

## Bandwidth and gain enhancement of a circular microstrip antenna using a DNG split ring resonator radome

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### ABSTRACT

This paper present the design of a circular patch microstrip antenna with enhancement in terms of bandwidth and gain using a dielectric double negative (DNG) split ring metamaterial radome. This radome is positioned on top of the CP antenna operating from 5.2 GHz to 6.4 GHz. The metamaterial radome comprises of two alternate split rings of negative permittivity, permeability and refractive index. The circular microstrip antenna bandwidth of 430 MHz has been realized by the presence of DNG metamaterial radome compared to 220 MHz without the radome. The gain has been increased as well from 1.84 dBi to 3.87 dBi.

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## 1. INTRODUCTION

The enhancement of microstrip antennas using radomes enhances their practical application, besides protecting them from different environmental effects such as wind, rain, ice, ultraviolet radiation etc. Radome can be of different shapes such as spherical, geodesic, planar etc., dependings on the application (radar, telemetry, tracking, and point-to-point). They can be designed using different types of low losses materials, for example fiberglass, and coated using PTFE- for indoor and outdoor environments [1], However, the main challenge for designing radome is avoiding antenna degradation in terms of attenuation, scattering and depolarization. Furthermore, scattered radiation from the use of radomes may degrade antenna performance in terms of antenna directivity via the enhancement of side lobes [2], The main disadvantages of the microstrip patch antenna are narrower band and low gain [3], Due to these factors, many researches have investigated methods to improve the bandwidth and antenna gain by modifying the ground plane orradiating patch [4-5].

A different types of artificial magnetic conductor has been used to design radome as-partially reflecting surfaces, or frequency selective surfaces. Metamaterial-based radomes can be great addition to microstrip antennas due to the unusual electromagnetic properties that they are able to provide [6-7], Metamaterial attains exotic electromagnetic property over certain frequency band, which is abnormal in nature. It can show totally opposite characteristics compared to natural materials in terms of negative permittivity or permeability [8], An axial symmetrical CRLH circular patch antenna was proposed to support the zeroth order mode metamaterial [9], MNZ or MNG metamaterial in the central part of circular patch

would increase the resonant frequency of mode TM<sub>11</sub> while keeping the frequency of mode TM<sub>21</sub> unchanged, and there would be increment of bandwidth by enlarged if they are so close to connect two band together [10]. A compact low-profile dual-band patch antenna in which designed by inserting an array of the TL-MTM unit cell into the conventional microstrip patch. a compact single-layer dual-band patch antenna design. The TL-MTM unit cell has advantages for antenna design such as small size and aperture enhancement [11], the using ENZ MTM as a dielectric substrate remarkably improved the antenna impedance bandwidth. Such super-bandwidth phenomenon is demonstrated experimentally by exploiting the intrinsic dispersion characteristic of metallic wires inspired in a dielectric substrate [12], TL metamaterial is derived to analyze this circular antenna. Since the unit cells of this TL can reinforce unpredictable phase shift, the antenna can form negative modes, positive modes and zeroth-order resonant (ZOR) modes. For a ZOR antenna, the resonant frequency is independent of its physical size. The resonant frequency, input impedance and radiation characteristics of the ZOR circular antenna are analyzed in terms of the physical parameters of the unit cells [13], a compact triple-band microstrip antenna based on MTM complementary split ring resonator (CSRR) with two different geometries loaded on the ground plane of the antenna. MTM lens that is created by a modified H-shape unit cells. A MTM metamaterial super lens positioned at the focal point above the patch is introduced using a novel complementary H-shaped unit cells to maximize the gain and mounted on the overall antenna structure.

This work explores the design of such metamaterial split, ring radome for a circular patch antenna operating at 5.8 GHz. A method is used to extract the effective permeability, refractive index, and impedance from S-parameter to analyze whether the metamaterial structure is also DNG at the same frequency.

However, another advantages of using Double Negative (DNG) Split Ring Resonator (SRR) radome. Some research are going on to improve the bandwidth and gain of patch antenna. Existing solutions leads to the problems of specious radiation and high complexity. This new approach come up with a new solution called metamaterial radome, which play an important role in the antenna design due to its interesting and unusual properties.

## 2. ANTENNA DESIGN AND UNIT CELL RADOME

Explaining In this proposed work, a circular patch microstrip antenna resonating at 5.8 GHz designed. The crucial inconvenience of a microstrip antenna is its narrow bandwidth. Thus, Double Negative (DNG) Split Ring Resonator (SRR) radome is designed to focus on enhancing the bandwidth and gain by achieving the maximum efficiency. Circular patch antenna is chosen since due to the less complexity compared to rectangular patch antenna since it has only one parameter to control i.e. radius. Circular patch antenna ha's been designed based on (1):

Circular Patch Radius

$$\alpha = \frac{F}{\left\{1 + \frac{2h}{\pi F \epsilon_r} \left[ \ln \left( \frac{\pi F}{2h} \right) + 1.7726 \right] \right\}^{1/2}} \quad (1)$$

Where;

$$F = \frac{8.791 \times 10^9}{f_r \sqrt{\epsilon_r}} \quad (2)$$

The complete structure of proposed antenna radome is etched using FR4 substrate  $\epsilon_r=4.3$  with dimension of 56 x 56 mm, and a dielectric thickness of =1.6 mm. Figure 1(a) shows the perspective view of the circular patch antenna with radius of the patch denotes as 'a' while thickness of the dielectric substrate notifies by 'h'. Figure 1(b) and (c) show the front and back view of circular patch microstrip antenna respectively. Figure 2(a) presents the DNG-SRR structure where the permittivity and permeability is in negative scale ranging from 2 to 8 GHz. Figure 2(b) illustrates the complete simulation setup of proposed structure where the circular antenna has been covered by the DNG-SRRs which act as radome. The detailed dimensions of the proposed structure is given in Table 1.

