OEE yang sedia ada, produk atau proses yang mempunyai tertinggi menurunkan kadar masa perlu dikenal pasti di Chassis-Final Jabatan Perhimpunan. Kaedah yang digunakan untuk menganalisis pelbagai sebab adalah carta kawalan untuk mencari titik keluar dari kawalan, Analisis Pareto untuk mencari masalah yang kritikal, gambarajah Ishikawa untuk mengesan punca utama masalah, dan 5 W 1 H untuk mengusulkan cadangan. Setelah mengetahui punca-punca pelbagai aktiviti yang membawa kepada kadar downtime tinggi, maka cadangan untuk penambahbaikan yang boleh digunakan oleh Nissan Tan Chong Motor Assemblies Sdn Bhd bersedia untuk dibuat.


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## LIST OF ABBREVIATIONS

OEE Overall Equipment Effectiveness
TPM Total Productive Maintenance

## CHAPTER 1

## INTRODUCTION

### 1.1 INTRODUCTION

This chapter discusses about the introduction, overall ideas and concepts to the Total Productive Maintenance (TPM) and Overall Equipment Effectiveness (OEE). Besides, the background of the study, problem statements, objective of the study, and scope of the study will also be described in details in the sections below.

### 1.2 BACKGROUND OF STUDY

In a competitive market, the growing demand for quality as the most important factor for a company to survive in the global market is growing. Quality is important in determining the economic success of manufacturing companies. Total Quality Management (TQM) is an approach to improve the quality of goods and services delivered through the involvement of individuals at all levels and functions of the organization. Quality management practices also help improve in reducing scrap, rework and stabilize the production process. Thus, can reduce production costs and increase productivity.

Tan Chong Motor Assemblies Sdn. Bhd. (TCMA) was selected to be studied in this research. It is one of the largest national conglomerates involved in a myriad of business activities. The current activities of the Tan Chong Motor Assemblies Sdn. Bhd. (TCMA) are assembly and distribution of motor vehicles, provision after-sales services and motor related financial services.

This study is conducted by choosing the Assembly Shop Chassis line as a research. Assembly Chassis line has 2 shifts with 7.9 hours per shift, which means the total operation per shift is 474 minutes-based. They explained that they are facing a high probability of loss of production lines for machine damage stoppage.

Through the first visit to the company in accordance Assembly Shop Chassis line, the operator were observed that they could not read the air leak tester due to failure of reading and Chassis-Final conveyor cannot running very well. In addition, the chassis assembly line downtime loss is 10 to 20 minutes by the time available of 474 minutes per shift, therefore, the operating time was decrease to 4.22 per cent, and this is due to equipment failure affected from waiting and no raw materials. Downtime losses was reflected to low availability. The number of units produced is 50 units out of total potential targets of 60 units in every shift. So that, it shown that the performance is low by 83.3 percent. This is due to minor stoppage due to speed loss because the machine not running smoothly at stable speed. Losses of speed also reflected to low performance of equipment. There are also issues of quality of the process and the vehicle, the number of defects per shift is 5 units from 50 units produced per shift. Therefore, the quality of the product decreased to 10 percent because of the product did not meet the specifications.

Any number of factors leading to low production output with machine operating time low. The maintenance department has been struggling to make a countermeasure with equipment be tracked in a problem. They have done a monthly maintenance practices in the last 3 months; however, the results did not show any significant progress in the breakdown of machinery. Given this situation, there is a need to observe and study the causes of machine damage and suggest the most appropriate method for further improvement that can benefit the production process.

### 1.3 PROBLEM STATEMENT

From the observation made in the Assembly Shop Chassis line, there have a number of machine breakdown, line stoppage cases through the production, the productivity not achieve the target and also the low product quality and affect the

Overall Equipment Effectiveness (OEE). So that, this research is to study and analyze the existing of Overall Equipment Effectiveness (OEE) and to propose on how to improve the productivity by reduced the machine breakdown, decrease the defects and increase the quality of productivity.

### 1.4 OBJECTIVE OF STUDY

This research was carried out to:

- To identify and analyse the elements of Overall Equipment Effectiveness (OEE).
- To calculate the existing of Overall Equipment Effectiveness (OEE).
- To evaluate, analyse and proposed improvement of the revised Overall Equipment Effectiveness (OEE).


### 1.5 SCOPE OF STUDY

The project objective is narrowed down by performing scopes of study.

- A case study will be conducted at Tan Chong Motor Assemblies Sdn. Bhd. On Assembly Shop Chassis line area.
- The study will be conducted for a period of 3 months for the latest Overall Equipment Effectiveness (OEE).


## CHAPTER 2

## LITERATURE REVIEW

### 2.1 INTRODUCTION

This chapter describes the principle of Overall Equipment Effectiveness and Total Productive Maintenance in general, and the principles behind the system. All related terms, terminology and formulas will be clearly stated.

### 2.2 HISTORY OF THE MAINTENANCE

Traditionally, maintenance is considered to be carried out to repair the broken machine, and the machine is considered to be fixed, to perform the operation correctly. Maintenance tasks are include re-adjust, replace parts or components, oil change, lubrication and cleaning (Sullivan, 2004). Literature maintenance often show flow changes from three generations before World War II had begun, as shown in Figure 2.1.


Figure 2.1: The Maintenance History

### 2.3 TOTAL PRODUCTIVE MAINTENANCE (TPM)

TPM is one of total quality culture that followed many good practices; it is through the use of lean principles to increase their competitiveness. The new assignment is likely to include improved equipment, repair, training, preventive maintenance, predictive maintenance. The task is transferred to production Kaizen including easy maintenance, cleaning, inspection, lubrication, and adjustments. Figure 2.2 shows schematically how TPM switch the stewardship of the Department of Production Maintenance team.


Figure 2.2: TPM Shifts Maintenance Tasks

### 2.3.1 Define Total Productive Maintenance (TPM)

Total Productive Maintenance (TPM) is a maintenance philosophy that requires total participation in the labour force. TPM combines the ease and availability of the skills of all employees with a focus on improving the overall efficiency of the facility. Efficiency is enhanced by eliminating the waste of time and resources. Typically, total productive maintenance is a concept that is easy to use for most of the manufacturing facility.

### 2.3.2 8 Pillar of TPM

Ahuja and Kamba (2008) was said that there is an eight pillar of TPM. By implementing all of these pillars, the TPM will function correctly and can absolutely help the company to achieve their goals. The eight pillars of TPM are mostly focused on proactive and preventative techniques for improving equipment reliability. The eight pillars of TPM illustrated in Figure 2.3.


Figure 2.3: Eight Pillars Approach for TPM

### 2.4 OVERALL EQUIPMENT EFFECTIVENESS

OEE is a tools to measure and recognized that the equipment breakdown sources by production losses. OEE is a simple tool that will help managers to evaluate their effectiveness equipment. (Sermin Elevli and Birol Elevli 2010) It is the most common and important loss of productivity, which is called the six big losses and are given in Table 2.1. Equation below is to measure the equipment effectiveness.

OEE $=$ Availability $\times$ Performance $\times$ Quality

Table 2.1: Six Big Losses of Equipment

| Category | OEE Loss | Example |
| :--- | :--- | :--- |
| Breakdowns <br> Setup adjustment | Availability | Tooling failures <br> Setup / Changeover |
| Small stop <br> Reduced speed | Performance | Cleaning / checking <br> Inefficient operator |
| Startup rejects <br> Production rejects | Quality | Incorrect assembly <br> Scrap / rework |

Overall equipment effectiveness (OEE) is a hierarchy of metrics developed by Seiichi Nakajima in (by Harrington Emerson in 1960 in a way of thinking about the labor efficiency) that evaluates and demonstrates how effective manufacturing operations used.

### 2.4.1 The Elements of Overall Equipment Effectiveness

Overall equipment effectiveness is calculated by combining three factors of the availability rate, the performance rate, and the quality rate.

Availability is the ratio of the amount of time that the tool capable to running a quality product to the total time it could be running. Availability rate can be defined as follows:

Availability $=($ Total Operating Time - Downtime $) /$ Total Time Available

Performance of tools is defined as the ratio of the amount of product made to the amount of target product that could be made. Then, performance is determined as follows:

Performance $=$ number of unit manufactured $/$ possible number of units (target)

Quality of the product is the ratio of the amount of good products made to the total amount of product made. The rate of quality can be determined as follows:

Quality = number of goods unit produced / number of units produced

### 2.4.2 World Class Ranking of OEE

Generally accepted world class target for each factor different from each other. Table 2.2 below shows the percentage of world class ranking of OEE.

Table 2.2: World Class of OEE Factor

| OEE Factor | World Class |
| :--- | :--- |
| Availability | $90.0 \%$ |
| Performance | $95.0 \%$ |
| Quality | $99.9 \%$ |
| Overall OEE | $85.0 \%$ |

### 2.5 PROCESS IMPROVEMENT TOOLS

Process improvement is important to be used to determine an ongoing process within the company to achieve target and objectives. The most used methods in the implementation process, tools and techniques will be shown as below:
i. Pareto analysis
ii. Cause And Effect Analysis
iii. Statistical Process Control (SPC) Charts
iv. 5 Whys Analysis
v. 5W IH Analysis

### 2.5.1 Pareto Charts

Pareto charts was invented by an economist who is Alfredo Pareto that listed that by a few people that controlled the most of the nation's wealth. Pareto charts is a simple method for identifying priority of changes to identify the problem. From this method, we can prioritize the most perfect state of individual modifications. Figure 2.4. shows the type of Pareto Charts.


Figure 2.4: Pareto Chart

### 2.5.2 Ishikawa Diagram

Ishikawa diagram was invented by Kaoru Ishikawa. It is also called fishbone diagrams. Function of Ishikawa diagram is to identify the factors that are causes the undesired effect or defects. The major factors of the Ishikawa diagrams are Method, Man, Machine, Material and Environment. The completed Ishikawa diagram is shown in Figure 2.5.


Figure 2.5: Ishikawa Diagram

### 2.5.3 Control Chart

A control chart is a graph used to study how the process of change over time. Data was plotted for the future control. Control charts always have a diameter of an average, the top line of the upper control limit and the lower line of the lower control limit.

### 2.5.4 5Whys Method

The 5-Whys Method was invented by Toyota Founder, Kiichiro Toyoda's father Sakichi and become popular in the 1970s by the Toyota Production System. The 5Whys Method is a strategy that involve in solving problem by looking at any problem asking: "Why?" and "What causes the problem?". It is a simple tool to determine the root cause of a problem. It can be done by using an innovative and creative technique, such as brainstorming, by asking questions repeatedly as shown in Figure 2.6.

5 Why Analysis


Figure 2.6: 5Whys Method

### 2.5.5 5W1H Method

5W1H shown in Figure 2.7 is the first problem solving tool in a team have been taught. This is the most recommended method to use initially. This method is not
depends on technical skills and it is easy to used. This method ensures a team involved in problem solving process. Another way to help is brainstorming, which more reasons are described in Table 2.3. The 5W1H simple method can also be used to simplify the analysis process.


Figure 2.7: 5W1H Method

Table 2.3: 5W1H Analysis Example

| What | What should be improved? What is the purpose of the improvement? |
| :--- | :--- |
| Where | Is the workers orientation or method correct when changing the <br> workplace? |
| When | Change the time, period or sequence of the operation. |
| Who | Manpower, collaboration or task assignment. Check and discuss this <br> issue again. |
| How | Is there better method to replace the current one? |
| Why | Why follow the present way. Is there any necessary change? |

## CHAPTER 3

## METHODOLOGY

### 3.1 INTRODUCTION

This chapter describes the description of the methods to be used for this research. A methodology can be considered to include a various methods. It can be also defined as the study or description of methods. This study is based on observation on events happens in Tan Chong Motor Assemblies Sdn. Bhd. The flow chart in Figure 3.1 shows the steps that will be taken in this research.

### 3.2 EXPLANATION OF FLOWCHART

### 3.2.1 Research Background

In a field study of any organization that involves the establishment of information and reference real and tangible by the operator in the field. It can also be defined as a set of laboratory information and settings outside the workplace. This process involves the determination of accurate data on what is important, what kind of methods used included interviews informal group of direct observation, life group discussions, self-analysis, personal files, the resulting analysis, and the history of life.

At this level, the method used was to put to direct observation in order to gather information in an overview of the problems in selected company. First of all, the company must be selected to make observations and case studies. Application letter was drafted and sent to the Tan Chong Motor Assemblies Sdn Bhd. visit the company made
an appointment before visiting. During the visit, an industrial engineer and plant manager briefly describes the background of the company; the type of products manufactured, their main customer and how the product is produced. After the presentation, a visit to the Department of Maintenance been held to get an overview of how the parts are produced. Some of the problems highlighted by the engineers and all the problems that were jotted down for analysis purposes.


Figure 3.1: Flowchart of Study Framework

### 3.2.2 Problem Identification

Identification of the problem is defined as identify problems before trying to solve it. In other words, it is the first strategy in problem solving. First, we must realize and accept that there is a problem. Once a problem has been identified, then made direct observations. The information collected in connection with the problem as soon as possible to begin work on a solution.

### 3.2.3 Data Collection

Collection of data is defined as data collection and processing information by measuring the variables of interest, in a systematic pattern created that can answer research questions as stated, hypothesis testing, and evaluating results. The collection of data necessary step in order to establish a consistent analytical approach to problem occurs. The method of collecting data is to use Overall Equipment Effectiveness (OEE).

### 3.2.4 Overview of Literature

The literature review is conducted after the data is collected. In the literature review, similar methods are found from other journals, thesis, published papers, and articles. From the study, all the methods and solutions are summarized and the most suitable method is selected.

### 3.2.5 Data Analysis and Processing

The method of analysis will be carried out in the next chapter where to find the problem by using some of the tools that will be exposed. In order to find a solution, of data must be collected in accordance with the specification analysis. Analysis is the process of solving complex topic or issue into parts smaller in order to obtain a better understanding of it. In this study, of data relating collected and then move on to the next process of analyzing the of data. One of the main purposes of of data analysis is to find
the cause of the problem, highlighting useful information, suggesting conclusions, and supporting decision making.

### 3.2.6 Conclusion and Recommendation

Various issues were integrated, covered in paper, and understanding into all comment. This includes observing the discussions, proposals, and further studies are required to remove any residue. It is recommended for future solutions to improve the OEE, in order to improve the efficiency of the equipment.

## CHAPTER 4

## RESULTS AND DISCUSSIONS

### 4.1 INTRODUCTION

This chapter will discuss the results of the study and presented the results in the industry related to real-time production monitoring system. This chapter will also show information and data to analyze and discuss.

Based on the results and information obtained from observations and records of the factory, there are a few tables, diagrams and graphs that have been built. There are several explanations for the details of the data and calculations are made to determine the availability and overall equipment per the last record.

### 4.2 DATA COLLECTION

### 4.2.1 Company Background

Tan Chong Motor Assemblies Sdn Bhd was choosen to be study in this studies. Tan Chong Motor Assemblies Sdn Bhd (TCMA) is a subsidiary of Tan Chong Motor Holdings (TCMH). Tan Chong Motor Holdings Berhad (TCMH) was incorporated in Malaysia on 14 October 1972. From the humble beginning as the distributor of small motor vehicles by its founders back in the 1950s, TCMH Group (the Group) has grown up into one of the largest national conglomerates involved in a myriad of business activities; from the assembly and marketing of motor vehicles and auto parts manufacturing to property development as well as trading in various
heavy machineries, industrial equipment and consumer products both locally and abroad.

As part of a restructuring exercise to strengthen our foothold as an industry major player; in 1998 various business interests of TCMH abroad were eventually demerged and subsequently listed on The Stock Exchange of Hong Kong Limited under the Tan Chong International Limited flagship. This was followed by the demerger of its automotive parts division, non-motor division involving cosmetics, undergarments, and the distribution of heavy machinery as well as tourism-related businesses; which was subsequently listed on the Main Board of Bursa Malaysia Berhad in 1999 under APM Automotive Holdings Berhad and Warisan TC Holdings Berhad respectively. These exercises have enabled the Group to realign its focus on motor industry business.

TCMH is basically an investment holding company and the Group's current principal activities among others are; assembly and distribution of motor vehicles, provision of after-sales services and motor related financial services such as hire purchase, an insurance agency, and leasing.

The Group is the franchise holder and exclusive distributor of Nissan passenger and light commercial vehicles as well as Renault vehicles in Malaysia. The vehicle distribution business is operated with an extensive network of sales branches and authorized dealership outlets nationwide; supported by more than 80 after-sales service centre. We are also the franchise holder and exclusive distributor for trucks and buses under the UD Trucks and Silverbus brands, operating through an established network of sales branches and sales dealers, after-sales branches and authorized service dealers. Having achieved a notable market share for heavy commercial vehicles (HCV), light commercial vehicles (LCV) and buses, the Group is recognized as one of the leading commercial vehicle distributors in Malaysia.

The two assembly plants in Segambut (Kuala Lumpur) and Serendah (Selangor) have very close capacity; both plants together can deliver 100,000 units a year with additional shift and reasonable overtime; the Group's vehicles sales enjoyed a market
share of $12.1 \%$ for non-national cars and $6.4 \%$ for the industry-wide market as of September 2014.

### 4.2.2 Corporate Logo



Figure 4.1: Tan Chong Motor Assemblies Sdn Bhd Corporate Logo

The four Discs represent four major diverse interest groups, namely: as Shareholders, Employees, Suppliers and Public and Customers. The position of the Discs portrays the four corners of the social economics of the nation - north, south, east and west - to where our business activities extend. The four Discs represent four major diverse interest groups, namely as Shareholders, Employees, Suppliers and Public and Customers.

The position of the Discs portrays the four corners of the social economics of the nation - north, south, east and west - to where our business activities extend. The central inflated Red Cross represents the concerted efforts with which the company's businessactivities are extended to the abovementioned four diverse groups in a systematic manner towards the attainment of our corporate objectives with increased prosperity.

The red which symbolises prosperity and blue which symbolises loyalty are colours technically chosen to highlight the image of the company and its subsidiaries. The factory was awarded the ISO 9001:2000 for Quality Management Systems (QMS) and ISO 14001:2004 for Environmental Management Systems (EMS).

### 4.2.2.1 Vision, Mission and Objective of Organization

Nissan is developing corporate activities centred on automobile manufacturing based on our vision of "enriching people's lives." In order for cars, which provide mobility, to truly become reliable partners for our customers, a number of issues including global environmental issues, traffic accidents and congestion problems must be tackled as part of a long-term vision. To realize our vision, Nissan is developing technologies based on a framework called the "Orchard" concept.Technical development encompasses a wide range of elements. It is necessary to think about how we will look at technology development and formulate strategies and plans for such development. For example, there are various technologies ranging from ones we wish to introduce onto the market right away, to basic ones that are developed slowly over time. The "Orchard" concept is an overall construct that allows us to think about these various technologies in a comprehensive manner.Nissan must have its own distinct value so that customers will choose Nissan cars. When combined, our activities to produce such value can be likened to the management of a fruit orchard in which "fruit" is planted and raised. The process is defined as having the following three phases.

## 1. Harvest Plan

First, we develop a plan for commercializing the technology. We clarify the value the technology holds for the target customers, who have been clearly defined based on the technology's performance and functions, as well as the time frame for the provision of the technology. We are not developing technology simply for technology's sake. We must formulate plans in conjunction with social needs and market demands in order to provide in a timely fashion value that pleases customers.

## 2. Seeding \& Growth

Next, we plan the strategy and implementation that will make the Harvest Plan a reality. We specify what elemental technologies are needed in order to make the Harvest Plan a reality and form strategies for developing them quickly and at a high level of quality. We plan and implement partnerships with universities and suppliers, lobby government officials, establish new organizations and structures,
make regular progress reviews, and continuously improve the technology after it has been introduced.
3. Soil Enrichment

This phase includes fundamental technologies and basic research, which are required competencies for continuing to create value in the long term. Some examples are technologies that improve reliability, which form the soil of the orchard; analysis and measurement technologies; and material technologies. In order to raise quality in the car manufacturing process, which runs from research and advanced development to car development, it is necessary to enrich the "soil" of the orchard with technology management that covers human resources and intrinsic company processes. Nissan's "orchard" includes a number of key technology areas, including the environment and safety. We discuss Harvest Plans for each area and plan and develop technologies for each over the mid and long terms.

### 4.2.2.1.1 Objective

### 4.2.2.1.1.1 Quality Policy

Aims to maintain and improve its position as high as quality automobile assembler by following quality policy

1. to continually satisfy customer requirements.
2. Company wide Quality Management System (QMS)
3. Manpower development through training and education.
4. Achieve built-in quality at lowest cost.

### 4.2.2.1.1.2 Environmental Policy

## Tan Chong Motor Assemblies Sdn Bhd is committed and will endeavour

To comply and adhere to applicable law, regulations and other requirements in the interest of communities where we operate.

Continually improve environmental performance by actively pursuing pollution prevention, energy conservation and waste reduction.

5S Policy

We are committed to continuously maintain a high standard of 5 S practices at our workplace though teamwork and self-discipline to improve quality, productivity and create harmonious and conducive working environment in line with Company Policy

### 4.2.3 Organizational Chart

There are 5 divisions in Tan Chong Motor Assemblies Sdn Bhd. The divisions at Tan Chong Motor consists of Manufacturing, Engineering Services, Finance, Admin, Multimedia System, General Admin, Purchasing and Local. Figure 4.2 shows the organizational chart of Tan Chong Motor Assemblies Sdn Bhd .

In the Manufacturing section, there is 4 department under this division. There is Body Shop, Paint Shop, Assembly Line and Logistics. Each of the department have their own responsible. For the Engineering Services there are 4 departments, each of the department have their own functions for the company. There is Nissan Production Way (NPW),Quality Department (QD),Production Engineering Department (PED), Maintenance and Jig. Under the Nissan Production Way (NPW) there is 3 sections, there is IE, GK and PPC. Another department is General Admin that responsible for the human resources, payroll, safety and hostel.


Figure 4.2: Organizational Chart of the Tan Chong Motor Assemblies Sdn Bhd

### 4.2.4 Manufacturing process of Tan Chong Motor Assemblies Sdn Bhd



Figure 4.3: Process flow of Tan Chong Motor Assemblies Sdn Bhd Manufacturing

### 4.2.4.1 Body shop

The Body Shop is a highly automated section of the factory with robots in operation. Pressed-panels are welded together to create complete body shells.

### 4.2.4.2 Paint shop

Body shells are painted in a semi-clean environment using solvent-based paint. Shells are dipped in chemical tanks to cleanse them of any oils picked up on the panels during their manufacture in Body Shop. Once bodies have been dipped and cleansed, they are then immersed in an anti-corrosion paint dip called ED (Electrocoat Dip). This 'dip' coats the entire body, both inside and outside, and is the first paint coating it will receive. Once the 'dipped' body has been stoved in the ED oven, the body progresses to the 'Sealing' Booth. In this booth, the body has its interior panel joints, floor, tailgate, hood and door edges sealed with a PVC based sealant, to prevent water ingress and corrosion as the car is driven on the road. Also within this zone, sound pads are added to the floor and boot to reduce road noise (standard practice in the motor industry). The next booth it enters is the 'Underbody' Booth. In this booth, similar to 'Sealing' Booth, the body's wheel arches are sealed using the same PVC based sealant. Robots then apply the underseal to the underfloor and wheel arches. Also robots are used to apply the SGC (Stone Guard Coat) layer to
the sills: this coating is designed for abrasion resistance, i.e. preventing stone chips, scuffs, etc. From here, the body proceeds into the Undercoat Oven. The next zone is 'ED Sanding' booth where the body is inspected for any minor imperfections received in the ED Coat. The next zone is the 'Surfacer' Booth, where the body receives its second coat of paint, this being the Surfacer Coat, then into the Surfacer Oven. Next is 'Surfacer Sanding' Booth: the same as ED Sanding, this zone inspects the body for any imperfections picked up within the Surfacer coating. Next comes the 'Topcoat' Booth, where the body receives its final coats of paint, these being Topcoat and Clearcoat layers. After being stoved in the Topcoat oven, the body then enters the 'Touch-up' Booth where the body has its final inspection for any imperfections picked up in the Topcoat process. Once the body leaves here, it then moves on to the PBS (Painted Body Store) above Trim and Chassis to await the next step in the production process.

### 4.2.4.3 Assembly Line

There are two parallel assembly lines in TCMA: Line A currently handles the P32R and J32Q; Line B handles the L02B and M11X. Painted bodies are stored in a large holding area called PBS (Painted Body Store), and are released in a specific scheduled sequence. They are brought into Trim \& Chassis on suspended cradles. Each body moves through the assembly line and is fitted with interior (Trim), and exterior (Chassis) components. At one point in the process, the bodies are 'married' to a sub-assembled engine and subframe. Completed vehicles are sent down a Final Line, where all aspects of the car, from brakes to waterproofing, are tested. The car is then driven off-line to a holding area, ready to be distributed to a dealer

### 4.2.5 Process Flow in Chassis Line

Figure 4.4 shows the process happening in Chassis line, there are 12 sections for each process. After a trim line settles down, next to be chassis process that begins with process Underfloor 1 and 2 which include the process to fix the pipe, hose, and band assy fuel tank mounting into the front floor by using insulin heat and set control card. Next process of rear Axle sub 1 and 2 which is the process to fix and fit the component
such ABS assy shock, hoist, tube assy brake and drive shaft at the rear beam. After that, Rear and Front Disc subprocess which install the front brake, adjust beam at brake assy and set hub at rear brake assy. Next, the process of engine mounting 1,2 and 3 which include fix engine on left and right side, then fix the bracket assy torque and propeller shaft. After that, process engine sub 1 and 2 which include a process to fix the gearbox and assemble cable with harness and hose. Next, engine sub 3 added with engine drop which process include fixing alternator, compressor and motor assy, then mounting the engine with the front strut and tighten with oil disc. And then, process steering member combined with engine drop which is set the engine with the lifter and set drive shaft and rear disc and fix with struts. And then front axle with steering link which is the process to fix the engine frame with struts. Proceed into undercarriage process which is to assemble propeller shaft with disc stopper and adjust at the front disc, and then assemble extractor, cover the assay and exhaust sensor with gasket. Next process goes to engine room 1 and 2 and the engine room 3 which is fix torque road, duct assy air, battery bracket and front bumper. Lastly, process tire fitting which includes inserting tire and fixes the machine and runs the machine, after that install valve into tire lastly removes the tire from the machine. After chassis process done, it will next transfer into final line process.


Figure 4.4: Process in Chassis Line

### 4.3 CURRENT CONDITION

In the beginning, data is recorded to identify any problems during the machine has been set up. Higher down time occurred during the preparation of the machine on which it will indicate the problem. The data will identify and count to get the OEE, availability, quality and performance. It intends to examine the problems affecting the OEE. In order to produce a better product at a lower damage, the company wants to cut their losses. The best products means that it comply with the specifications given.

Attribute data are typical for the size of the data or the sample size in the range of 50-10 per sample, it signifies a qualitative sample and good or bad. Using the p type of chart will calculate the percentage of defects in the sample. P chart will be built using Microsoft excel. Out of control chart, identify processes that are out of control. The process needs to be stabilized before it can improve the process of dealing with the problem.

Special causes require immediate analysis of cause and effect to eliminate variation. Once out of the control samples are removed (revised), attention will go to the control samples were sampled within the control limits. Then remove the samples will be carried out under the control limits (target). So last chart shows the maximum value of each of availability, performance, quality and overall equipment effectiveness. The investigation using Ishikawa diagrams necessary to determine whether a special reason will be changed. So from the same cause, it will use to solve problems in the production line.

### 4.3.1 Calculating Existing OEE

Table 4.1: Example of machine production data for sample on 01/07/2015 for Shift A

| Production data |  |
| :--- | :--- |
| Shift length | 545 minutes |
| Tea breaks | 15 minutes |
| Lunch break | 35 minutes |
| Meeting, walking, 5S | 21 minutes |
| Down time | 71 minutes |
| Actual cycle time | 5.18 minutes/unit |
| Total output | 2 units |
| Offline unit | 55 units $\times 7.18$ minutes/unit $=395$ <br> minutes |
| Net operation time $=$ Total output per shift <br> actual cycle time |  |

Table 4.2: Processing data

| Support variable | Calculation | Result |
| :--- | :--- | :--- |
| Planned <br> production time | Total operating hours per shift - <br> planned downtime per shift | 453 minutes -71 minutes $=$ <br> 474 minutes |
| Operation time | Planned production time <br> downtime loss- speed loss | 474 minutes -0 minute -0 <br> minute $=474$ minutes |
| OK product | Total output per shift - offline unit <br> per day | 55 units -2 units $=53$ units |

Table 4.3: Calculation of OEE factor

| OEE factor | Calculation | OEE | $\%$ OEE |
| :--- | :--- | :--- | :--- |
| Availability | Operation time / planned <br> production time | $474 / 474=1.00$ | 100 |
| Performance | net operation time $/$ operation <br> time | $395 / 474=0.833$ |  |
| Quality | OK product / total output | $53 / 55=0.964$ | 83.3 |
| Overalll OEE | Availability $\times$ Performance $\times$ <br> Quality | $1.00 \times 0.833 \times 0.964$ <br> $=0.803$ | 80.3 |

Table 4.1 shows the example of machine production data for sample on 01/07/2015 for Shift A in Chassis final, table 4.2 shows the processing data to calculate the support variable and table 4.3 shows the calculation to calculate the factor of availability, performance and quality to find the percentage of OEE factor.

### 4.4 DATA ANALYSIS

The process of evaluating data using analytical and logical reasoning to examine each component of the data provided. This form of analysis is just one of the many steps that must be completed when conducting a research experiment. Data from various sources is gathered, reviewed, and then analyzed to form some sort of finding or conclusion. There is a variety of specific data analysis method, some of which include data mining, text analytics, business intelligence, and data visualizations.

### 4.4.1 Current Condition Control Chart

Control chart is constructed to find the percentage value for each component in OEE of Availability, Performance and Quality. The pattern was observed in the control chart by supporting information gathered from the data collected.

### 4.4.1.1 Availability

### 4.4.1.1.1 Shift A

Table 4.4 shows the availability data get from plant and calculate using the p chart equation to get percentage of availability for shift A and shows the out of control point in the data. Above shows the calculation for availability factor on July 1st 2015 for Shift A for existing condition. Figure 4.5 shows the availability control chart for Shift A and constructed to find the percentage of availability pattern. Average value is 0.9909 , while UCL and LCL value is vary based on their n number.

Table 4.4: control chart data for Availability in shift A

| DAY | OPERATION TIME | PLANNED PRODUCTION TIME | AVAILABILITY (p) | CENTER (P-BAR) | UCL | LCL | SIGMA P BAR | z |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-Jul-15 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 2 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 3 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 6 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 7 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 8 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 9 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 10 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 11 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 13 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 14 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 22 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 23 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 24 | 472 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 27 | 463 | 474 | 0.98 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 28 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 29 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 30 | 465 | 474 | 0.98 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 3-Aug-15 | 534 | 534 | 1.00 | 0.9909 | 1.0032 | 0.9786 | 0.0041 | 3.0000 |
| 4 | 534 | 534 | 1.00 | 0.9909 | 1.0032 | 0.9786 | 0.0041 | 3.0000 |
| 5 | 534 | 534 | 1.00 | 0.9909 | 1.0032 | 0.9786 | 0.0041 | 3.0000 |
| 6 | 534 | 534 | 1.00 | 0.9909 | 1.0032 | 0.9786 | 0.0041 | 3.0000 |
| 7 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 10 | 448 | 474 | 0.95 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 13 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 15 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 17 | 435 | 474 | 0.92 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 18 | 525 | 534 | 0.98 | 0.9909 | 1.0032 | 0.9786 | 0.0041 | 3.0000 |
| 19 | 534 | 534 | 1.00 | 0.9909 | 1.0032 | 0.9786 | 0.0041 | 3.0000 |
| 20 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 21 | 534 | 534 | 1.00 | 0.9909 | 1.0032 | 0.9786 | 0.0041 | 3.0000 |
| 22 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 24 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 25 | 437 | 474 | 0.92 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 26 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 27 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 3-Sep-15 | 523 | 534 | 0.98 | 0.9909 | 1.0032 | 0.9786 | 0.0041 | 3.0000 |
| 4 | 514 | 534 | 0.96 | 0.9909 | 1.0032 | 0.9786 | 0.0041 | 3.0000 |
| 10 | 466 | 474 | 0.98 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 11 | 447 | 456 | 0.98 | 0.9909 | 1.0042 | 0.9776 | 0.0044 | 3.0000 |
| 12 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 14 | 479 | 484 | 0.99 | 0.9909 | 1.0038 | 0.9780 | 0.0043 | 3.0000 |
| 17 | 471 | 474 | 0.99 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 18 | 534 | 534 | 1.00 | 0.9909 | 1.0032 | 0.9786 | 0.0041 | 3.0000 |
| 19 | 526 | 534 | 0.99 | 0.9909 | 1.0032 | 0.9786 | 0.0041 | 3.0000 |
| 21 | 475 | 479 | 0.99 | 0.9909 | 1.0039 | 0.9779 | 0.0043 | 3.0000 |
| 22 | 474 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 28-Sep | 470 | 474 | 0.99 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 29 | 460 | 474 | 0.97 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 30 | 472 | 474 | 1.00 | 0.9909 | 1.0040 | 0.9778 | 0.0044 | 3.0000 |
| 24136 |  | $24357 \quad 0.9909$ |  |  |  |  |  |  |

$$
\begin{aligned}
& \begin{aligned}
\bar{p} & =\frac{24136}{24357} \\
& =0.9909
\end{aligned} \\
& \begin{aligned}
U C L_{p} & =0.9909+3 \sqrt{\frac{0.9909(1-0.9909)}{474}} \\
& =1.0040
\end{aligned} \\
& \begin{aligned}
L C L_{p} & =0.9909-3 \sqrt{\frac{0.9909(1-0.9909)}{474}} \\
& =0.9778
\end{aligned}
\end{aligned}
$$



Figure 4.5: Control Chart for Availability in Shift A

### 4.4.1.1.2 Shift B

Figure 4.6 shows the availability control chart for Shift B and constructed to find the percentage of availability pattern. Average value is 0.999 , while UCL and LCL value is varying based on their $n$ number.


Figure 4.6: Control Chart for Availability in Shift B

Referring to figure 4.5 and figure 4.6, the process is out of control because there are points exceeding the control limit. However, point below the lower control limit are investigated and studied to help to increase the percentage in the future. The assignable cause responsible for the condition indicated that daily mechanical problems in this line, including machine breakdown and process quality problems.

### 4.4.1.2 Performance

### 4.4.1.2.1 Shift A

Table 4.5 shows the performance data get from plant and calculate using the p chart equation to get percentage of performance for shift A and shows the out of control point in the data. Above shows the calculation for performance factor on July 1st 2015 for Shift A for existing condition. Figure 4.7 shows the performance control chart for Shift A and constructed to find the percentage of availability pattern. Average value is 0.8507 , while UCL and LCL value is vary based on their n number.

Table 4.5: control chart data for Performance in shift A

| DAY | $\begin{gathered} \hline \text { NET OPERATION } \\ \text { TIME (np) } \\ \hline \end{gathered}$ | OPERATION TIME ( n ) | PERFORMANCE <br> (p) | CENTER P BAR | UCL | LCL | SIGMA P BAR | Z |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-Jul-15 | 395 | 474 | 0.833 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 2 | 395 | 474 | 0.833 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 3 | 359 | 474 | 0.757 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 6 | 431 | 474 | 0.909 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 7 | 409 | 474 | 0.863 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 8 | 452 | 474 | 0.954 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 9 | 359 | 474 | 0.757 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 10 | 359 | 474 | 0.757 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 11 | 373 | 474 | 0.787 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 13 | 381 | 474 | 0.804 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 14 | 395 | 474 | 0.833 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 22 | 409 | 474 | 0.863 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 23 | 402 | 474 | 0.848 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 24 | 402 | 472 | 0.852 | 0.8507 | 0.8999 | 0.8015 | 0.0164 | 3 |
| 27 | 373 | 463 | 0.806 | 0.8507 | 0.9004 | 0.8010 | 0.0166 | 3 |
| 28 | 402 | 474 | 0.848 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 29 | 402 | 474 | 0.848 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 30 | 395 | 465 | 0.849 | 0.8507 | 0.9003 | 0.8011 | 0.0165 | 3 |
| 3-Aug-15 | 503 | 534 | 0.942 | 0.8507 | 0.8970 | 0.8044 | 0.0154 | 3 |
| 4 | 416 | 534 | 0.779 | 0.8507 | 0.8970 | 0.8044 | 0.0154 | 3 |
| 5 | 474 | 534 | 0.888 | 0.8507 | 0.8970 | 0.8044 | 0.0154 | 3 |
| 6 | 445 | 534 | 0.833 | 0.8507 | 0.8970 | 0.8044 | 0.0154 | 3 |
| 7 | 445 | 474 | 0.939 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 10 | 373 | 448 | 0.833 | 0.8507 | 0.9012 | 0.8002 | 0.0168 | 3 |
| 13 | 460 | 474 | 0.970 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 15 | 359 | 474 | 0.757 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 17 | 408 | 435 | 0.938 | 0.8507 | 0.9020 | 0.7994 | 0.0171 | 3 |
| 18 | 352 | 525 | 0.670 | 0.8507 | 0.8974 | 0.8040 | 0.0156 | 3 |
| 19 | 394 | 534 | 0.738 | 0.8507 | 0.8970 | 0.8044 | 0.0154 | 3 |
| 20 | 422 | 474 | 0.890 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 21 | 493 | 534 | 0.923 | 0.8507 | 0.8970 | 0.8044 | 0.0154 | 3 |
| 22 | 465 | 474 | 0.981 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 24 | 444 | 474 | 0.937 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 25 | 429 | 437 | 0.982 | 0.8507 | 0.9018 | 0.7996 | 0.0170 | 3 |
| 26 | 458 | 474 | 0.966 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 27 | 352 | 474 | 0.743 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 3-Sep-15 | 452 | 523 | 0.864 | 0.8507 | 0.8975 | 0.8039 | 0.0156 | 3 |
| 4 | 359 | 514 | 0.698 | 0.8507 | 0.8979 | 0.8035 | 0.0157 | 3 |
| 10 | 395 | 466 | 0.848 | 0.8507 | 0.9002 | 0.8012 | 0.0165 | 3 |
| 11 | 330 | 447 | 0.738 | 0.8507 | 0.9013 | 0.8001 | 0.0169 | 3 |
| 12 | 438 | 474 | 0.924 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 14 | 409 | 479 | 0.854 | 0.8507 | 0.8996 | 0.8018 | 0.0163 | 3 |
| 17 | 401 | 471 | 0.851 | 0.8507 | 0.9000 | 0.8014 | 0.0164 | 3 |
| 18 | 493 | 534 | 0.923 | 0.8507 | 0.8970 | 0.8044 | 0.0154 | 3 |
| 19 | 500 | 526 | 0.951 | 0.8507 | 0.8973 | 0.8041 | 0.0155 | 3 |
| 21 | 429 | 475 | 0.903 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 22 | 401 | 474 | 0.846 | 0.8507 | 0.8998 | 0.8016 | 0.0164 | 3 |
| 28-Sep | 416 | 470 | 0.885 | 0.8507 | 0.9000 | 0.8014 | 0.0164 | 3 |
| 29 | 431 | 460 | 0.937 | 0.8507 | 0.9005 | 0.8009 | 0.0166 | 3 |
| 30 | 294 | 472 | 0.623 | 0.8507 | 0.8999 | 0.8015 | 0.0164 | 3 |
|  | 20533 | 24136 | 0.8507 |  |  |  |  |  |

$$
\begin{aligned}
\bar{p} & =\frac{20533}{24136} \\
& =0.8507
\end{aligned}
$$

$$
\begin{aligned}
U C L_{p} & =0.8507+3 \sqrt{\frac{0.8507(1-0.8507)}{474}} \\
& =0.8998 \\
L C L_{p} & =0.8507-3 \sqrt{\frac{0.8507(1-0.8507)}{474}} \\
& =0.8016
\end{aligned}
$$



Figure 4.7: Control Chart for Performance in Shift A

### 4.4.1.2.2 Shift B

Figure 4.8 shows the performance control chart for Shift B and constructed to find the percentage of performance pattern. Average value is 0.8227 , UCL and LCL value is varying because the n value is variable.


Figure 4.8: Control Chart for Performance in Shift B

Referring to figure 4.7 and figure 4.8, the process is out of control because there are points exceeding the control limit. However, point upper and lower control limit are investigated and studied to help to increase the percentage in the future. The assignable cause responsible for the condition indicated that daily mechanical problems in this line, including machine breakdown and process quality problems.

### 4.4.1.3 Quality

### 4.4.1.3.1 Shift A

Table 4.6 shows the quality data get from plant and calculate using the p chart equation to get percentage of quality for shift A and shows the out of control point in the data. Above shows the calculation for quality factor on July 1st 2015 for Shift A for existing condition. Figure 4.9 shows the quality control chart for Shift A and constructed to find the percentage of quality pattern. Average value is 0.9541 , while UCL and LCL value is vary based on their n number.

Table 4.6: control chart data for Quality in shift A

| DAY | OK PRODUCT PER SHIFT (np) | TOTAL OUTPUT PER SHIFT ( n ) | Quality (p) | CENTER (P-BAR) | UCL | LCL | SIGMA P-BAR | z |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-Jul-15 | 53 | 55 | 0.9636 | 0.9541 | 1.0388 | 0.8694 | 0.0282 | 3 |
| 2 | 54 | 55 | 0.9818 | 0.9541 | 1.0388 | 0.8694 | 0.0282 | 3 |
| 3 | 50 | 50 | 1.0000 | 0.9541 | 1.0429 | 0.8653 | 0.0296 | 3 |
| 6 | 58 | 60 | 0.9667 | 0.9541 | 1.0351 | 0.8731 | 0.0270 | 3 |
| 7 | 56 | 57 | 0.9825 | 0.9541 | 1.0373 | 0.8709 | 0.0277 | 3 |
| 8 | 57 | 63 | 0.9048 | 0.9541 | 1.0332 | 0.8750 | 0.0264 | 3 |
| 9 | 47 | 50 | 0.9400 | 0.9541 | 1.0429 | 0.8653 | 0.0296 | 3 |
| 10 | 48 | 50 | 0.9600 | 0.9541 | 1.0429 | 0.8653 | 0.0296 | 3 |
| 11 | 50 | 52 | 0.9615 | 0.9541 | 1.0412 | 0.8670 | 0.0290 | 3 |
| 13 | 53 | 53 | 1.0000 | 0.9541 | 1.0403 | 0.8679 | 0.0287 | 3 |
| 14 | 54 | 55 | 0.9818 | 0.9541 | 1.0388 | 0.8694 | 0.0282 | 3 |
| 22 | 55 | 57 | 0.9649 | 0.9541 | 1.0373 | 0.8709 | 0.0277 | 3 |
| 23 | 54 | 56 | 0.9643 | 0.9541 | 1.0380 | 0.8702 | 0.0280 | 3 |
| 24 | 55 | 56 | 0.9821 | 0.9541 | 1.0380 | 0.8702 | 0.0280 | 3 |
| 27 | 52 | 52 | 1.0000 | 0.9541 | 1.0412 | 0.8670 | 0.0290 | 3 |
| 28 | 56 | 56 | 1.0000 | 0.9541 | 1.0380 | 0.8702 | 0.0280 | 3 |
| 29 | 54 | 56 | 0.9643 | 0.9541 | 1.0380 | 0.8702 | 0.0280 | 3 |
| 30 | 54 | 55 | 0.9818 | 0.9541 | 1.0388 | 0.8694 | 0.0282 | 3 |
| 3-Aug-15 | 68 | 70 | 0.9714 | 0.9541 | 1.0291 | 0.8791 | 0.0250 | 3 |
| 4 | 57 | 58 | 0.9828 | 0.9541 | 1.0365 | 0.8717 | 0.0275 | 3 |
| 5 | 64 | 66 | 0.9697 | 0.9541 | 1.0314 | 0.8768 | 0.0258 | 3 |
| 6 | 61 | 62 | 0.9839 | 0.9541 | 1.0338 | 0.8744 | 0.0266 | 3 |
| 7 | 58 | 62 | 0.9355 | 0.9541 | 1.0338 | 0.8744 | 0.0266 | 3 |
| 10 | 49 | 52 | 0.9423 | 0.9541 | 1.0412 | 0.8670 | 0.0290 | 3 |
| 13 | 60 | 64 | 0.9375 | 0.9541 | 1.0326 | 0.8756 | 0.0262 | 3 |
| 15 | 45 | 50 | 0.9000 | 0.9541 | 1.0429 | 0.8653 | 0.0296 | 3 |
| 17 | 52 | 58 | 0.8966 | 0.9541 | 1.0365 | 0.8717 | 0.0275 | 3 |
| 18 | 48 | 50 | 0.9600 | 0.9541 | 1.0429 | 0.8653 | 0.0296 | 3 |
| 19 | 53 | 56 | 0.9464 | 0.9541 | 1.0380 | 0.8702 | 0.0280 | 3 |
| 20 | 57 | 60 | 0.9500 | 0.9541 | 1.0351 | 0.8731 | 0.0270 | 3 |
| 21 | 66 | 70 | 0.9429 | 0.9541 | 1.0291 | 0.8791 | 0.0250 | 3 |
| 22 | 64 | 66 | 0.9697 | 0.9541 | 1.0314 | 0.8768 | 0.0258 | 3 |
| 24 | 61 | 63 | 0.9683 | 0.9541 | 1.0332 | 0.8750 | 0.0264 | 3 |
| 25 | 59 | 61 | 0.9672 | 0.9541 | 1.0345 | 0.8737 | 0.0268 | 3 |
| 26 | 62 | 65 | 0.9538 | 0.9541 | 1.0320 | 0.8762 | 0.0260 | 3 |
| 27 | 45 | 50 | 0.9000 | 0.9541 | 1.0429 | 0.8653 | 0.0296 | 3 |
| 3-Sep-15 | 62 | 63 | 0.9841 | 0.9541 | 1.0332 | 0.8750 | 0.0264 | 3 |
| 4 | 45 | 50 | 0.9000 | 0.9541 | 1.0429 | 0.8653 | 0.0296 | 3 |
| 10 | 55 | 55 | 1.0000 | 0.9541 | 1.0388 | 0.8694 | 0.0282 | 3 |
| 11 | 46 | 46 | 1.0000 | 0.9541 | 1.0467 | 0.8615 | 0.0309 | 3 |
| 12 | 61 | 61 | 1.0000 | 0.9541 | 1.0345 | 0.8737 | 0.0268 | 3 |
| 14 | 57 | 57 | 1.0000 | 0.9541 | 1.0373 | 0.8709 | 0.0277 | 3 |
| 17 | 43 | 57 | 0.7544 | 0.9541 | 1.0373 | 0.8709 | 0.0277 | 3 |
| 18 | 64 | 70 | 0.9143 | 0.9541 | 1.0291 | 0.8791 | 0.0250 | 3 |
| 19 | 66 | 71 | 0.9296 | 0.9541 | 1.0286 | 0.8796 | 0.0248 | 3 |
| 21 | 55 | 61 | 0.9016 | 0.9541 | 1.0345 | 0.8737 | 0.0268 | 3 |
| 22 | 55 | 57 | 0.9649 | 0.9541 | 1.0373 | 0.8709 | 0.0277 | 3 |
| 28-Sep | 53 | 58 | 0.9138 | 0.9541 | 1.0365 | 0.8717 | 0.0275 | 3 |
| 29 | 60 | 60 | 1.0000 | 0.9541 | 1.0351 | 0.8731 | 0.0270 | 3 |
| 30 | 35 | 41 | 0.8537 | 0.9541 | 1.0521 | 0.8561 | 0.0327 | 3 |
| 2746 |  | $2878 \quad 0.9541$ |  |  |  |  |  |  |

$$
\begin{aligned}
& \begin{array}{l}
\bar{p}=\frac{2746}{2878} \\
\\
=0.9541 \\
U C L_{p}= \\
\quad=1.0388 \\
\begin{aligned}
L C L_{p} & =0.9541+3 \sqrt{\frac{0.9541(1-0.9541)}{55}} \\
\quad & =0.8694
\end{aligned}
\end{array} . \begin{aligned}
\frac{0.9541(1-0.9541)}{55} \\
\end{aligned}
\end{aligned}
$$



Figure 4.9: Control Chart for Quality in Shift A

### 4.4.1.3.2 Shift B

Figure 4.10 shows the quality control chart for Shift B and constructed to find the percentage of quality pattern. Average value is 0.9748 , UCL and LCL value is varying because the n value is variable.


Figure 4.10: Control Chart for Quality in Shift B

Referring to figure 4.9 and figure 4.10 , the process is out of control because there are points exceeding the control limit. However, point below the lower control limit are investigated and studied to help to increase the percentage in the future.

The assignable cause responsible for the condition indicated that daily mechanical problems in this line, including machine breakdown and process quality problems.

### 4.4.1.4 OEE

### 4.4.1.4.1 OEE shift A

Figure 4.11 shows the existing OEE in A shift compare with world class OEE. As it shown, it shows that there is a assignable cause in the control chart.


Figure 4.11: Control Chart for OEE Percentage in A Shift

### 4.4.1.4.2 OEE shift B

Figure 4.12 shows the existing OEE in B shift compare with world class OEE. As it shown, it shows that there is a assignable cause in the control chart.


Figure 4.12: Control Chart for OEE Percentage in B Shift

### 4.4.1.5 Detailed explanation of point of out of control in control charts

### 4.4.1.5.1 Availability Factor

Based on Figure 4.5, it is noted that on date July $27^{\text {th }}$ the availability percentage falls below the lower control limit of $97.78 \%$. Besides, it also noted that on date August $10^{\text {th }}, 17^{\text {th }}$, and $25^{\text {th }}$, the availability percentage falls below lower control limit of $97.78 \%$. Similarly, it also noted that on date September $4^{\text {th }}$ and $29^{\text {th }}$ with availability percentage falls below lower limit of $97.86 \%$ and $97.78 \%$. Although high percentage is preferable, the process aims to achieve a stable pattern. Therefore, the points are investigated before they are eliminated.

Based on figure 4.6, it is noted that on date September $17^{\text {th }}$ and $28^{\text {th }}$ the availability percentage falls below the lower control limit of $99.00 \%$.

Based on the observation there is machine breakdown due to line stoppage reduction. Item to be countermeasure was door manipulator and air leak tester. First equipment is door manipulator than can't push up and down, this factor causes by hose leaking. Second equipment is air leak tester indicate a NG reading this phenomena is causes by hose bend. Countermeasure that can take action is to check, repair and properly layout the air hose of the equipment.

### 4.4.1.5.2 Performance Factor

Based on Figure 4.7, it is noted that on date July 3 rd $9^{\text {th }}, 10^{\text {th }}$, and $11^{\text {th }}$ with performance percentage falls below control limits of $80.22 \%$. On July $6^{\text {th }}$, and 8th with performance percentage falls upper control limits of $90.02 \%$. Although high percentage is preferable, the process aims to achieve a stable pattern. Besides, it is also noted that on date August $4^{\text {th }}, 15^{\text {th }}, 18^{\text {th }}, 19^{\text {th }}$, and $27^{\text {th }}$ with performance percentage falls below the lower control limit of $80.50 \%, 80.22 \%, 80.46 \%, 80.50 \%$ and $80.22 \%$. on $3^{\text {rd }}, 7^{\text {th }}$, $13^{\text {th }}, 17^{\text {th }}, 21^{\text {th }}, 22^{\text {th }}, 24^{\text {th }}, 25^{\text {th }}$, and $27^{\text {th }}$ with performance percentage falls above the upper control limit of $89.74 \%, 90.02 \%, 90.02 \%, 90.24 \%, 89.74 \%, 90.02 \%$,
$90.02 \%, 90.23$ and $90.02 \%$. Similarly, on September $4^{\text {th }}, 11^{\text {th }}$, and $30^{\text {th }}$ with performance percentage falls below the lower control limit of $80.41 \%, 80.07 \%$ and $80.21 \%$. Therefore, the points are investigated before they are eliminated.

Similarly, based on Figure 4.8, it is noted that on date July $6^{\text {th }}, 7^{\text {th }}, 8^{\text {th }}$, with performance percentage falls above the upper control limit of $87.65 \%$. On July $10^{\text {th }}$, $11^{\text {th }}, 23$ th, $24^{\text {th }}, 28^{\text {th }}$ and $29^{\text {th }}$ with performance percentage fall below the lower control limit of $77.15 \%$. Besides, it is also noted that on date August $3^{\text {rd }}, 7^{\text {th }}, 13^{\text {th }}, 14^{\text {th }}, 20^{\text {th }}, 24^{\text {th }}$, $25^{\text {th }}$ and $26^{\text {th }}$ the performance percentage respectively falls above the upper control limit of $87.34 \%, 87.57 \%, 87.65 \%, 87.34 \%, 87.65 \%, 87.65 \%, 87.65 \%$ and $87.6555 \%$. On date August $10^{\text {th }}, 15^{\text {th }}, 17^{\text {th }}, 18^{\text {th }}$ and $19^{\text {th }}$ with performance percentage falls below the lower control limit of $77.46 \%, 77.15 \%, 77.46 \%$ and $77.46 \%$. on September $4^{\text {th }}, 7^{\text {th }}$, $12^{\text {th }}, 14^{\text {th }}, 19^{\text {th }}$ and $30^{\text {th }}$ with performance percentage falls above the upper control limit of $87.65 \%, 87.57 \%, 87.65 \%, 87.34 \%, 87.65 \%$ and $87.65 \%$. on September $1^{\text {st }}, 3^{\text {rd }}, 9^{\text {th }}$, $10^{\text {th }}, 11^{\text {th }}, 15^{\text {th }}, 18^{\text {th }}$ and $29^{\text {th }}$ with performance percentage falls below the lower control limit of $77.15 \%, 77.46 \%, 77.51 \%, 77.46 \%, 77.64 \%, 77.15 \%, 77.15 \%$, and $77.15 \%$.Therefore, the points are also investigated before they are eliminated.

Based on observation, there is problem with operator that has a bad attendance, factor of this situation is problem among operator. Secondly, miscommunication between operator and leader. Most of the operator is from outside from Malaysia, and it takes more than 3 months to teach them the language. Thirdly, some operator has to attend a training to improve their knowledge. This situation can be decrease by making a schedule to attend a training to prevent the operator missing from their workstation.

### 4.4.1.5.3 Quality Factor

Based on Figure 4.9, it is noted that on date $17^{\text {th }}$ and $30^{\text {th }}$ with quality percentage falls below the lower control limit of $87.06 \%$ and $85.57 \%$.. Although high percentage is preferable, the process aims to achieve a stable pattern. Similar process pattern is also observed in Figure 4.10 on date September 28th with quality percentage falls below the
lower control limit of $94.78 \%$. These out-of-control points are investigated before they are eliminated.

Based on observation, there is downtime loss happen. This factor occur when there is machine breakdown and process quality issues. This issue happen when new operator operate the machine without supervised from leader. This issue can be reduced by attend a training to handle the machine.

### 4.4.2 $\quad 1^{\text {st }}$ Revised control chart

When a process is out of control, the assignable cause responsible for the condition must be found. Remove any points from the calculations that have been corrected. Revise the control charts with the remaining points. A new average can be obtained and set as a target value to make an improvement which can reduce downtime that affect OEE value.

Figure below shows the revised control chart for Chassis Assembly line in each shift and constructed to find average percentage in the process. The mean value in control chart is used as a value to propose a new target each OEE factor.

### 4.4.2.1 Availability

### 4.4.2.1.1 Shift A

Table 4.7 shows the data after revising the out of control point from the existing condition. Below shows the establish revised central line and control limits. Figure 4.13 shows the first revision of availability control chart for Shift A and constructed to find the percentage of availability pattern. Average value is 0.9966 , while UCL and LCL value is vary based on their n number.

Table 4.7: revised control chart data for Availability in shift A

| DAY | OPERATION TIME | PLANNED PRODUCTION TIME | AVAILABILITY (p) | CENTER (P-BAR) | UCL | LCL | SIGMA P BAR | 2 |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-Jul-15 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 2 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 3 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 6 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 7 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 8 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 9 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 10 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 11 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 13 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 14 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 22 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 23 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 24 | 472 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 28 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 29 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 30 | 465 | 474 | 0.98 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 3-Aug-15 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 | 0.0025 | 3.0000 |
| 4 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 | 0.0025 | 3.0000 |
| 5 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 | 0.0025 | 3.0000 |
| 6 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 | 0.0025 | 3.0000 |
| 7 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 13 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 15 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 18 | 525 | 534 | 0.98 | 0.9966 | 1.0042 | 0.9890 | 0.0025 | 3.0000 |
| 19 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 | 0.0025 | 3.0000 |
| 20 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 21 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 | 0.0025 | 3.0000 |
| 22 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 24 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 26 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 27 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 3-Sep-15 | 523 | 534 | 0.98 | 0.9966 | 1.0042 | 0.9890 | 0.0025 | 3.0000 |
| 10 | 466 | 474 | 0.98 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 11 | 447 | 456 | 0.98 | 0.9966 | 1.0048 | 0.9884 | 0.0027 | 3.0000 |
| 12 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 14 | 479 | 484 | 0.99 | 0.9966 | 1.0045 | 0.9887 | 0.0026 | 3.0000 |
| 17 | 471 | 474 | 0.99 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 18 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 | 0.0025 | 3.0000 |
| 19 | 526 | 534 | 0.99 | 0.9966 | 1.0042 | 0.9890 | 0.0025 | 3.0000 |
| 21 | 475 | 479 | 0.99 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 22 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 28-Sep | 470 | 474 | 0.99 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
| 30 | 472 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | 0.0027 | 3.0000 |
|  | 2137 | 214530.9966 |  |  |  |  |  |  |

$$
\begin{aligned}
\bar{p} & =\frac{21379}{21453} \\
& =0.9966
\end{aligned}
$$

$$
\begin{aligned}
U C L_{p} & =0.9966+3 \sqrt{\frac{0.9966(1-0.9966)}{474}} \\
& =1.0046 \\
L C L_{p} & =0.9966-3 \sqrt{\frac{0.9966(1-0.9966)}{474}} \\
& =0.9886
\end{aligned}
$$



Figure 4.13: Control Chart for Revised Availability in Shift A

### 4.4.2.1.2 Shift B

Figure 4.14, shows the first revision of availability control chart for Shift B and constructed to find the percentage of availability pattern. Average value is 1.000 , while UCL and LCL value is varying based on their n number.


Figure 4.14: Control Chart for Revised Availability in Shift B

Apparently, the average value of availability percentage has increased after revising. Therefore, it is highly recommended to eliminate the assignable causes in the
process in order to achieve the OEE value. Some of the point still out of control, however, this control chart can be revised again in order to achieve a stable level of process.

### 4.4.2.2 Performance

### 4.4.2.2.1 Shift A

Table 4.8 shows the data after revising the out of control point from the existing condition. Below shows the establish revised central line and control limits. Figure 4.15, shows the first revision of performance control chart for Shift A and constructed to find the percentage of performance pattern. Average value is 0.8490 , UCL and LCL value is varying because the n value is variable.

Table 4.8: revised control chart data for Performance in shift A


$$
\bar{p}=\frac{21379}{21453}
$$

$$
=0.9966
$$

$$
\begin{aligned}
U C L_{p} & =0.9966+3 \sqrt{\frac{0.9966(1-0.9966)}{474}} \\
& =1.0046
\end{aligned}
$$

$$
\begin{aligned}
L C L_{p} & =0.9966-3 \sqrt{\frac{0.9966(1-0.9966)}{474}} \\
& =0.9886
\end{aligned}
$$



Figure 4.15: Control Chart for Performance in Shift A

### 4.4.2.2.2 Shift B

Figure 4.16, shows the first revision of performance control chart for Shift B and constructed to find the percentage of performance pattern. Average value is 0.8287 , UCL and LCL value is varying because the n value is variable.


Figure 4.16: Control Chart Revised for Performance in Shift B

Apparently, the average value of performance percentage has increased after revising. Therefore, it is highly recommended to eliminate the assignable causes in the process in order to achieve the OEE value.

### 4.4.2.3 Quality

### 4.4.2.3.1 Shift A

Table 4.9 shows the data after revising the out of control point from the existing condition. Below shows the establish revised central line and control limits. Figure 4.17 shows the first revision of quality control chart for Shift A and constructed to find the percentage of quality pattern. Average value is 0.9597 , UCL and LCL value is varying because the n value is variable.

Table 4.9: revised control chart data for Quality in shift A

| DAY | OK PRODUCT PER SHIFT (np) | TOTAL OUTPUT PER SHIFT ( n ) | QUALITY (p) | CENTER (P-BAR) | UCL | LCL | SIGMA P-BAR | Z |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-Jul-15 | 53 | 55 | 0.9636 | 0.9597 | 1.0393 | 0.8801 | 0.0265 | 3 |
| 2 | 54 | 55 | 0.9818 | 0.9597 | 1.0393 | 0.8801 | 0.0265 | 3 |
| 3 | 50 | 50 | 1.0000 | 0.9597 | 1.0431 | 0.8763 | 0.0278 | 3 |
| 6 | 58 | 60 | 0.9667 | 0.9597 | 1.0359 | 0.8835 | 0.0254 | 3 |
| 7 | 56 | 57 | 0.9825 | 0.9597 | 1.0378 | 0.8816 | 0.0260 | 3 |
| 8 | 57 | 63 | 0.9048 | 0.9597 | 1.0340 | 0.8854 | 0.0248 | 3 |
| 9 | 47 | 50 | 0.9400 | 0.9597 | 1.0431 | 0.8763 | 0.0278 | 3 |
| 10 | 48 | 50 | 0.9600 | 0.9597 | 1.0431 | 0.8763 | 0.0278 | 3 |
| 11 | 50 | 52 | 0.9615 | 0.9597 | 1.0415 | 0.8779 | 0.0273 | 3 |
| 13 | 53 | 53 | 1.0000 | 0.9597 | 1.0407 | 0.8787 | 0.0270 | 3 |
| 14 | 54 | 55 | 0.9818 | 0.9597 | 1.0393 | 0.8801 | 0.0265 | 3 |
| 22 | 55 | 57 | 0.9649 | 0.9597 | 1.0378 | 0.8816 | 0.0260 | 3 |
| 23 | 54 | 56 | 0.9643 | 0.9597 | 1.0385 | 0.8809 | 0.0263 | 3 |
| 24 | 55 | 56 | 0.9821 | 0.9597 | 1.0385 | 0.8809 | 0.0263 | 3 |
| 27 | 52 | 52 | 1.0000 | 0.9597 | 1.0415 | 0.8779 | 0.0273 | 3 |
| 28 | 56 | 56 | 1.0000 | 0.9597 | 1.0385 | 0.8809 | 0.0263 | 3 |
| 29 | 54 | 56 | 0.9643 | 0.9597 | 1.0385 | 0.8809 | 0.0263 | 3 |
| 30 | 54 | 55 | 0.9818 | 0.9597 | 1.0393 | 0.8801 | 0.0265 | 3 |
| 3-Aug-15 | 68 | 70 | 0.9714 | 0.9597 | 1.0302 | 0.8892 | 0.0235 | 3 |
| 4 | 57 | 58 | 0.9828 | 0.9597 | 1.0372 | 0.8822 | 0.0258 | 3 |
| 5 | 64 | 66 | 0.9697 | 0.9597 | 1.0323 | 0.8871 | 0.0242 | 3 |
| 6 | 61 | 62 | 0.9839 | 0.9597 | 1.0346 | 0.8848 | 0.0250 | 3 |
| 7 | 58 | 62 | 0.9355 | 0.9597 | 1.0346 | 0.8848 | 0.0250 | 3 |
| 10 | 49 | 52 | 0.9423 | 0.9597 | 1.0415 | 0.8779 | 0.0273 | 3 |
| 13 | 60 | 64 | 0.9375 | 0.9597 | 1.0334 | 0.8860 | 0.0246 | 3 |
| 15 | 45 | 50 | 0.9000 | 0.9597 | 1.0431 | 0.8763 | 0.0278 | 3 |
| 17 | 52 | 58 | 0.8966 | 0.9597 | 1.0372 | 0.8822 | 0.0258 | 3 |
| 18 | 48 | 50 | 0.9600 | 0.9597 | 1.0431 | 0.8763 | 0.0278 | 3 |
| 19 | 53 | 56 | 0.9464 | 0.9597 | 1.0385 | 0.8809 | 0.0263 | 3 |
| 20 | 57 | 60 | 0.9500 | 0.9597 | 1.0359 | 0.8835 | 0.0254 | 3 |
| 21 | 66 | 70 | 0.9429 | 0.9597 | 1.0302 | 0.8892 | 0.0235 | 3 |
| 22 | 64 | 66 | 0.9697 | 0.9597 | 1.0323 | 0.8871 | 0.0242 | 3 |
| 24 | 61 | 63 | 0.9683 | 0.9597 | 1.0340 | 0.8854 | 0.0248 | 3 |
| 25 | 59 | 61 | 0.9672 | 0.9597 | 1.0352 | 0.8842 | 0.0252 | 3 |
| 26 | 62 | 65 | 0.9538 | 0.9597 | 1.0329 | 0.8865 | 0.0244 | 3 |
| 27 | 45 | 50 | 0.9000 | 0.9597 | 1.0431 | 0.8763 | 0.0278 | 3 |
| 3-Sep-15 | 62 | 63 | 0.9841 | 0.9597 | 1.0340 | 0.8854 | 0.0248 | 3 |
| 4 | 45 | 50 | 0.9000 | 0.9597 | 1.0431 | 0.8763 | 0.0278 | 3 |
| 10 | 55 | 55 | 1.0000 | 0.9597 | 1.0393 | 0.8801 | 0.0265 | 3 |
| 11 | 46 | 46 | 1.0000 | 0.9597 | 1.0467 | 0.8727 | 0.0290 | 3 |
| 12 | 61 | 61 | 1.0000 | 0.9597 | 1.0352 | 0.8842 | 0.0252 | 3 |
| 14 | 57 | 57 | 1.0000 | 0.9597 | 1.0378 | 0.8816 | 0.0260 | 3 |
| 18 | 64 | 70 | 0.9143 | 0.9597 | 1.0302 | 0.8892 | 0.0235 | 3 |
| 19 | 66 | 71 | 0.9296 | 0.9597 | 1.0297 | 0.8897 | 0.0233 | 3 |
| 21 | 55 | 61 | 0.9016 | 0.9597 | 1.0352 | 0.8842 | 0.0252 | 3 |
| 22 | 55 | 57 | 0.9649 | 0.9597 | 1.0378 | 0.8816 | 0.0260 | 3 |
| 28-Sep | 53 | 58 | 0.9138 | 0.9597 | 1.0372 | 0.8822 | 0.0258 | 3 |
| 29 | 60 | 60 | 1.0000 | 0.9597 | 1.0359 | 0.8835 | 0.0254 | 3 |

$$
\begin{aligned}
& \begin{array}{l}
\bar{p}=\frac{2668}{2780} \\
\\
=0.9597 \\
U C L_{p}= \\
\quad=1.0393 \\
\begin{aligned}
L C L_{p} & =0.9597+3 \sqrt{\frac{0.9597(1-0.9597)}{55}} \\
& =0.8801
\end{aligned}
\end{array} . \begin{aligned}
\frac{0.9597(1-0.9597)}{55} \\
\end{aligned}
\end{aligned}
$$



Figure 4.17: Control Chart Revised for Quality in Shift A

### 4.4.2.3.2 Shift B

Figure 4.18 shows the first revision of quality control chart for Shift B and constructed to find the percentage of quality pattern. Average value is 0.9777 , UCL and LCL value is varying because the n value is variable.


Figure 4.18: Control Chart Revised for Quality in Shift B

Apparently, the average value of quality percentage has increased after revising. Therefore, it is highly recommended to eliminate the assignable causes in the process in order to achieve the OEE value.

### 4.4.3 $\quad 2^{\text {nd }}$ Revised Control Chart

Figure below shows the $2^{\text {nd }}$ revised control chart for Chassis Assembly line in each shift and constructed by eliminate the assignable cause point to get a stable control chart. The mean value in control chart is used as a value to propose a new target each OEE factor.

### 4.4.3.1 Availability

### 4.4.3.1.1 Shift A

Table 4.10 shows the data after eliminated the below point of central line to get a stable control chart. Below shows the establish central line and control limits for $2^{\text {nd }}$
revised. Figure 4.19 shows the second revision of availability control chart for Shift A and constructed to find the percentage of availability pattern. Average value is 0.99 , UCL and LCL value is varying because the n value is variable.

Table 4.10: 2nd revised control chart data for Availability in shift A

| DAY | OPERATION TIME | PLANNED PRODUCTION TIME | AVAILABILITY (p) | CENTER (P-BAR) | UCL | LCL | SIGMA P BAR | Z |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1-Jul-15 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 2 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 3 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 6 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 7 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 8 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 9 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 10 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 11 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 13 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 14 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 22 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 23 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 28 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 29 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 3-Aug-15 | 534 | 534 | 1.00 | 0.9900 | 1.0029 | 0.9771 | 0.0043 | 3.0000 |
| 4 | 534 | 534 | 1.00 | 0.9900 | 1.0029 | 0.9771 | 0.0043 | 3.0000 |
| 5 | 534 | 534 | 1.00 | 0.9900 | 1.0029 | 0.9771 | 0.0043 | 3.0000 |
| 6 | 534 | 534 | 1.00 | 0.9900 | 1.0029 | 0.9771 | 0.0043 | 3.0000 |
| 7 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 13 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 15 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 19 | 534 | 534 | 1.00 | 0.9900 | 1.0029 | 0.9771 | 0.0043 | 3.0000 |
| 20 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 21 | 534 | 534 | 1.00 | 0.9900 | 1.0029 | 0.9771 | 0.0043 | 3.0000 |
| 22 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 24 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 26 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 27 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 12 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
| 18 | 534 | 534 | 1.00 | 0.9900 | 1.0029 | 0.9771 | 0.0043 | 3.0000 |
| 22 | 474 | 474 | 1.00 | 0.9900 | 1.0037 | 0.9763 | 0.0046 | 3.0000 |
|  | 1558 | 15588 | 1.0000 |  |  |  |  |  |

$$
\begin{aligned}
\bar{p} & =\frac{15588}{15588} \\
& =1.000
\end{aligned}
$$

$$
U C L_{p}=1.000+3 \sqrt{\frac{1.000(1-1.000)}{474}}
$$

$$
=1.0037
$$

$$
\begin{aligned}
L C L_{p} & =1.000-3 \sqrt{\frac{1.000(1-1.000)}{474}} \\
& =0.9763
\end{aligned}
$$



Figure 4.19: Control Chart $2^{\text {nd }}$ Revised for Availability in Shift A

### 4.4.3.1.2 Shift B

Figure 4.20 shows the second revision of availability control chart for Shift B and constructed to find the percentage of availability pattern. Average value is 0.99 , UCL and LCL value is varying because the n value is variable.


Figure 4.20: Control Chart $2^{\text {nd }}$ Revised for Availability in Shift B

### 4.4.3.2 Performance

### 4.4.3.2.1 Shift A

Table 4.11 shows the data after eliminated the below point of central line to get a stable control chart. Below shows the establish central line and control limits for $2^{\text {nd }}$ revised. Figure 4.21 shows the second revision of performance control chart for Shift A and constructed to find the percentage of performance pattern. Average value is 0.8611 , UCL and LCL value is varying because the n value is variable.

Table 4.11: 2nd revised control chart data for Performance in shift A

| DAY | NET OPERATION TIME (np) | OPERATION <br> TIME (n) | PERFORMANCE <br> (p) | CENTER P BAR | UCL | LCL | SIGMA P BAR | Z |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 7 | 409 | 474 | 0.863 | 0.8611 | 0.9088 | 0.8134 | 0.0159 | 3 |
| 22 | 409 | 474 | 0.863 | 0.8611 | 0.9088 | 0.8134 | 0.0159 | 3 |
| 23 | 402 | 474 | 0.848 | 0.8611 | 0.9088 | 0.8134 | 0.0159 | 3 |
| 24 | 402 | 472 | 0.852 | 0.8611 | 0.9089 | 0.8133 | 0.0159 | 3 |
| 28 | 402 | 474 | 0.848 | 0.8611 | 0.9088 | 0.8134 | 0.0159 | 3 |
| 29 | 402 | 474 | 0.848 | 0.8611 | 0.9088 | 0.8134 | 0.0159 | 3 |
| 30 | 395 | 465 | 0.849 | 0.8611 | 0.9092 | 0.8130 | 0.0160 | 3 |
| 5 | 474 | 534 | 0.888 | 0.8611 | 0.9060 | 0.8162 | 0.0150 | 3 |
| 20 | 422 | 474 | 0.890 | 0.8611 | 0.9088 | 0.8134 | 0.0159 | 3 |
| 3-Sep-15 | 452 | 523 | 0.864 | 0.8611 | 0.9065 | 0.8157 | 0.0151 | 3 |
| 10 | 395 | 466 | 0.848 | 0.8611 | 0.9092 | 0.8130 | 0.0160 | 3 |
| 14 | 409 | 479 | 0.854 | 0.8611 | 0.9085 | 0.8137 | 0.0158 | 3 |
| 17 | 401 | 471 | 0.851 | 0.8611 | 0.9089 | 0.8133 | 0.0159 | 3 |
| 28-Sep | 416 | 470 | 0.885 | 0.8611 | 0.9090 | 0.8132 | 0.0160 | 3 |
|  | 5790 | 6724 | 0.8611 |  |  |  |  |  |

$$
\begin{aligned}
\bar{p} & =\frac{5790}{6724} \\
& =0.8611
\end{aligned}
$$

$$
U C L_{p}=0.8611+3 \sqrt{\frac{0.8611(1-0.8611)}{474}}
$$

$$
=0.9088
$$

$$
L C L_{p}=0.8611-3 \sqrt{\frac{0.8611(1-0.8611)}{474}}
$$

$$
=0.8134
$$



Figure 4.21: Control Chart $2^{\text {nd }}$ Revised for Performance in Shift A

### 4.4.2.2 Shift B

Figure 4.22 shows the second revision of performance control chart for Shift B and constructed to find the percentage of performance pattern. Average value is 0.9497 , UCL and LCL value is varying because the $n$ value is variable.


Figure 4.22: Control Chart $2^{\text {nd }}$ Revised for Performance in Shift B

### 4.4.3.3 Quality

### 4.4.3.3.1 Shift A

Table 4.12 shows the data after eliminated the below point of central line to get a stable control chart. Below shows the establish central line and control limits for $2^{\text {nd }}$ revised. Figure 4.23 shows the second revision of quality control chart for Shift A and constructed to find the percentage of quality pattern. Average value is 0.9797 , UCL and LCL value is varying because the n value is variable.

Table 4.12: 2nd revised control chart data for Quality in shift A

$\bar{p}=\frac{1734}{1770}$

$$
=0.9797
$$

$$
\begin{aligned}
U C L_{p} & =0.9797+3 \sqrt{\frac{0.9797(1-0.9797)}{55}} \\
& =1.0367
\end{aligned}
$$

$$
L C L_{p}=0.9797-3 \sqrt{\frac{0.9797(1-0.9797)}{55}}
$$

$$
=0.9227
$$



Figure 4.23: Control Chart $2^{\text {nd }}$ Revised for Quality in Shift A

### 4.4.3.3.2 Shift B

Figure 4.24 shows the second revision of quality control chart for Shift B and constructed to find the percentage of quality pattern. Average value is 0.9922 , UCL and LCL value is varying because the $n$ value is variable.


Figure 4.24: Control Chart $2^{\text {nd }}$ Revised for Quality in Shift B

### 4.4.4 Comparisons between the existing OEE with 1st and 2nd revised OEE and world class OEE in each shift

Figure 4.25 shown the comparison of existing, $1^{\text {st }}$ revised and $2^{\text {nd }}$ revised OEE with world class OEE.OEE value improved by $0.0089 \%$ after $1^{\text {st }}$ revised with existing OEE value. $2^{\text {nd }}$ revised improved by $0.0458 \%$ with existing OEE value.


Figure 4.25: the comparisons between the existing OEE with 1st and 2nd revised OEE and world class OEE in each shift

### 4.4.5 Pareto diagram

Through production data, the downtime rate is analyzed and categorized into 8 types of causes. Table 4.13 below shows the downtime causes including machine breakdown (A), logistics (B), waiting hanger (C), process quality issue (D), operator downstation (E), others (F), and vehicle quality issue (G).

Table 4.13: Downtime Causes Calculation

| issue | frequent | cumulative frequency | cumulative \% |
| :--- | :--- | :--- | :--- |
| machine breakdown | 896 | 896 | 59.46 |
| logistics | 222 | 1118 | 74.19 |
| waiting hanger | 217 | 1335 | 88.59 |
| process quality issue | 95 | 1430 | 94.89 |
| operator downstation | 32 | 1462 | 97.01 |
| others | 28 | 1490 | 98.87 |
| vehicle quality issue | 17 | 1507 | 100.00 |

The Pareto Chart shows the relative frequency of issues in rank-order. Figure 4.26 shows is a Pareto chart of issues due to line stoppage in Chassis-Final Assembly line. It shows that machine breakdown has the higher frequency issues on line stoppage.


Figure 4.26: Pareto Chart

### 4.4.6 Ishikawa Diagram

Ishikawa diagram is used to identify the root cause of high downtime losses. Figure 4.27 shows the Ishikawa diagram to analyze why downtime rate is higher. There are five major possibilities that lead to this problem. There are machine, man, method, materials, and environment.


Figure 4.27: Ishikawa Diagram

### 4.4.6.1 Man

- Bad attendance

This factor mostly happens to Malaysian citizen, they came to work not every day. They left the workstation without support operator and this cause machine cannot run properly. This is indicated at $1^{\text {st }}$ July 2015 for 55 times.

### 4.4.6.2 Method

- Low skilled operator

This happen only to new operator. They handling the machine without supervised from the leader and cannot understand the language used. This situation can be eliminate by sent them to training in the company.

### 4.4.6.3 Machine

- Frequent machine breakdown

Door manipulator cannot push up and down .This failure cause by hose leaking for about 12 times. This factor can be control by check, repair and properly layout air hose in the line. Air leak tester indicate NG reading. This failure cause by hose bend for about 9 times. This factor can be reduced by check, repair and properly layout air hose in the line. This factor indicated on 11 July 2015 for 62 times.

### 4.4.6.4 Material

- Logistics issue

Order from customer changing, and the changeover process delaying the process flow in the Chassis final Assembly Line. It also connected to logistics department to supply the parts from logistics department. This indicated on $1^{\text {st }}$ July 2015 for 63 times.

### 4.4.7 Improvement using 5W1H Method

From the Table 4.6 above, the problems are identified. 5 W 1 H method was used to improve problems happened Chassis Final Assembly Line. The information are gathered through What, Why, When, Who, Where and How question. For the first 5W
is used to specify more details on the root cause while 1 H is used to propose a solution to eliminate or reduce the problem. It will be shown in Table 4.7.

Table 4.14: 5W1H Method

| Question | Answer |
| :--- | :--- |
| Problem | Downtime loss |
| What? | Frequent machine breakdown due to line stoppages |
| Who? | Maintenance teams and operator |
| When? | Almost everyday <br> Where?Fhassis-Final Assembly Line Assembly Line because there is no proper schedule for <br> preventive maintenance. TCMA practice reactive maintenance <br> where they only fix the machine when breakdown happen. |
| Why? | Implementation and monitor of Planned Scheduled Maintenance for <br> the machines to reduce the downtime rate in Chassis-Final Assembly <br> Line so that the parts and supplies can be ready to go. |
| How? | There |

## CHAPTER 5

## CONCLUSION AND RECOMMENDATION

### 5.1 INTRODUCTION

In this chapter, the conclusion will be based on research done in previous chapters. There are also a few recommendations given to strengthen and improve the performance of the production system in TCMA Chassis-Final Assembly Line .

### 5.2 CONCLUSION

As a conclusion, the value of OEE can be measured by finding the three elements of OEE itself; availability, performance and quality. These three elements must be balance with each other in order to get stable value of OEE. In this study, Chassis-Final Assembly Line section was chosen because the higher downtime rate and solution is needed to solve the problem. Results from the existing graph collected from company was out of control and below World Class OEE benchmarking, because there are some point that out of control limit and there is out of control patterns exist.

Analyzing was done by revised the existing control chart by eliminate the point that out of control by calculating the existing OEE value to see if there any improvement. OEE value could be improved from $80.49 \%$ to $81.21 \%$, and $80.29 \%$ to $81.09 \%$ for A, and B shift respectively. $2^{\text {nd }}$ revised was done by eliminating the point which below control limit and taking the best point between central limit and upper control limit and calculating based on the best point and OEE value can improved from $81.21 \%$ to $84.35 \%$, and $81.09 \%$ to $84.31 \%$, for A, and B shift respectively. This shown that $2^{\text {nd }}$ revised OEE value nearly to World Class Ranking about $0.65 \%$ and $0.69 \%$ for
shift A and B respectively. This is possible to improve the OEE value by eliminating the problem occurred on Pareto Diagram such as machine breakdown, logistics issues and waiting hanger.. Based on the problem occurred, there are causes affecting the problem in Ishikawa Diagram such as Bad attendance, low skilled worker and frequent machine breakdown. From this problem and causes it was proposed in 5W1H method to find the solution as shown in below.

### 5.3 RECOMMENDATIONS

There is always space for improvement for every completed studies and research. As in the future, there are several recommendations to be proposed for making an improvement. An improvement can be proposed from 5 W 1 H method that has been done in previous chapter. To eliminate the problem occurred in Chassis final Assembly line, TCMA should implemented and monitor of Planned Scheduled Maintenance to decrease the downtime rate, so that the part and supplies can be ready to go in order to prevent zero spare parts of machine components. Scheduled maintenance tasks should be performed based on predicted and measured failure rates in previous history. Consequently, it will reduce the instances of unplanned downtime and enables most maintenance to be planned for times when equipment is not scheduled for production. It will also reduce inventory through better control of wear-prone and failure-prone parts.

The suggested future OEE value for this company is $84.35 \%$, and $84.31 \%$ for, A, and B shift respectively. Since these values are calculated based on the existing value of OEE elements in this company, hence it means that it is a possible for them to achieve this target OEE in the future if suggestions and methods analyzed are implemented for continuous improvement.

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## APPENDIX A

## A1: GANTT CHART

|  | FYP 1 | SEPT |  |  | OCT |  |  |  |  | NOV |  |  |  | DEC |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Project Activities | W1 | W2 | W3 | W4 | W5 | W6 | W7 | W8 | W9 | W10 | W11 | W12 | W13 | W14 |
| 1 | Identify suitable company for project |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | Study the current maintenance system |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | Verify the project title |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | Drafting Chapter 1: Introduction |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | Finalize and Submit draft Chapter 1 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | Drafting Chapter 2: Literature Review |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | Finalize and Submit draft Chapter 2 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | Verify suitable selection method |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 | Drafting Chapter 3: Methodology |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 10 | Finalize and Submit Draft Chapter 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 11 | Compile and Submit Chapter 1, 2, and 3 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 12 | Prepare for final presentation |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 13 | FYP 1 Final Presentation |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

## A2: GANTT CHART (Continued)

|  | FYP 2 | FEB | MAR |  |  |  | APR |  |  |  |  | MAY |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. | Project Activities | W1 | W2 | W3 | W4 | W5 | W6 | W7 | W8 | W9 | W10 | W11 | W12 | W13 | W14 |
| 1 | Data collection and analyze data |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 2 | Drafting Chapter 4: Results and Discussions |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 3 | Finalize and Submit Draft Chapter 4 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 4 | Drafting Chapter 5: Conclusions and Recommendations |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 5 | Finalize and Submit Draft Chapter 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 6 | Prepare Poster |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 7 | Poster Presentation |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 8 | Compiling Chapter $1,2,3,4$, and 5 |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 9 | Submit Final Report |  |  |  |  |  |  |  |  |  |  |  |  |  |  |

Remarks: $\square$

## APPENDIX B

## B1: Chassis-Final Assembly Line Production Data for July 2015



Shift B


## B2: Chassis-Final Assembly Line Production Data for August 2015



Shift B

| No. Chassis-FINAL LINE | 1 | 2 | ${ }^{3}$ | ${ }_{7}$ | 5 | 6 | 7 | 8 | 9 |  | 11 | 12 | 13 | 14 | ${ }^{15}$ | 16 | 17 |  | 19 | 20 |  |  |  |  |  |  |  |  | 29 | ${ }^{30}$ | ${ }^{31}$ | Cumul. |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 Planned dommime eer Shit | $\bigcirc$ |  |  |  |  |  |  |  |  |  | 89 | 71 |  |  | ${ }^{71}$ | , |  |  |  |  |  |  |  |  | ${ }^{71}$ | ${ }^{71}$ | ${ }^{71}$ | 0 |  |  | 0 |  |
| ${ }^{2}{ }^{2 A}$ Downtime Loss ${ }^{\text {- Machine brakdown ( }}$ (G) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ${ }_{4}^{0}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\bigcirc$ |
| -Tools /Jg (J) | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |  |  |
| 28 Speed Loss | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |  |
| - Procoss qually issue (Q) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  | ${ }^{3}$ | 0 |  | 0 |  |  | 0 | 0 | 0 | 0 |  |  |  |
| Venicle quality issue (1) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 11 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | ${ }^{27}$ | 0 |  | 0 |  | 0 |  |  |  |  |  |
| Looisics (0) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| PPC (H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 7 | ${ }^{15}$ | ${ }^{15}$ | 0 | 0 | 0 | 0 | 0 |  |
| Chassis jimmed (C) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 6 | ${ }^{75}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 11 | 0 | 18 | 0 | 0 | 0 |  |  |
| Operator domnstation (P) | 0 | 0 | 0 | ${ }^{20}$ | ${ }^{12}$ | 0 | 0 | 0 | 0 | ${ }^{18}$ | 10 | 19 | ${ }^{22}$ | 0 | ${ }^{8}$ | 0 | 0 | 0 | 6 | 0 | ${ }^{28}$ | ${ }^{22}$ | 0 | ${ }^{18}$ | ${ }^{11}$ | 3 | ${ }^{41}$ | 0 | 0 | 0 | 0 |  |
| New operator under training (N) | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 |  |  |  |  |  |  |  |  | 0 | 0 | 0 | 0 | 0 |  |  |  |
| - Bad atendance ( $A$ ) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| - Wating hanger (W) | 0 | 0 | 0 | ${ }^{6}$ | $\stackrel{11}{0}$ | $\bigcirc$ | 0 | 0 | 0 | 3 0 0 | 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | ${ }^{138}$ | $\bigcirc$ | ${ }^{103}$ | $\stackrel{70}{0}$ | ${ }^{26}$ | 5 <br> 0 | $\bigcirc$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | $\frac{0}{0}$ |  |
| 3 Offine Unit per day | 0 | 0 | 2 |  |  | 1 | 3 | 0 | 0 | 2 | 2 | 1 | 2 | 2 |  | , |  | 2 |  |  |  |  |  |  |  |  | 3 |  |  |  |  |  |
| ${ }^{4} 4$ Toial operating hours per Shit | 0 | 0 | 605 | 545 | 605 | 605 | ${ }_{4}^{615}$ | $\bigcirc$ | $\bigcirc$ | ${ }_{6}^{605}$ | ${ }_{\substack{665 \\ 576}}$ | 545 474 | 545 474 | 605 534 | 545 474 | $\bigcirc$ | ¢ 545 | 605 <br> 534 <br> 5 | 605 <br> 534 <br> 5 | 545 474 | ${ }_{6}^{615}$ | 545 <br> 474 | $\bigcirc$ | 545 <br> 474 | 545 <br> 474 | 545 <br> 474 | 545 <br> 444 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 12125 <br> ${ }_{1056}$ <br> 120 |
|  | 0 | 0 | ${ }_{534}$ | ${ }_{474}^{474}$ | ${ }_{534}{ }_{534}$ | ${ }_{534}{ }_{534}$ | ${ }_{489}^{489}$ | 0 | 0 | ${ }_{534}^{534}$ | ${ }_{576}$ | ${ }_{474}^{474}$ | ${ }_{4} 474$ | ${ }_{534}$ | ${ }_{4}^{474}$ | 0 | ${ }_{4}^{474}$ | ${ }_{534} 5$ | ${ }_{534}{ }_{5} 5$ | ${ }_{4}^{474}$ | ${ }_{489}^{489}$ | ${ }_{4} 474$ | 0 | ${ }_{474}^{4}$ | ${ }_{4}^{474}$ | ${ }_{474}^{474}$ | ${ }_{4}^{474}$ | 0 | 0 | 0 | 0 |  |
| 7 Total Output Per Shit | 0 | 0 | 70 | 56 |  |  |  | 0 | 0 | ${ }_{5}^{53}$ | 64 | 71 | 66 |  | 50 | 0 | ${ }^{38}$ | ${ }^{48}$ | ${ }^{48}$ | 60 |  | 54 | 0 |  |  |  |  | 0 | 0 |  |  |  |
|  | $\stackrel{0}{7.18}$ | $\stackrel{0}{7.18}$ | ${ }_{7.18}^{68}$ | ${ }^{55}$ | ${ }^{58}$ | ${ }_{7}^{61}$ | ${ }_{7}^{58}$ | $\stackrel{0}{7.18}$ | $\stackrel{0}{7.18}$ | ${ }_{7}{ }_{7}^{51}$ | ${ }_{7}^{62}$ | ${ }_{7}^{70}$ | ${ }_{7}^{64}$ | ${ }_{7.18}^{65}$ | ${ }_{7.18}^{49}$ |  | ${ }_{7.04}^{37}$ | ${ }_{7}^{4.04}$ | ${ }_{7.04}^{47}$ |  | ${ }_{5}^{56}$ | 52 <br> 7.04 | $\stackrel{0}{7.04}$ | ${ }_{7}^{65}$ | ${ }_{7.04}^{65}$ | ${ }_{7}^{69}$ | ${ }_{5}^{50}$ | $\stackrel{0}{7.04}$ | $\stackrel{0}{7.04}$ | $\stackrel{0}{7.04}$ |  |  |
| $1{ }^{10}$ Net Operation Time $=(7) \times(9)$ | ${ }^{\circ}$ | $\stackrel{1}{0}$ | ${ }_{503}$ | 402 | 431 | 445 | 438 | 0 | 0 | ${ }_{381}$ | 460 | 510 | 474 | 481 | ${ }_{3} 59$ | ${ }_{0}$ | ${ }_{268}$ | ${ }_{338}$ | ${ }_{338}$ | 422 | ${ }_{401}$ | ${ }_{300}$ | $\stackrel{0}{0}$ | 472 | ${ }_{4}{ }_{4}$ | $\stackrel{4}{493}$ | ${ }_{373}$ | $\stackrel{\square}{0}$ | $\stackrel{\square}{0}$ | $\stackrel{1}{0}$ | $\stackrel{\square}{0}$ | ${ }_{8839}$ |
| 11 Avalability (\%) $=(6) /(5) \times 100 \%$ | Iovo | IVVOO | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | \#DVVO! | IDVO) | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | 100.0 | OVVO | 100.0 | 100.0 | 100.0 | 00.0 | 100.0 | 100.0 | IVVo | 100.0 | 100.0 | 100.0 | 硅 | Ivo | IVVO | \#\#DVO | IvVo, |  |
| 12 Periormance (\%) $)$ (10) /(6) $\times 100 \%$ | \#ovol | Hovol | 94.1 | 84.8 |  |  |  |  | \#ivo! |  |  |  |  |  |  | ovio | 56.4 | ${ }^{63.3}$ | ${ }^{63.3}$ | ${ }^{89.1}$ |  |  |  |  |  |  |  |  |  |  |  |  |
| (13) | \#DIV/0! | \%oivo! | ${ }^{97.4}$ |  | ${ }^{96.0}$ |  |  | \%olvo! | ! $\begin{aligned} & \text { \#ovivo! } \\ & \text { \#DVa! }\end{aligned}$ |  | ${ }^{\text {77. }} 7$ |  | ${ }_{96.9}$ |  |  | $\xrightarrow{\text { \#olvivo }}$ | ${ }_{55.0} 9$ | $\stackrel{95.8}{60.6}$ | ${ }_{62,0}$ | ${ }^{954.7}$ | 98.2 80.6 | ${ }_{77.2} 96$ | \#\#vo! | ${ }^{97.0}$ | ${ }_{96.5}^{97.0}$ | ${ }^{988.6}$ | ${ }^{\text {74.3 }}$ | \#\#DV! | \%olv! | \%olvo | \% \#olvo! | ${ }^{97.0}{ }^{\text {97. }}$ |

## B3: Chassis-Final Assembly Line Production Data for September 2015

| Shift A |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| No. ${ }^{\text {Natasil }}$ CHASIS-FINALLINE | 1 | $\frac{2}{71}$ | 3 | ${ }_{71}$ | 5 | 6 | $\frac{7}{126}$ | 8 | 9 | $\frac{10}{71}$ | ${ }^{11}$ | $\frac{12}{71}$ | 13 | ${ }^{14}$ | ${ }^{15}$ | 16 | ${ }_{71}^{17}$ | ${ }_{71}^{18}$ | ${ }^{19}$ | 20 | ${ }_{121}^{21}$ | $\frac{22}{71}$ | ${ }^{23}$ | ${ }^{24}$ | 25 | ${ }^{26}$ | ${ }^{27}$ | ${ }^{28}$ | $\frac{29}{71}$ | ${ }^{30}$ | ${ }^{\text {Cumul. }}$ |
| 1 Planned domntime per Shit | ${ }^{71}$ | 71 | ${ }^{71}$ | ${ }^{71}$ | 0 | 0 | ${ }^{126}$ | 0 | 0 | ${ }^{71}$ | ${ }^{89}$ | 0 | 0 |  | ${ }^{71}$ | 0 | , | ${ }^{71}$ | ${ }^{71}$ | 0 | ${ }^{126}$ | ${ }^{71}$ | 0 | 0 | 0 |  | 0 | ${ }^{71}$ | ${ }^{71}$ | ${ }^{71}$ | ${ }^{1406}$ |
| 22. Downtime Loss | ${ }^{12}$ | 0 | ${ }^{11}$ | ${ }^{20}$ | 0 | 0 | ${ }^{26}$ | - | 0 | 8 | 9 | 0 | 0 | 5 | 0 | 0 | ${ }_{3}^{3}$ | 0 | 8 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | $\stackrel{4}{4}$ | 14 14 14 | $\stackrel{2}{2}$ | ${ }^{126}{ }_{126}^{126}$ |
| - Machine braakdown (G) | ${ }^{12}$ | 0 | ${ }^{11}$ | ${ }^{20}$ | $\bigcirc$ | $\bigcirc$ | ${ }^{26}$ | $\bigcirc$ | $\bigcirc$ | 8 | ${ }_{0} 9$ | $\bigcirc$ | $\bigcirc$ | 5 | $\bigcirc$ | 0 | ${ }_{3}^{3}$ | $\bigcirc$ | ${ }^{8}$ | 0 | ${ }_{0}^{4}$ | 0 | 0 | 0 | 0 | 0 | 0 | ${ }_{0}^{4}$ | $\stackrel{14}{14}$ | $\stackrel{2}{0}$ | $\stackrel{126}{10}$ |
|  | $\bigcirc$ | $\bigcirc$ | 0 | 0 | $\bigcirc$ | 0 | 0 | $\bigcirc$ | $\bigcirc$ | 0 | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | 0 | $\bigcirc$ | $\bigcirc$ | $\bigcirc$ |  | 0 | 0 | 0 |  |  | $\stackrel{0}{0}$ |  |
| - -rocoess quality issue ( $Q$ ) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 5 |
| - Venicle quality issue (I) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Logisitics (D) | 63 | 0 | 0 | 49 | 0 | 0 | 3 | 4 | 0 | 8 | 24 | ${ }^{33}$ | 0 | 21 | 0 | 0 | 2 | 8 | 7 | 0 | 17 | 0 | 0 | 0 | 0 | 0 |  | 40 | 20 | 8 | 307 |
| PPC (H) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 | 0 | 0 |  |
| Chassis jimmed (C) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |
| Operator downstation ( $P$ ) | 6 | 2 | 0 | 15 | 0 | 0 | 10 | ${ }^{47}$ | ${ }^{33}$ | 18 | 25 | 10 | 0 | 0 | 13 | 0 | 27 | 9 | 2 | 0 | 3 | ${ }^{26}$ | ${ }^{38}$ | 0 | 0 | 0 | 0 | 2 | 0 | 0 | 286 |
| New operator under traning (N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  |
| Bad attendance ( $($ ) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Watiting hanger ( W ) | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 0 | ${ }^{43}$ | ${ }^{23}$ | 4 | 0 | 0 | 21 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 15 | 7 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Oiters (B) | 0 | 2 | 0 | 0 | 0 | 0 | 11 | 0 | 0 | 4 | 9 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 34 |
| 3 Ofline Unit per day | 0 | 10 | 1 | 5 | 0 | 0 | 0 | 0 | 6 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 14 | 6 | 5 | 0 | 6 | 2 | 0 | 0 | 0 | 0 | 0 | 5 | 0 | 6 |  |
| 4 - Totala poerating hours per SSit | ${ }^{0}$ | ${ }^{0}$ | ${ }^{605}$ | ${ }_{6}^{605}$ | ${ }_{605}^{605}$ | ${ }_{6}^{605}$ | ${ }_{545}$ | 0 | 0 | ${ }_{545}^{54}$ | ${ }_{545}^{545}$ | ${ }_{545}$ | ${ }_{545}^{545}$ | ${ }_{555}^{545}$ | ${ }_{545}^{545}$ | 0 | 545 | ${ }_{6}^{605}$ | $\stackrel{605}{54}$ | ${ }_{545}^{545}$ | ${ }_{6}^{605}$ | $\stackrel{545}{44}$ | 0 | 0 | 0 | 0 | 0 | ${ }_{4}^{545}$ | 545 | 545 | ${ }^{11330}$ |
| ( 5 Planead Production Tme $=(4)-(1)$ | $\stackrel{.71}{-83}$ | $\stackrel{.71}{.71}$ | ${ }_{523}^{53}$ |  |  | ${ }_{605}^{605}$ | ${ }_{393}^{493}$ | 0 | 0 | 474 | ${ }_{447}^{448}$ | ${ }_{474}^{474}$ | ${ }_{545}^{545}$ | ${ }_{479}^{484}$ | ${ }_{474}^{474}$ | 0 |  | ${ }_{534}^{534}$ | 534 <br> 526 | 545 | 479 | ${ }_{4}^{474} 4$ |  |  |  |  |  | 474 470 |  |  |  |
| 7 Total Output Per Shitt | 50 | 63 | 63 | 50 | 0 | 0 | ${ }_{63}$ | 55 | 51 | 55 | 46 | 61 | 0 | 57 |  | 0 | 57 | 70 | 71 | 0 | 61 | 57 | 60 | 0 | 0 | 0 | 0 | 58 | 60 | 41 |  |
| 8 OK Procuct per Shit $=(7)$ - 3 ) | 50 | 53 | 62 | 45 | 0 | 0 | 63 | ${ }^{55}$ | 45 | 55 | 46 | 61 | 0 | 57 | 67 | 0 |  | 64 | 66 | 0 | 55 | 55 | 60 | 0 | 0 | 0 | 0 | 53 | 60 | ${ }^{35}$ |  |
| 9 Actual cycle time | 7.18 | 7.18 | ${ }^{7.18}$ | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 |  | 7.18 | 7.04 | 7.04 | 7.04 | 7.04 | 7.04 | 7.04 | 7.04 | 7.04 | 7.04 | 7.04 | 7.04 | 7.18 | 7.18 | 7.18 |  |
| 10. Net Operation Tme $=(7) \times(9)$ | 359 | 452 | ${ }^{452}$ | ${ }_{359}$ | 0 | 0 | 452 | 395 | ${ }^{366}$ | 395 | 330 | 438 | 0 | 409 | 481 | 0 | 401 | 493 | 500 | 0 | 429 | 401 | 422 | 0 | 0 | 0 | 0 | 416 | 431 | 294 | ${ }_{8678}$ |
| 11 Avaliability (\%) = (6) / (5) $\times 100 \%$ | 116.9 | 100.0 | 97.9 | ${ }^{96.3}$ |  | 100.0 | ${ }^{93.8}$ | \#ovvol | \#olvol |  |  |  | 100.0 |  | 100.0 | \#ovvo! | 99.4 | 100.0 | ${ }^{98.5}$ | 100.0 | 99.2 | 100.0 | \#ovivol | \#ovol | \#DivV! | \#Divol | \#olvol | 99.2 | 97.0 | 99.6 |  |
| 12 Performance (\%) $=(10) /(6) \times 100 \%$ |  |  | ${ }_{86.5}^{894}$ | 69.8 |  |  | ${ }^{115.1}$ | \# $\quad 10 \times 0$ O! |  | $\stackrel{847}{10}$ | ${ }^{7} 3.9$ |  |  | $\frac{85.4}{100 .}$ | $\frac{101.5}{100 .}$ |  | ${ }^{85.2}$ | ${ }^{92,3}$ |  |  | $\frac{90.4}{90.2}$ | ${ }^{84.7}{ }^{96.5}$ |  |  |  |  |  | ${ }^{88.6}$ |  | ${ }_{62,4}^{654}$ |  |
|  | - 1000.0 | ${ }_{\text {- }}^{536.0}$ | ${ }^{98.4} 8$ | ${ }^{90.0}$ | $\xrightarrow{\text { \#idvo }}$ | \#\#DVIV! | 100.0 1080 | Hovivo! | -8.2. | ${ }_{8}^{100.0}$ | $\xrightarrow{100.4}$ | ${ }^{102.0}$ | - \#ivol | ${ }^{100.0} 8$ | 10015 | - \#olvo! | 63.9 | ${ }^{84.4}$ | ${ }^{937.0}$ | \#\#DVO! | ${ }^{90.8}$ | ${ }_{81.7}$ | [\#OVV: | f\#livo! | T\#OIVO! ! | \#\#lvo! | ) + \#lvivo! | ${ }^{90.3}$ | ${ }^{\text {900.9 }}$ | ${ }^{85.0}$ | ${ }^{942.6}$ |


| No. CHASSIS-FINAL LINE | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | ${ }^{23}$ | ${ }^{24}$ | 25 | 26 | 27 | 28 | 29 | 30 |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 Planned downtime per Shith | 71 | 71 | 71 | 71 | 0 | 0 | ${ }^{126}$ | 0 | 0 | 71 | 89 | 71 | 0 | 71 | 71 | 0 | 71 | 71 | 71 | 0 | 126 | 7 | , | 0 | 0 | 0 | 0 | 71 | 71 | 71 | 1406 |
| 22. Downtime Loss | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ${ }^{22}$ | 0 | 0 | ${ }^{25}$ |
| - Machine breakcown (G) | 0 | 0 |  | 0 | 0 |  | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ${ }^{22}$ | 0 | 0 |  |
| - Tools Jig () | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| 28 Speed Loss | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| - Procoss quality isue (Q) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  | 0 | 0 | 0 | 0 |  | 0 | 0 |  |  | 0 | 0 | ${ }^{20}$ | 0 | - |  |
| - Venicle quality issue () | ${ }^{22}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ${ }^{13}$ | 8 | 0 | 5 | 0 | ${ }^{22}$ | ${ }_{5} 5$ | 0 | 5 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Looisitics (D) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 17 | 13 | 0 |
| -PPC (H) | 9 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| Chassis jimmed (C) | 0 | 47 | 0 | 0 | 0 | 0 | 0 | 0 | 4 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |
| -Operator downstation ( $P$ ) | 0 | 15 | 4 | 0 | 0 | 0 | 0 | 0 | 2 | ${ }^{38}$ | 10 | 0 | 0 | 0 | 14 | 0 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | ${ }^{12}$ | 0 |
| - New operator under training (N) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |  |  |
| - Bad atendance ( $A$ ) | 55 | 0 | 0 | 0 | 0 | 0 | 18 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| Wating hanger ( W ) | 10 | 0 | ${ }^{28}$ | 0 | 0 | 0 | 0 | ${ }^{33}$ | 45 | 6 | 7 | ${ }^{15}$ | 0 | 7 | ${ }^{31}$ | 0 | ${ }^{46}$ | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | ${ }^{42}$ | ${ }^{12}$ |  |
| Others (B) | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 8 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 32 | 0 | 0 |
| 3 Ooftine Unit per day | 0 | 0 | 0 | 3 | 0 | 0 | 0 | 0 | 1 |  | 0 | 1 | 0 | 0 | 0 | 0 | ${ }_{5}^{2}$ |  | 0 | 0 | 0 | 0 | 0 |  | 0 | 0 |  | ${ }^{11}$ |  | ${ }^{2}$ | ${ }^{21}$ |
| 4 Total peprating hours per Shit | 545 | 545 | 605 | 545 | 0 | 0 | 615 | 545 | 545 | 605 | 665 | 545 | 0 | 605 | 545 | 0 | 545 | 605 | 605 | 0 | 615 | 545 | 0 | , | 0 | 0 | 0 | 545 | 545 | 545 | ${ }^{11460}$ |
| 5 Planned Prociction Time $=(4)-(1)$ | 474 | 474 | 534 | 474 | 0 | 0 | 489 | 545 | 545 | 534 | 576 | 474 | 0 | 534 | 474 | 0 | 474 | 534 | 534 | 0 | 489 | 474 | 0 | - | 0 | 0 | 0 | 474 | 474 | 474 |  |
| ${ }^{6}$ O Operation Tme $=(5)-(2 A)-(28)$ | 474 | ${ }_{5}^{474}$ | ${ }_{57}^{53}$ | 474 | 0 | 0 | 489 | 545 | 545 | ${ }_{534}$ | 576 | 474 | 0 | 534 | 474 | 0 | 471 | 534 | ${ }_{534}$ | 0 | 489 | 474 | 0 | 0 | 0 | 0 | 0 | 452 | 474 | 474 |  |
| 7 Total Output Per Shitt | 48 | 52 | 57 | 60 | 0 | 0 | 71 | 61 | ${ }^{52}$ | ${ }_{5}^{56}$ | 60 | 62 | 0 | 67 | 44 | 0 | ${ }_{5} 5$ | 44 | 70 | 0 | 60 | ${ }_{5}^{57}$ | 0 | 0 | 0 | 0 | 0 | ${ }_{5} 5$ | ${ }^{50}$ | 61 | 1144 |
| 8 OK Product per Shit = (7) - (3) | 48 | 5 | 57 | 57 | 0 | 0 | 71 | ${ }^{61}$ | 51 | 55 | 60 | ${ }^{61}$ | 0 | 67 | 44 | 0 | ${ }^{54}$ | 44 | 70 | 0 | 60 | 57 | 0 | 0 | 0 | 0 | 0 | 45 | 50 | 59 | 1123 |
| 9 Actual cycle time | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 | 7.18 |  |  | 7.18 | 7.18 | 7.18 | 7.04 | 7.04 | 7.04 | 7.04 |  | 7.04 | 7.04 | 7.04 |  | 7.04 |  | 7.04 |  | 7.04 |  |
| 10. Net Operation Time $=(7) \times$ (9) | 345 | ${ }^{373}$ | 409 | 431 | 0 | 0 | 510 | 438 | 373 | 402 | 431 | 445 | 0 | 481 | 316 | 0 | 394 | 310 | 493 | 0 | 422 | 401 | 0 | 0 | 0 | 0 | 0 | 394 | 352 | 429 | 8150 |
| 11. Avilability (\%) $=(66) /(5) \times 100 \%$ | 100.0 | 100.0 | 100.0 | 100.0 | \#oivol | \#DVVIO! | 100.0 | 100.0 | 100.0 | ${ }^{100.0}$ | 100.0 | 100.0 | \# \#ivol | 100.0 | 100.0 | (\#DVIV! | 99.4. | 100.0 | 100.0 | \#olvol | 100.0 | 100.0 | (\#Divol |  | \#DVVO! | \#olvol | \#olvol | 95.4. | ${ }^{100.0}$ | 100.0 | ${ }^{99.8}$ |
|  |  |  | ${ }^{160.6}$ | ${ }_{950.9}^{90}$ |  |  |  |  | ${ }_{98,1}^{68.5}$ |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |  |
| 14 Overall Eawimment Etfectiveness (OEE) \% | 72.7 | 78.8 | 76.6 | 86.3 | \#Divo! | *DIV0! | 104.2 | 80.4 | 67.2 | 74.0 | 74.8 | 92.4 | [\#OIVO! | 90.1 | 66.6 | [\#DVIV! | ${ }^{80.2}$ | 58.0 | ${ }_{923}$ | ? + DVVO! | 88.4 | 84.7 | \#DIVO! | \#DIVO! | - $\ddagger$ DIVO! | [\#DVV0! | [\#IVV0! | 66.8 | ${ }_{74.3}$ | ${ }_{87,6}$ | ${ }_{7} 9.6$ |

## APPENDIX C

## C1: Control Chart Data for Availability by Shifts

| shift A |  |  |  |  |  | shift B |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DAY | AVAILABILITY (p) | CENTER (P-BAR) | UCL | LCL |  | DAY | AVAILABILITY (p) | CENTER (P-BAR) | UCL | LCL |
| july | 1 | 1 | 0.9909 | 1.003985 | 0.977815 | july | 1 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 2 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 2 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 3 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 3 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 6 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 6 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 7 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 7 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 8 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 8 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 9 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 9 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 10 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 10 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 11 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 11 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 13 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 13 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 14 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 14 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 22 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 22 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 23 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 23 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 24 | 0.995780591 | 0.9909 | 1.003985 | 0.977815 |  | 24 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 27 | 0.976793249 | 0.9909 | 1.003985 | 0.977815 |  | 27 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 28 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 28 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 29 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 29 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 30 | 0.981012658 | 0.9909 | 1.003985 | 0.977815 |  | 30 | 1 | 0.999 | 1.003351 | 0.994649 |
| august | 3 | 1 | 0.9909 | 1.003228 | 0.978572 | august | 3 | 1 | 0.999 | 1.003103 | 0.994897 |
|  | 4 | 1 | 0.9909 | 1.003228 | 0.978572 |  | 4 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 5 | 1 | 0.9909 | 1.003228 | 0.978572 |  | 5 | 1 | 0.999 | 1.003103 | 0.994897 |
|  | 6 | 1 | 0.9909 | 1.003228 | 0.978572 |  | 6 | 1 | 0.999 | 1.003103 | 0.994897 |
|  | 7 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 7 | 1 | 0.999 | 1.003288 | 0.994712 |
|  | 10 | 0.945147679 | 0.9909 | 1.003985 | 0.977815 |  | 10 | 1 | 0.999 | 1.003103 | 0.994897 |
|  | 13 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 11 | 1 | 0.999 | 1.002951 | 0.995049 |
|  | 15 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 13 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 17 | 0.917721519 | 0.9909 | 1.003985 | 0.977815 |  | 14 | 1 | 0.999 | 1.003103 | 0.994897 |
|  | 18 | 0.983146067 | 0.9909 | 1.003228 | 0.978572 |  | 15 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 19 | 1 | 0.9909 | 1.003228 | 0.978572 |  | 17 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 20 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 18 | 1 | 0.999 | 1.003103 | 0.994897 |
|  | 21 | 1 | 0.9909 | 1.003228 | 0.978572 |  | 18 | 1 | 0.999 | 1.003103 | 0.994897 |
|  | 22 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 20 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 24 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 21 | 1 | 0.999 | 1.003288 | 0.994712 |
|  | 25 | 0.921940928 | 0.9909 | 1.003985 | 0.977815 |  | 22 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 26 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 24 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 27 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 25 | 1 | 0.999 | 1.003355 | 0.994645 |
| sept | 3 | 0.979400749 | 0.9909 | 1.003228 | 0.978572 |  | 26 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 4 | 0.962546816 | 0.9909 | 1.003228 | 0.978572 |  | 27 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 10 | 0.983122363 | 0.9909 | 1.003985 | 0.977815 | sept | 1 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 11 | 0.980263158 | 0.9909 | 1.004241 | 0.977559 |  | 2 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 12 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 3 | 1 | 0.999 | 1.003103 | 0.994897 |
|  | 14 | 0.989669421 | 0.9909 | 1.003849 | 0.977951 |  | 4 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 17 | 0.993670886 | 0.9909 | 1.003985 | 0.977815 |  | 7 | 1 | 0.999 | 1.003288 | 0.994712 |
|  | 18 | 1 | 0.9909 | 1.003228 | 0.978572 |  | 8 | 1 | 0.999 | 1.003062 | 0.994938 |
|  | 19 | 0.985018727 | 0.9909 | 1.003228 | 0.978572 |  | 9 | 1 | 0.999 | 1.003062 | 0.994938 |
|  | 21 | 0.991649269 | 0.9909 | 1.003916 | 0.977884 |  | 10 | 1 | 0.999 | 1.003103 | 0.994897 |
|  | 22 | 1 | 0.9909 | 1.003985 | 0.977815 |  | 11 | 1 | 0.999 | 1.002951 | 0.995049 |
|  | 28 | 0.991561181 | 0.9909 | 1.003985 | 0.977815 |  | 12 | 1 | 0.999 | 1.003355 | 0.994645 |
|  | 29 | 0.970464135 | 0.9909 | 1.003985 | 0.977815 |  | 14 | 1 | 0.999 | 1.003103 | 0.994897 |
|  | 30 | 0.995780591 | 0.9909 | 1.003985 | 0.977815 |  | 15 | 1 | 0.999 | 1.003355 | 0.994645 |
|  |  |  |  |  |  |  | 17 | 0.993670886 | 0.999 | 1.003355 | 0.994645 |
|  |  |  |  |  |  |  | 18 | 1 | 0.999 | 1.003355 | 0.994645 |
|  |  |  |  |  |  |  | 19 | 1 | 0.999 | 1.003355 | 0.994645 |
|  |  |  |  |  |  |  | 21 | 1 | 0.999 | 1.003355 | 0.994645 |
|  |  |  |  |  |  |  | 22 | 1 | 0.999 | 1.003355 | 0.994645 |
|  |  |  |  |  |  |  | 28 | 0.953586498 | 0.999 | 1.003355 | 0.994645 |
|  |  |  |  |  |  |  | 29 | 1 | 0.999 | 1.003355 | 0.994645 |
|  |  |  |  |  |  |  | 30 | 1 | 0.999 | 1.003355 | 0.994645 |

C2: Control Chart Data for Performance by Shifts

| shift A |  |  |  |  |  | shift B |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DAY | PERFORMANCE (p) | CENTER P BAR | UCL | LCL |  | DAY | PERFORMANCE (P) | CENTER P BAR | UCL | LCL |
| july | 1 | 0.833333333 | 0.8512 | 0.90024 | 0.80216 | july | 1 | 0.848101266 | 0.824 | 0.876475 | 0.771525 |
|  | 2 | 0.833333333 | 0.8512 | 0.90024 | 0.80216 |  | 2 | 0.803797468 | 0.824 | 0.876475 | 0.771525 |
|  | 3 | 0.757383966 | 0.8512 | 0.90024 | 0.80216 |  | 3 | 0.862869198 | 0.824 | 0.876475 | 0.771525 |
|  | 6 | 0.9092827 | 0.8512 | 0.90024 | 0.80216 |  | 6 | 0.924050633 | 0.824 | 0.876475 | 0.771525 |
|  | 7 | 0.862869198 | 0.8512 | 0.90024 | 0.80216 |  | 7 | 0.9092827 | 0.824 | 0.876475 | 0.771525 |
|  | 8 | 0.953586498 | 0.8512 | 0.90024 | 0.80216 |  | 8 | 0.9092827 | 0.824 | 0.876475 | 0.771525 |
|  | 9 | 0.757383966 | 0.8512 | 0.90024 | 0.80216 |  | 9 | 0.833333333 | 0.824 | 0.876475 | 0.771525 |
|  | 10 | 0.757383966 | 0.8512 | 0.90024 | 0.80216 |  | 10 | 0.772151899 | 0.824 | 0.876475 | 0.771525 |
|  | 11 | 0.786919831 | 0.8512 | 0.90024 | 0.80216 |  | 11 | 0.757383966 | 0.824 | 0.876475 | 0.771525 |
|  | 13 | 0.803797468 | 0.8512 | 0.90024 | 0.80216 |  | 13 | 0.848101266 | 0.824 | 0.876475 | 0.771525 |
|  | 14 | 0.833333333 | 0.8512 | 0.90024 | 0.80216 |  | 14 | 0.786919831 | 0.824 | 0.876475 | 0.771525 |
|  | 22 | 0.862869198 | 0.8512 | 0.90024 | 0.80216 |  | 22 | 0.848101266 | 0.824 | 0.876475 | 0.771525 |
|  | 23 | 0.848101266 | 0.8512 | 0.90024 | 0.80216 |  | 23 | 0.757383966 | 0.824 | 0.876475 | 0.771525 |
|  | 24 | 0.851694915 | 0.8512 | 0.900344 | 0.802056 |  | 24 | 0.772151899 | 0.824 | 0.876475 | 0.771525 |
|  | 27 | 0.805615551 | 0.8512 | 0.900819 | 0.801581 |  | 27 | 0.848101266 | 0.824 | 0.876475 | 0.771525 |
|  | 28 | 0.848101266 | 0.8512 | 0.90024 | 0.80216 |  | 28 | 0.757383966 | 0.824 | 0.876475 | 0.771525 |
|  | 29 | 0.848101266 | 0.8512 | 0.90024 | 0.80216 |  | 29 | 0.757383966 | 0.824 | 0.876475 | 0.771525 |
|  | 30 | 0.849462366 | 0.8512 | 0.900712 | 0.801688 |  | 30 | 0.861052632 | 0.824 | 0.87642 | 0.77158 |
| august | 3 | 0.941947566 | 0.8512 | 0.897403 | 0.804997 | august | 3 | 0.941947566 | 0.824 | 0.873439 | 0.774561 |
|  | 4 | 0.779026217 | 0.8512 | 0.897403 | 0.804997 |  | 4 | 0.848101266 | 0.824 | 0.876475 | 0.771525 |
|  | 5 | 0.887640449 | 0.8512 | 0.897403 | 0.804997 |  | 5 | 0.807116105 | 0.824 | 0.873439 | 0.774561 |
|  | 6 | 0.833333333 | 0.8512 | 0.897403 | 0.804997 |  | 6 | 0.833333333 | 0.824 | 0.873439 | 0.774561 |
|  | 7 | 0.938818565 | 0.8512 | 0.90024 | 0.80216 |  | 7 | 0.895705521 | 0.824 | 0.875664 | 0.772336 |
|  | 10 | 0.832589286 | 0.8512 | 0.901643 | 0.800757 |  | 10 | 0.713483146 | 0.824 | 0.873439 | 0.774561 |
|  | 13 | 0.970464135 | 0.8512 | 0.90024 | 0.80216 |  | 11 | 0.798611111 | 0.824 | 0.871603 | 0.776397 |
|  | 15 | 0.757383966 | 0.8512 | 0.90024 | 0.80216 |  | 13 | 1 | 0.824 | 0.876475 | 0.771525 |
|  | 17 | 0.937931034 | 0.8512 | 0.902391 | 0.800009 |  | 14 | 0.900749064 | 0.824 | 0.873439 | 0.774561 |
|  | 18 | 0.67047619 | 0.8512 | 0.897797 | 0.804603 |  | 15 | 0.757383966 | 0.824 | 0.876475 | 0.771525 |
|  | 19 | 0.737827715 | 0.8512 | 0.897403 | 0.804997 |  | 17 | 0.565400844 | 0.824 | 0.876475 | 0.771525 |
|  | 20 | 0.890295359 | 0.8512 | 0.90024 | 0.80216 |  | 18 | 0.632958801 | 0.824 | 0.873439 | 0.774561 |
|  | 21 | 0.923220974 | 0.8512 | 0.897403 | 0.804997 |  | 18 | 0.632958801 | 0.824 | 0.873439 | 0.774561 |
|  | 22 | 0.981012658 | 0.8512 | 0.90024 | 0.80216 |  | 20 | 0.890295359 | 0.824 | 0.876475 | 0.771525 |
|  | 24 | 0.936708861 | 0.8512 | 0.90024 | 0.80216 |  | 21 | 0.8200409 | 0.824 | 0.875664 | 0.772336 |
|  | 25 | 0.981693364 | 0.8512 | 0.902274 | 0.800126 |  | 22 | 0.801687764 | 0.824 | 0.876475 | 0.771525 |
|  | 26 | 0.966244726 | 0.8512 | 0.90024 | 0.80216 |  | 24 | 0.995780591 | 0.824 | 0.876475 | 0.771525 |
|  | 27 | 0.742616034 | 0.8512 | 0.90024 | 0.80216 |  | 25 | 0.995780591 | 0.824 | 0.876475 | 0.771525 |
| sept | 3 | 0.864244742 | 0.8512 | 0.897886 | 0.804514 |  | 26 | 1.040084388 | 0.824 | 0.876475 | 0.771525 |
|  | 4 | 0.69844358 | 0.8512 | 0.898293 | 0.804107 |  | 27 | 0.786919831 | 0.824 | 0.876475 | 0.771525 |
|  | 10 | 0.847639485 | 0.8512 | 0.900659 | 0.801741 | sept | 1 | 0.727848101 | 0.824 | 0.876475 | 0.771525 |
|  | 11 | 0.738255034 | 0.8512 | 0.901699 | 0.800701 |  | 2 | 0.786919831 | 0.824 | 0.876475 | 0.771525 |
|  | 12 | 0.924050633 | 0.8512 | 0.90024 | 0.80216 |  | 3 | 0.765917603 | 0.824 | 0.873439 | 0.774561 |
|  | 14 | 0.853862213 | 0.8512 | 0.899983 | 0.802417 |  | 4 | 0.9092827 | 0.824 | 0.876475 | 0.771525 |
|  | 17 | 0.851380042 | 0.8512 | 0.900396 | 0.802004 |  | 7 | 1.042944785 | 0.824 | 0.875664 | 0.772336 |
|  | 18 | 0.923220974 | 0.8512 | 0.897403 | 0.804997 |  | 8 | 0.803669725 | 0.824 | 0.872938 | 0.775062 |
|  | 19 | 0.950570342 | 0.8512 | 0.897753 | 0.804647 |  | 9 | 0.68440367 | 0.824 | 0.872938 | 0.775062 |
|  | 21 | 0.903157895 | 0.8512 | 0.900188 | 0.802212 |  | 10 | 0.752808989 | 0.824 | 0.873439 | 0.774561 |
|  | 22 | 0.845991561 | 0.8512 | 0.90024 | 0.80216 |  | 11 | 0.748263889 | 0.824 | 0.871603 | 0.776397 |
|  | 28 | 0.885106383 | 0.8512 | 0.900448 | 0.801952 |  | 12 | 0.938818565 | 0.824 | 0.876475 | 0.771525 |
|  | 29 | 0.936956522 | 0.8512 | 0.900981 | 0.801419 |  | 14 | 0.900749064 | 0.824 | 0.873439 | 0.774561 |
|  | 30 | 0.622881356 | 0.8512 | 0.900344 | 0.802056 |  | 15 | 0.666666667 | 0.824 | 0.876475 | 0.771525 |
|  |  |  |  |  |  |  | 17 | 0.836518047 | 0.824 | 0.876475 | 0.771525 |
|  |  |  |  |  |  |  | 18 | 0.580524345 | 0.824 | 0.876475 | 0.771525 |
|  |  |  |  |  |  |  | 19 | 0.923220974 | 0.824 | 0.876475 | 0.771525 |
|  |  |  |  |  |  |  | 21 | 0.862985685 | 0.824 | 0.876475 | 0.771525 |
|  |  |  |  |  |  |  | 22 | 0.845991561 | 0.824 | 0.876475 | 0.771525 |
|  |  |  |  |  |  |  | 28 | 0.871681416 | 0.824 | 0.876475 | 0.771525 |
|  |  |  |  |  |  |  | 29 | 0.742616034 | 0.824 | 0.876475 | 0.771525 |
|  |  |  |  |  |  |  | 30 | 0.905063291 | 0.824 | 0.876475 | 0.771525 |

C3: Control Chart Data for Quality by Shifts

| shift A |  |  |  |  |  | shift B |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DAY | QUALITY (p) | CENTER (P-BAR) | UCL | LCL |  | DAY | QUALITY (P) | CENTER (P-BAR) | UCL | LCL |
| july | 1 | 0.963636364 | 0.9539 | 1.038729 | 0.869071 | july | 1 | 1 | 0.9749 | 1.037611 | 0.912189 |
|  | 2 | 0.981818182 | 0.9539 | 1.038729 | 0.869071 |  | 2 | 0.962264151 | 0.9749 | 1.039361 | 0.910439 |
|  | 3 | 1 | 0.9539 | 1.042869 | 0.864931 |  | 3 | 0.964912281 | 0.9749 | 1.037059 | 0.912741 |
|  | 6 | 0.966666667 | 0.9539 | 1.035117 | 0.872683 |  | 6 | 0.967213115 | 0.9749 | 1.034986 | 0.914814 |
|  | 7 | 0.98245614 | 0.9539 | 1.037227 | 0.870573 |  | 7 | 0.966666667 | 0.9749 | 1.035485 | 0.914315 |
|  | 8 | 0.904761905 | 0.9539 | 1.03316 | 0.87464 |  | 8 | 0.933333333 | 0.9749 | 1.035485 | 0.914315 |
|  | 9 | 0.94 | 0.9539 | 1.042869 | 0.864931 |  | 9 | 0.963636364 | 0.9749 | 1.038179 | 0.911621 |
|  | 10 | 0.96 | 0.9539 | 1.042869 | 0.864931 |  | 10 | 0.980392157 | 0.9749 | 1.040613 | 0.909187 |
|  | 11 | 0.961538462 | 0.9539 | 1.041141 | 0.866659 |  | 11 | 0.96 | 0.9749 | 1.041267 | 0.908533 |
|  | 13 | 1 | 0.9539 | 1.040314 | 0.867486 |  | 13 | 0.964285714 | 0.9749 | 1.037611 | 0.912189 |
|  | 14 | 0.981818182 | 0.9539 | 1.038729 | 0.869071 |  | 14 | 0.961538462 | 0.9749 | 1.039978 | 0.909822 |
|  | 22 | 0.964912281 | 0.9539 | 1.037227 | 0.870573 |  | 22 | 0.964285714 | 0.9749 | 1.037611 | 0.912189 |
|  | 23 | 0.964285714 | 0.9539 | 1.037968 | 0.869832 |  | 23 | 1 | 0.9749 | 1.041267 | 0.908533 |
|  | 24 | 0.982142857 | 0.9539 | 1.037968 | 0.869832 |  | 24 | 1 | 0.9749 | 1.040613 | 0.909187 |
|  | 27 | 1 | 0.9539 | 1.041141 | 0.866659 |  | 27 | 1 | 0.9749 | 1.037611 | 0.912189 |
|  | 28 | 1 | 0.9539 | 1.037968 | 0.869832 |  | 28 | 0.94 | 0.9749 | 1.041267 | 0.908533 |
|  | 29 | 0.964285714 | 0.9539 | 1.037968 | 0.869832 |  | 29 | 1 | 0.9749 | 1.041267 | 0.908533 |
|  | 30 | 0.981818182 | 0.9539 | 1.038729 | 0.869071 |  | 30 | 1 | 0.9749 | 1.041267 | 0.908533 |
| august | 3 | 0.971428571 | 0.9539 | 1.029092 | 0.878708 | august | 3 | 0.971428571 | 0.9749 | 1.03099 | 0.91881 |
|  | 4 | 0.982758621 | 0.9539 | 1.036506 | 0.871294 |  | 4 | 0.982142857 | 0.9749 | 1.037611 | 0.912189 |
|  | 5 | 0.96969697 | 0.9539 | 1.031337 | 0.876463 |  | 5 | 0.966666667 | 0.9749 | 1.035485 | 0.914315 |
|  | 6 | 0.983870968 | 0.9539 | 1.033796 | 0.874004 |  | 6 | 0.983870968 | 0.9749 | 1.034499 | 0.915301 |
|  | 7 | 0.935483871 | 0.9539 | 1.033796 | 0.874004 |  | 7 | 0.950819672 | 0.9749 | 1.034986 | 0.914814 |
|  | 10 | 0.942307692 | 0.9539 | 1.041141 | 0.866659 |  | 10 | 0.962264151 | 0.9749 | 1.039361 | 0.910439 |
|  | 13 | 0.9375 | 0.9539 | 1.032538 | 0.875262 |  | 11 | 0.96875 | 0.9749 | 1.033561 | 0.916239 |
|  | 15 | 0.9 | 0.9539 | 1.042869 | 0.864931 |  | 13 | 0.96969697 | 0.9749 | 1.032665 | 0.917135 |
|  | 17 | 0.896551724 | 0.9539 | 1.036506 | 0.871294 |  | 14 | 0.970149254 | 0.9749 | 1.032232 | 0.917568 |
|  | 18 | 0.96 | 0.9539 | 1.042869 | 0.864931 |  | 15 | 0.98 | 0.9749 | 1.041267 | 0.908533 |
|  | 19 | 0.946428571 | 0.9539 | 1.037968 | 0.869832 |  | 17 | 0.973684211 | 0.9749 | 1.051028 | 0.898772 |
|  | 20 | 0.95 | 0.9539 | 1.035117 | 0.872683 |  | 18 | 0.958333333 | 0.9749 | 1.042636 | 0.907164 |
|  | 21 | 0.942857143 | 0.9539 | 1.029092 | 0.878708 |  | 18 | 0.979166667 | 0.9749 | 1.042636 | 0.907164 |
|  | 22 | 0.96969697 | 0.9539 | 1.031337 | 0.876463 |  | 20 | 0.95 | 0.9749 | 1.035485 | 0.914315 |
|  | 24 | 0.968253968 | 0.9539 | 1.03316 | 0.87464 |  | 21 | 0.98245614 | 0.9749 | 1.037059 | 0.912741 |
|  | 25 | 0.967213115 | 0.9539 | 1.034449 | 0.873351 |  | 22 | 0.962962963 | 0.9749 | 1.038762 | 0.911038 |
|  | 26 | 0.953846154 | 0.9539 | 1.031931 | 0.875869 |  | 24 | 0.970149254 | 0.9749 | 1.032232 | 0.917568 |
|  | 27 | 0.9 | 0.9539 | 1.042869 | 0.864931 |  | 25 | 0.970149254 | 0.9749 | 1.032232 | 0.917568 |
| sept | 3 | 0.984126984 | 0.9539 | 1.03316 | 0.87464 |  | 26 | 0.985714286 | 0.9749 | 1.03099 | 0.91881 |
|  | 4 | 0.9 | 0.9539 | 1.042869 | 0.864931 |  | 27 | 0.943396226 | 0.9749 | 1.039361 | 0.910439 |
|  | 10 | 1 | 0.9539 | 1.038729 | 0.869071 | sept | 1 | 1 | 0.9749 | 1.042636 | 0.907164 |
|  | 11 | 1 | 0.9539 | 1.046656 | 0.861144 |  | 2 | 1 | 0.9749 | 1.039978 | 0.909822 |
|  | 12 | 1 | 0.9539 | 1.034449 | 0.873351 |  | 3 | 1 | 0.9749 | 1.037059 | 0.912741 |
|  | 14 | 1 | 0.9539 | 1.037227 | 0.870573 |  | 4 | 0.95 | 0.9749 | 1.035485 | 0.914315 |
|  | 17 | 0.754385965 | 0.9539 | 1.037227 | 0.870573 |  | 7 | 1 | 0.9749 | 1.030594 | 0.919206 |
|  | 18 | 0.914285714 | 0.9539 | 1.029092 | 0.878708 |  | 8 | 1 | 0.9749 | 1.034986 | 0.914814 |
|  | 19 | 0.929577465 | 0.9539 | 1.028561 | 0.879239 |  | 9 | 0.980769231 | 0.9749 | 1.039978 | 0.909822 |
|  | 21 | 0.901639344 | 0.9539 | 1.034449 | 0.873351 |  | 10 | 0.982142857 | 0.9749 | 1.037611 | 0.912189 |
|  | 22 | 0.964912281 | 0.9539 | 1.037227 | 0.870573 |  | 11 | 1 | 0.9749 | 1.035485 | 0.914315 |
|  | 28 | 0.913793103 | 0.9539 | 1.036506 | 0.871294 |  | 12 | 0.983870968 | 0.9749 | 1.034499 | 0.915301 |
|  | 29 | 1 | 0.9539 | 1.035117 | 0.872683 |  | 14 | 1 | 0.9749 | 1.032232 | 0.917568 |
|  | 30 | 0.853658537 | 0.9539 | 1.05215 | 0.85565 |  | 15 | 1 | 0.9749 | 1.045648 | 0.904152 |
|  |  |  |  |  |  |  | 17 | 0.964285714 | 0.9749 | 1.001994 | 0.947806 |
|  |  |  |  |  |  |  | 18 | 1 | 0.9749 | 1.001994 | 0.947806 |
|  |  |  |  |  |  |  | 19 | 1 | 0.9749 | 1.001994 | 0.947806 |
|  |  |  |  |  |  |  | 21 | 1 | 0.9749 | 1.001994 | 0.947806 |
|  |  |  |  |  |  |  | 22 | 1 | 0.9749 | 1.001994 | 0.947806 |
|  |  |  |  |  |  |  | 28 | 0.803571429 | 0.9749 | 1.001994 | 0.947806 |
|  |  |  |  |  |  |  | 29 | 1 | 0.9749 | 1.001994 | 0.947806 |
|  |  |  |  |  |  |  | 30 | 0.967213115 | 0.9749 | 1.001994 | 0.947806 |

C4: Control Chart Data for OEE by Shifts

| shift A |  |  |  |  |  | shift B |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DAY | OEE | CENTER (P-BAR) | UCL | LCL |  | DAY | OEE | CENTER (P-BAR) | UCL | LCL |
| july | 1 | 0.8 | 0.8049 | 0.859505 | 0.750295 | july | 1 | 0.85 | 0.8029 | 0.857716 | 0.748084 |
|  | 2 | 0.82 | 0.8049 | 0.859505 | 0.750295 |  | 2 | 0.77 | 0.8029 | 0.857716 | 0.748084 |
|  | 3 | 0.76 | 0.8049 | 0.859505 | 0.750295 |  | 3 | 0.83 | 0.8029 | 0.857716 | 0.748084 |
|  | 6 | 0.88 | 0.8049 | 0.859505 | 0.750295 |  | 6 | 0.89 | 0.8029 | 0.857716 | 0.748084 |
|  | 7 | 0.85 | 0.8049 | 0.859505 | 0.750295 |  | 7 | 0.88 | 0.8029 | 0.857716 | 0.748084 |
|  | 8 | 0.86 | 0.8049 | 0.859505 | 0.750295 |  | 8 | 0.85 | 0.8029 | 0.857716 | 0.748084 |
|  | 9 | 0.71 | 0.8049 | 0.859505 | 0.750295 |  | 9 | 0.8 | 0.8029 | 0.857716 | 0.748084 |
|  | 10 | 0.73 | 0.8049 | 0.859505 | 0.750295 |  | 10 | 0.76 | 0.8029 | 0.857716 | 0.748084 |
|  | 11 | 0.76 | 0.8049 | 0.859505 | 0.750295 |  | 11 | 0.73 | 0.8029 | 0.857716 | 0.748084 |
|  | 13 | 0.8 | 0.8049 | 0.859505 | 0.750295 |  | 13 | 0.82 | 0.8029 | 0.857716 | 0.748084 |
|  | 14 | 0.82 | 0.8049 | 0.859505 | 0.750295 |  | 14 | 0.76 | 0.8029 | 0.857716 | 0.748084 |
|  | 22 | 0.83 | 0.8049 | 0.859505 | 0.750295 |  | 22 | 0.82 | 0.8029 | 0.857716 | 0.748084 |
|  | 23 | 0.82 | 0.8049 | 0.859505 | 0.750295 |  | 23 | 0.76 | 0.8029 | 0.857716 | 0.748084 |
|  | 24 | 0.83 | 0.8049 | 0.85962 | 0.75018 |  | 24 | 0.77 | 0.8029 | 0.857716 | 0.748084 |
|  | 27 | 0.79 | 0.8049 | 0.86015 | 0.74965 |  | 27 | 0.85 | 0.8029 | 0.857716 | 0.748084 |
|  | 28 | 0.85 | 0.8049 | 0.859505 | 0.750295 |  | 28 | 0.71 | 0.8029 | 0.857716 | 0.748084 |
|  | 29 | 0.82 | 0.8049 | 0.859505 | 0.750295 |  | 29 | 0.76 | 0.8029 | 0.857716 | 0.748084 |
|  | 30 | 0.82 | 0.8049 | 0.860031 | 0.749769 |  | 30 | 0.86 | 0.8029 | 0.857716 | 0.748084 |
| august | 3 | 0.915 | 0.8049 | 0.856346 | 0.753454 | august | 3 | 0.92 | 0.8029 | 0.857716 | 0.748084 |
|  | 4 | 0.766 | 0.8049 | 0.856346 | 0.753454 |  | 4 | 0.83 | 0.8029 | 0.857716 | 0.748084 |
|  | 5 | 0.861 | 0.8049 | 0.856346 | 0.753454 |  | 5 | 0.78 | 0.8029 | 0.857716 | 0.748084 |
|  | 6 | 0.82 | 0.8049 | 0.856346 | 0.753454 |  | 6 | 0.82 | 0.8029 | 0.857716 | 0.748084 |
|  | 7 | 0.878 | 0.8049 | 0.859505 | 0.750295 |  | 7 | 0.85 | 0.8029 | 0.857716 | 0.748084 |
|  | 10 | 0.742 | 0.8049 | 0.861067 | 0.748733 |  | 10 | 0.69 | 0.8029 | 0.857716 | 0.748084 |
|  | 13 | 0.91 | 0.8049 | 0.859505 | 0.750295 |  | 11 | 0.77 | 0.8029 | 0.857716 | 0.748084 |
|  | 15 | 0.682 | 0.8049 | 0.859505 | 0.750295 |  | 13 | 0.97 | 0.8029 | 0.857716 | 0.748084 |
|  | 17 | 0.772 | 0.8049 | 0.8619 | 0.7479 |  | 14 | 0.87 | 0.8029 | 0.857716 | 0.748084 |
|  | 18 | 0.633 | 0.8049 | 0.856785 | 0.753015 |  | 15 | 0.74 | 0.8029 | 0.857716 | 0.748084 |
|  | 19 | 0.698 | 0.8049 | 0.856346 | 0.753454 |  | 17 | 0.55 | 0.8029 | 0.857716 | 0.748084 |
|  | 20 | 0.846 | 0.8049 | 0.859505 | 0.750295 |  | 18 | 0.61 | 0.8029 | 0.857716 | 0.748084 |
|  | 21 | 0.87 | 0.8049 | 0.856346 | 0.753454 |  | 18 | 0.62 | 0.8029 | 0.857716 | 0.748084 |
|  | 22 | 0.951 | 0.8049 | 0.859505 | 0.750295 |  | 20 | 0.85 | 0.8029 | 0.857716 | 0.748084 |
|  | 24 | 0.907 | 0.8049 | 0.859505 | 0.750295 |  | 21 | 0.81 | 0.8029 | 0.857716 | 0.748084 |
|  | 25 | 0.875 | 0.8049 | 0.86177 | 0.74803 |  | 22 | 0.77 | 0.8029 | 0.857716 | 0.748084 |
|  | 26 | 0.922 | 0.8049 | 0.859505 | 0.750295 |  | 24 | 0.97 | 0.8029 | 0.857716 | 0.748084 |
|  | 27 | 0.668 | 0.8049 | 0.859505 | 0.750295 |  | 25 | 0.97 | 0.8029 | 0.857716 | 0.748084 |
| sept | 3 | 0.833 | 0.8049 | 0.856884 | 0.752916 |  | 26 | 1.03 | 0.8029 | 0.857716 | 0.748084 |
|  | 4 | 0.605 | 0.8049 | 0.857337 | 0.752463 |  | 27 | 0.74 | 0.8029 | 0.857716 | 0.748084 |
|  | 10 | 0.833 | 0.8049 | 0.859972 | 0.749828 | sept | 1 | 0.73 | 0.8029 | 0.857716 | 0.748084 |
|  | 11 | 0.724 | 0.8049 | 0.86113 | 0.74867 |  | 2 | 0.79 | 0.8029 | 0.857716 | 0.748084 |
|  | 12 | 0.924 | 0.8049 | 0.859505 | 0.750295 |  | 3 | 0.77 | 0.8029 | 0.857716 | 0.748084 |
|  | 14 | 0.845 | 0.8049 | 0.859219 | 0.750581 |  | 4 | 0.86 | 0.8029 | 0.857716 | 0.748084 |
|  | 17 | 0.638 | 0.8049 | 0.859679 | 0.750121 |  | 7 | 1.04 | 0.8029 | 0.857716 | 0.748084 |
|  | 18 | 0.844 | 0.8049 | 0.856346 | 0.753454 |  | 8 | 0.8 | 0.8029 | 0.857716 | 0.748084 |
|  | 19 | 0.87 | 0.8049 | 0.856736 | 0.753064 |  | 9 | 0.67 | 0.8029 | 0.857716 | 0.748084 |
|  | 21 | 0.808 | 0.8049 | 0.859447 | 0.750353 |  | 10 | 0.74 | 0.8029 | 0.857716 | 0.748084 |
|  | 22 | 0.816 | 0.8049 | 0.859505 | 0.750295 |  | 11 | 0.75 | 0.8029 | 0.857716 | 0.748084 |
|  | 28 | 0.802 | 0.8049 | 0.859737 | 0.750063 |  | 12 | 0.92 | 0.8029 | 0.857716 | 0.748084 |
|  | 29 | 0.909 | 0.8049 | 0.86033 | 0.74947 |  | 14 | 0.9 | 0.8029 | 0.857716 | 0.748084 |
|  | 30 | 0.529 | 0.8049 | 0.85962 | 0.75018 |  | 15 | 0.67 | 0.8029 | 0.857716 | 0.748084 |
|  |  |  |  |  |  |  | 17 | 0.8 | 0.8029 | 0.857716 | 0.748084 |
|  |  |  |  |  |  |  | 18 | 0.58 | 0.8029 | 0.857716 | 0.748084 |
|  |  |  |  |  |  |  | 19 | 0.92 | 0.8029 | 0.857716 | 0.748084 |
|  |  |  |  |  |  |  | 21 | 0.86 | 0.8029 | 0.857716 | 0.748084 |
|  |  |  |  |  |  |  | 22 | 0.85 | 0.8029 | 0.857716 | 0.748084 |
|  |  |  |  |  |  |  | 28 | 0.67 | 0.8029 | 0.857716 | 0.748084 |
|  |  |  |  |  |  |  | 29 | 0.74 | 0.8029 | 0.857716 | 0.748084 |
|  |  |  |  |  |  |  | 30 | 0.88 | 0.8029 | 0.857716 | 0.748084 |

## APPENDIX D

D1: Attribute Control Chart, p-chart Formula

| For finding average, Centreline: | $\bar{p}=\frac{\sum n p}{\sum n}$ |
| :--- | :--- |
| Upper Control Limit, UCL: | $U C L_{p}=\bar{p}+3 \sqrt{\frac{\bar{p}(1-\bar{p})}{n}}$ |
| Lower Control Limit, LCL: | $L C L_{p}=\bar{p}-3 \sqrt{\frac{\bar{p}(1-\bar{p})}{n}}$ |

## APPENDIX E

E1: Calculation for availability factor on July $1^{\text {st }} 2015$ for Shift A for existing condition

$$
\begin{aligned}
& \begin{aligned}
\bar{p} & =\frac{24136}{24357} \\
& =0.9909
\end{aligned} \\
& \begin{aligned}
U C L_{p} & =0.9909+3 \sqrt{\frac{0.9909(1-0.9909)}{474}} \\
& =1.0040
\end{aligned} \\
& \begin{aligned}
L C L_{p} & =0.9909-3 \sqrt{\frac{0.9909(1-0.9909)}{474}} \\
& =0.9778
\end{aligned}
\end{aligned}
$$

E2: Calculation for availability factor on July $1^{\text {st }} 2015$ for Shift A for $1^{\text {st }}$ revised condition

$$
\begin{aligned}
& \begin{aligned}
\bar{p} & =\frac{21379}{21453} \\
& =0.9966
\end{aligned} \\
& \begin{aligned}
U C L_{p} & =0.9966+3 \sqrt{\frac{0.9966(1-0.9966)}{474}} \\
& =1.0046
\end{aligned} \\
& \begin{aligned}
L C L_{p} & =0.9966-3 \sqrt{\frac{0.9966(1-0.9966)}{474}} \\
& =0.9886
\end{aligned}
\end{aligned}
$$

## APPENDIX F

F1: Revised Control Chart Data for Availability by Shifts

| shift A |  |  |  |  |  |  |  | shift B |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DAY | OPERATION time | PLANNED PRODUCTION TIME | AVAILABILITY <br> (p) | $\begin{aligned} & \text { CENTER } \\ & \text { (P-BAR) } \end{aligned}$ | UCL | LCL |  | DAY | OPERATION time | PLANNED PRODUCTION TIME | AVAILABILITY <br> (p) | $\begin{aligned} & \text { CENTER } \\ & \text { (P-BAR) } \end{aligned}$ | UCL | LCL |
| july | 1-Jul-15 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 | july | 1-Jul-15 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 2 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 2 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 3 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 3 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 6 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 6 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 7 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 7 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 8 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 8 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 9 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 9 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 10 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 10 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 11 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 11 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 13 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 13 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 14 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 14 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 22 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 22 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 23 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 23 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 24 | 472 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 24 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 28 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 27 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 29 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 28 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 30 | 465 | 474 | 0.98 | 0.9966 | 1.0046 | 0.9886 |  | 29 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
| august | 3-Aug-15 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 |  | 30 | 475 | 475 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 4 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 | august | 3-Aug-15 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 5 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 |  | 4 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 6 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 |  | 5 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 7 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 6 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 13 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 7 | 489 | 489 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 15 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 10 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 18 | 525 | 534 | 0.98 | 0.9966 | 1.0042 | 0.9890 |  | 11 | 576 | 576 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 19 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 |  | 13 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 20 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 14 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 21 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 |  | 15 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 22 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 17 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 24 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 18 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 26 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 18 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 27 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 20 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
| sept | 3-Sep-15 | 523 | 534 | 0.98 | 0.9966 | 1.0042 | 0.9890 |  | 21 | 489 | 489 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 10 | 466 | 474 | 0.98 | 0.9966 | 1.0046 | 0.9886 |  | 22 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 11 | 447 | 456 | 0.98 | 0.9966 | 1.0048 | 0.9884 |  | 24 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 12 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 25-Aug-15 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 14 | 479 | 484 | 0.99 | 0.9966 | 1.0045 | 0.9887 |  | 26 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 17 | 471 | 474 | 0.99 | 0.9966 | 1.0046 | 0.9886 |  | 27 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 18 | 534 | 534 | 1.00 | 0.9966 | 1.0042 | 0.9890 | sept | 1-Sep-15 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 19 | 526 | 534 | 0.99 | 0.9966 | 1.0042 | 0.9890 |  | 2 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 21 | 475 | 479 | 0.99 | 0.9966 | 1.0046 | 0.9886 |  | 3 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 22 | 474 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 4 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 28-Sep | 470 | 474 | 0.99 | 0.9966 | 1.0046 | 0.9886 |  | 7 | 489 | 489 | 1.00 | 0.999 | 1.00 | 1.00 |
|  | 30 | 472 | 474 | 1.00 | 0.9966 | 1.0046 | 0.9886 |  | 8 | 545 | 545 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 9 | 545 | 545 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 10 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 11-Sep | 576 | 576 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 12 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 14 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 15 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 18 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 19 | 534 | 534 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 21 | 489 | 489 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 22 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 29 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |
|  |  |  |  |  |  |  |  |  | 30 | 474 | 474 | 1.00 | 0.999 | 1.00 | 1.00 |

F2: Revised Control Chart Data for Performance by Shifts

| shift A |  |  |  |  |  |  |  | shift B |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DAY | NET OPERATION TIME (np) | OPERATION TIME ( n ) | $\begin{array}{\|c} \text { PERFORMAN } \\ \text { CE }(\mathrm{p}) \end{array}$ | CENTER P BAR | UCL | LCL |  | DAY | NET <br> OPERATION <br> TIME | PERATION TIM | $\begin{array}{\|c\|} \hline \text { PERFORMANC } \\ E(P) \end{array}$ | CENTER P <br> BAR | UCL | LCL |
| july | 1-Jul-15 | 395 | 474 | 0.833 | 0.8490 | 0.8983 | 0.7997 | july | 1-Jul-15 | 402 | 474 | 0.848 | 0.8287 | 0.8287 | 0.8287 |
|  | 2 | 395 | 474 | 0.833 | 0.8490 | 0.8983 | 0.7997 |  | 2 | 381 | 474 | 0.804 | 0.8287 | 0.8287 | 0.8287 |
|  | 7 | 409 | 474 | 0.863 | 0.8490 | 0.8983 | 0.7997 |  | 3 | 409 | 474 | 0.863 | 0.8287 | 0.8287 | 0.8287 |
|  | 13 | 381 | 474 | 0.804 | 0.8490 | 0.8983 | 0.7997 |  | 9 | 395 | 474 | 0.833 | 0.8287 | 0.8287 | 0.8287 |
|  | 14 | 395 | 474 | 0.833 | 0.8490 | 0.8983 | 0.7997 |  | 13 | 402 | 474 | 0.848 | 0.8287 | 0.8287 | 0.8287 |
|  | 22 | 409 | 474 | 0.863 | 0.8490 | 0.8983 | 0.7997 |  | 14 | 373 | 474 | 0.787 | 0.8287 | 0.8287 | 0.8287 |
|  | 23 | 402 | 474 | 0.848 | 0.8490 | 0.8983 | 0.7997 |  | 22 | 402 | 474 | 0.848 | 0.8287 | 0.8287 | 0.8287 |
|  | 24 | 402 | 472 | 0.852 | 0.8490 | 0.8984 | 0.7996 |  | 27 | 402 | 474 | 0.848 | 0.8287 | 0.8287 | 0.8287 |
|  | 27 | 373 | 463 | 0.806 | 0.8490 | 0.8989 | 0.7991 |  | 30 | 409 | 475 | 0.861 | 0.8287 | 0.8287 | 0.8287 |
|  | 28 | 402 | 474 | 0.848 | 0.8490 | 0.8983 | 0.7997 | august | 4 | 402 | 474 | 0.848 | 0.8287 | 0.8287 | 0.8287 |
|  | 29 | 402 | 474 | 0.848 | 0.8490 | 0.8983 | 0.7997 |  | 5 | 431 | 534 | 0.807 | 0.8287 | 0.8287 | 0.8287 |
|  | 30 | 395 | 465 | 0.849 | 0.8490 | 0.8988 | 0.7992 |  | 6 | 445 | 534 | 0.833 | 0.8287 | 0.8287 | 0.8287 |
| august | 5 | 474 | 534 | 0.888 | 0.8490 | 0.8955 | 0.8025 |  | 11 | 460 | 576 | 0.799 | 0.8287 | 0.8287 | 0.8287 |
|  | 6 | 445 | 534 | 0.833 | 0.8490 | 0.8955 | 0.8025 |  | 21 | 401 | 489 | 0.820 | 0.8287 | 0.8287 | 0.8287 |
|  | 10 | 373 | 448 | 0.833 | 0.8490 | 0.8997 | 0.7983 |  | 22 | 380 | 474 | 0.802 | 0.8287 | 0.8287 | 0.8287 |
|  | 20 | 422 | 474 | 0.890 | 0.8490 | 0.8983 | 0.7997 |  | 27 | 373 | 474 | 0.787 | 0.8287 | 0.8287 | 0.8287 |
| sept | 3-Sep-15 | 452 | 523 | 0.864 | 0.8490 | 0.8960 | 0.8020 | sept | 2 | 373 | 474 | 0.787 | 0.8287 | 0.8287 | 0.8287 |
|  | 10 | 395 | 466 | 0.848 | 0.8490 | 0.8988 | 0.7992 |  | 8 | 438 | 545 | 0.804 | 0.8287 | 0.8287 | 0.8287 |
|  | 14 | 409 | 479 | 0.854 | 0.8490 | 0.8981 | 0.7999 |  | 17 | 394 | 471 | 0.837 | 0.8287 | 0.8287 | 0.8287 |
|  | 17 | 401 | 471 | 0.851 | 0.8490 | 0.8985 | 0.7995 |  | 21 | 422 | 489 | 0.863 | 0.8287 | 0.8287 | 0.8287 |
|  | 22 | 401 | 474 | 0.846 | 0.8490 | 0.8983 | 0.7997 |  | 22 | 401 | 474 | 0.846 | 0.8287 | 0.8287 | 0.8287 |
|  | 28-Sep | 416 | 470 | 0.885 | 0.8490 | 0.8985 | 0.7995 |  | 28 | 394 | 452 | 0.872 | 0.8287 | 0.8287 | 0.8287 |

F3: Revised Control Chart Data for Quality by Shifts

| shift A |  |  |  |  |  |  |  | shift B |  |  |  |  |  |  |  |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  | DAY | $\begin{gathered} \hline \text { OK } \\ \text { PRODUCT } \\ \text { PER SHIFT } \\ (\mathrm{np}) \\ \hline \end{gathered}$ | total output PER SHIFT (n) | QUALITY (p) | $\begin{array}{\|l\|} \hline \text { CENTER } \\ \text { (P-BAR) } \end{array}$ | UCL | LCL |  | DAY | PRODUCT PER SHIFT | total output PER SHIFT | QUALITY (P) | $\begin{aligned} & \text { CENTER } \\ & (\mathrm{P}-\mathrm{BAR}) \end{aligned}$ | UCL | LCL |
| july | 1-Jul-15 | 53 | 55 | 0.964 | 0.9597 | 1.0393 | 0.8801 | july | 1-Jul-15 | 56 | 56 | 1.000 | 0.9777 | 1.0369 | 0.9185 |
|  | 2 | 54 | 55 | 0.982 | 0.9597 | 1.0393 | 0.8801 |  | 2 | 51 | 53 | 0.962 | 0.9777 | 1.0385 | 0.9169 |
|  | 3 | 50 | 50 | 1.000 | 0.9597 | 1.0431 | 0.8763 |  | 3 | 55 | 57 | 0.965 | 0.9777 | 1.0364 | 0.9190 |
|  | 6 | 58 | 60 | 0.967 | 0.9597 | 1.0359 | 0.8835 |  | 6 | 59 | 61 | 0.967 | 0.9777 | 1.0344 | 0.9210 |
|  | 7 | 56 | 57 | 0.982 | 0.9597 | 1.0378 | 0.8816 |  | 7 | 58 | 60 | 0.967 | 0.9777 | 1.0349 | 0.9205 |
|  | 8 | 57 | 63 | 0.905 | 0.9597 | 1.0340 | 0.8854 |  | 8 | 56 | 60 | 0.933 | 0.9777 | 1.0349 | 0.9205 |
|  | 9 | 47 | 50 | 0.940 | 0.9597 | 1.0431 | 0.8763 |  | 9 | 53 | 55 | 0.964 | 0.9777 | 1.0374 | 0.9180 |
|  | 10 | 48 | 50 | 0.960 | 0.9597 | 1.0431 | 0.8763 |  | 10 | 50 | 51 | 0.980 | 0.9777 | 1.0397 | 0.9157 |
|  | 11 | 50 | 52 | 0.962 | 0.9597 | 1.0415 | 0.8779 |  | 11 | 48 | 50 | 0.960 | 0.9777 | 1.0403 | 0.9151 |
|  | 13 | 53 | 53 | 1.000 | 0.9597 | 1.0407 | 0.8787 |  | 13 | 54 | 56 | 0.964 | 0.9777 | 1.0369 | 0.9185 |
|  | 14 | 54 | 55 | 0.982 | 0.9597 | 1.0393 | 0.8801 |  | 14 | 50 | 52 | 0.962 | 0.9777 | 1.0391 | 0.9163 |
|  | 22 | 55 | 57 | 0.965 | 0.9597 | 1.0378 | 0.8816 |  | 22 | 54 | 56 | 0.964 | 0.9777 | 1.0369 | 0.9185 |
|  | 23 | 54 | 56 | 0.964 | 0.9597 | 1.0385 | 0.8809 |  | 23 | 50 | 50 | 1.000 | 0.9777 | 1.0403 | 0.9151 |
|  | 24 | 55 | 56 | 0.982 | 0.9597 | 1.0385 | 0.8809 |  | 24 | 51 | 51 | 1.000 | 0.9777 | 1.0397 | 0.9157 |
|  | 27 | 52 | 52 | 1.000 | 0.9597 | 1.0415 | 0.8779 |  | 27 | 56 | 56 | 1.000 | 0.9777 | 1.0369 | 0.9185 |
|  | 28 | 56 | 56 | 1.000 | 0.9597 | 1.0385 | 0.8809 |  | 28 | 47 | 50 | 0.940 | 0.9777 | 1.0403 | 0.9151 |
|  | 29-Jul-15 | 54 | 56 | 0.964 | 0.9597 | 1.0385 | 0.8809 |  | 29 | 50 | 50 | 1.000 | 0.9777 | 1.0403 | 0.9151 |
|  | 30 | 54 | 55 | 0.982 | 0.9597 | 1.0393 | 0.8801 |  | 30 | 50 | 50 | 1.000 | 0.9777 | 1.0403 | 0.9151 |
| august | 3-Aug-15 | 68 | 70 | 0.971 | 0.9597 | 1.0302 | 0.8892 | august | 3-Aug-15 | 68 | 70 | 0.971 | 0.9777 | 1.0306 | 0.9248 |
|  | 4 | 57 | 58 | 0.983 | 0.9597 | 1.0372 | 0.8822 |  | 4 | 55 | 56 | 0.982 | 0.9777 | 1.0369 | 0.9185 |
|  | 5 | 64 | 66 | 0.970 | 0.9597 | 1.0323 | 0.8871 |  | 5 | 58 | 60 | 0.967 | 0.9777 | 1.0349 | 0.9205 |
|  | 6-Aug | 61 | 62 | 0.984 | 0.9597 | 1.0346 | 0.8848 |  | 6 | 61 | 62 | 0.984 | 0.9777 | 1.0340 | 0.9214 |
|  | 7 | 58 | 62 | 0.94 | 0.9597 | 1.0346 | 0.8848 |  | 7 | 58 | 61 | 0.95 | 0.978 | 1.03 | 0.92 |
|  | 10 | 49 | 52 | 0.94 | 0.9597 | 1.0415 | 0.8779 |  | 10 | 51 | 53 | 0.96 | 0.978 | 1.04 | 0.92 |
|  | 13 | 60 | 64 | 0.94 | 0.9597 | 1.0334 | 0.8860 |  | 11 | 62 | 64 | 0.97 | 0.978 | 1.03 | 0.92 |
|  | 15 | 45 | 50 | 0.90 | 0.9597 | 1.0431 | 0.8763 |  | 13 | 64 | 66 | 0.97 | 0.978 | 1.03 | 0.92 |
|  | 17 | 52 | 58 | 0.90 | 0.9597 | 1.0372 | 0.8822 |  | 14 | 65 | 67 | 0.97 | 0.978 | 1.03 | 0.92 |
|  | 18 | 48 | 50 | 0.96 | 0.9597 | 1.0431 | 0.8763 |  | 15 | 49 | 50 | 0.98 | 0.978 | 1.04 | 0.92 |
|  | 19 | 53 | 56 | 0.95 | 0.9597 | 1.0385 | 0.8809 |  | 17 | 37 | 38 | 0.97 | 0.978 | 1.05 | 0.91 |
|  | 20 | 57 | 60 | 0.95 | 0.9597 | 1.0359 | 0.8835 |  | 18 | 46 | 48 | 0.96 | 0.978 | 1.04 | 0.91 |
|  | 21 | 66 | 70 | 0.94 | 0.9597 | 1.0302 | 0.8892 |  | 18 | 47 | 48 | 0.98 | 0.978 | 1.04 | 0.91 |
|  | 22 | 64 | 66 | 0.97 | 0.9597 | 1.0323 | 0.8871 |  | 20 | 57 | 60 | 0.95 | 0.978 | 1.03 | 0.92 |
|  | 24-Aug-15 | 61 | 63 | 0.97 | 0.9597 | 1.0340 | 0.8854 |  | 21 | 56 | 57 | 0.98 | 0.978 | 1.04 | 0.92 |
|  | 25 | 59 | 61 | 0.97 | 0.9597 | 1.0352 | 0.8842 |  | 22 | 52 | 54 | 0.96 | 0.978 | 1.04 | 0.92 |
|  | 26 | 62 | 65 | 0.95 | 0.9597 | 1.0329 | 0.8865 |  | 24 | 65 | 67 | 0.97 | 0.978 | 1.03 | 0.92 |
|  | 27 | 45 | 50 | 0.90 | 0.9597 | 1.0431 | 0.8763 |  | 25-Aug-15 | 65 | 67 | 0.97 | 0.978 | 1.03 | 0.92 |
| sept | 3-Sep-15 | 62 | 63 | 0.98 | 0.9597 | 1.0340 | 0.8854 |  | 26 | 69 | 70 | 0.99 | 0.978 | 1.03 | 0.92 |
|  | 4 | 45 | 50 | 0.90 | 0.9597 | 1.0431 | 0.8763 |  | 27 | 50 | 53 | 0.94 | 0.978 | 1.04 | 0.92 |
|  | 10 | 55 | 55 | 1.00 | 0.9597 | 1.0393 | 0.8801 | sept | 1-Sep-15 | 48 | 48 | 1.00 | 0.978 | 1.04 | 0.91 |
|  | 11 | 46 | 46 | 1.00 | 0.9597 | 1.0467 | 0.8727 |  | 2 | 52 | 52 | 1.00 | 0.978 | 1.04 | 0.92 |
|  | 12 | 61 | 61 | 1.00 | 0.9597 | 1.0352 | 0.8842 |  | 3 | 57 | 57 | 1.00 | 0.978 | 1.04 | 0.92 |
|  | 14 | 57 | 57 | 1.00 | 0.9597 | 1.0378 | 0.8816 |  | 4 | 57 | 60 | 0.95 | 0.978 | 1.03 | 0.92 |
|  | 18-Sep | 64 | 70 | 0.91 | 0.9597 | 1.0302 | 0.8892 |  | 7 | 71 | 71 | 1.00 | 0.978 | 1.03 | 0.93 |
|  | 19 | 66 | 71 | 0.93 | 0.9597 | 1.0297 | 0.8897 |  | 8 | 61 | 61 | 1.00 | 0.978 | 1.03 | 0.92 |
|  | 21 | 55 | 61 | 0.90 | 0.96 | 1.04 | 0.88 |  | 9 | 51 | 52 | 0.98 | 0.978 | 1.04 | 0.92 |
|  | 22 | 55 | 57 | 0.96 | 0.96 | 1.04 | 0.88 |  | 10 | 55 | 56 | 0.98 | 0.978 | 1.04 | 0.92 |
|  | 28-Sep-15 | 53 | 58 | 0.91 | 0.96 | 1.04 | 0.88 |  | 11-Sep | 60 | 60 | 1.00 | 0.978 | 1.03 | 0.92 |
|  | 29 | 60 | 60 | 1.00 | 0.96 | 1.04 | 0.88 |  | 12 | 61 | 62 | 0.98 | 0.978 | 1.03 | 0.92 |
|  |  |  |  |  |  |  |  |  | 14 | 67 | 67 | 1.00 | 0.978 | 1.03 | 0.92 |
|  |  |  |  |  |  |  |  |  | 15 | 44 | 44 | 1.00 | 0.978 | 1.04 | 0.91 |
|  |  |  |  |  |  |  |  |  | 17 | 54 | 56 | 0.96 | 0.978 | 1.00 | 0.95 |
|  |  |  |  |  |  |  |  |  | 18 | 44 | 44 | 1.00 | 0.978 | 1.00 | 0.95 |
|  |  |  |  |  |  |  |  |  | 19 | 70 | 70 | 1.00 | 0.978 | 1.00 | 0.95 |
|  |  |  |  |  |  |  |  |  | 21 | 60 | 60 | 1.00 | 0.978 | 1.00 | 0.95 |
|  |  |  |  |  |  |  |  |  | 22 | 57 | 57 | 1.00 | 0.978 | 1.00 | 0.95 |
|  |  |  |  |  |  |  |  |  | 29 | 50 | 50 | 1.00 | 0.978 | 1.00 | 0.95 |
|  |  |  |  |  |  |  |  |  | 30 | 59 | 61 | 0.967 | 0.978 | 1.003 | 0.952 |