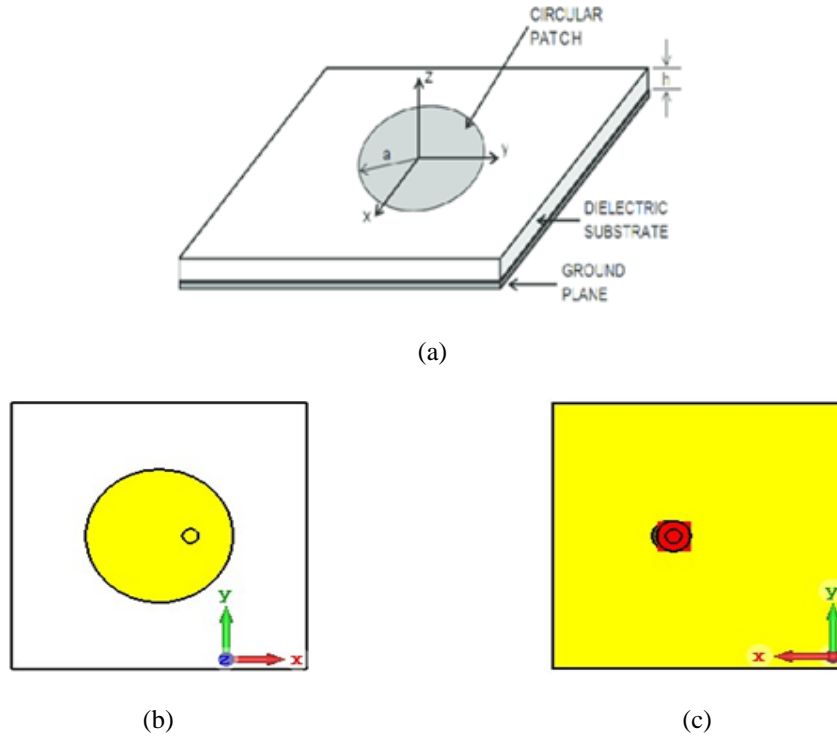


Figure 1. Design of circular patch antenna, (a) perspective view, (b) front view, (c) back view

Table 1. The specification of proposed antenna and radome

Parameters	Unit (mm)	Parameters	Unit (mm)
L	56	L	4.4
W	56	W	12.5
Radius CP	5.9	b	0.27
Frequency	5.8GHz	w	3.9
Sub. Material	FR4	g	0.3
Permittivity.	$\epsilon_r=4.3$		
Sub. Thick.	1.6		

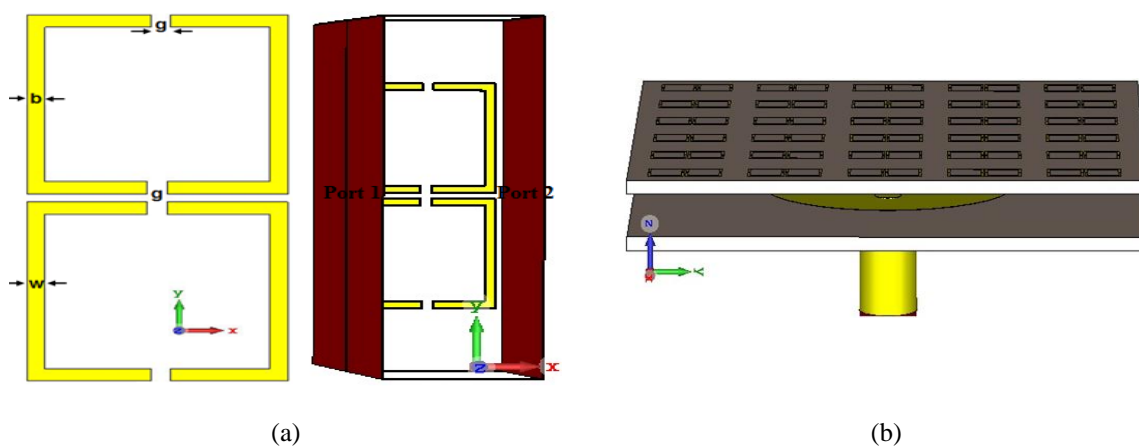


Figure 2. Proposed antenna structure, (a) DNG-SRR unit cell, (b) DNG-SRRs located on top of circular patch antenna

The negative permittivity and permeability of the structure that are obtained from the simulated complex value of S-parameters of Transmission Reflection (TR) technique of electromagnetic radiation at the boundary between two surfaces. Next, Nicolson-Ross-Weir (NRW) technique is deployed to find negative

values of permittivity and permeability [14]. The negative values of permittivity and permeability are retrieved by exporting the scattering parameters ( $S_{11}$ , and  $S_{21}$ ) to MATLAB using the following equations [15-16],

$$\varepsilon = n/\zeta \quad (3)$$

$$\mu = n\zeta \quad (4)$$

where

$$n = \frac{1}{ka} \cos^{-1} \left[ \frac{1}{2S_{21}} (1 - S_{11}^2 + S_{21}^2) \right] \quad (5)$$

$$\zeta = \sqrt{\frac{(1+S_{11})^2 - S_{21}^2}{(1+S_{11})^2 - S_{21}^2}} \quad (6)$$

### 3. RESULTS AND ANALYSIS

In this section, it is explained the results of research and at the same time is given the comprehensive discussion. Results can be presented in graphs, DNG-SRR radome structure with the circular patch antenna is simulated using CST Microwave Studio electromagnetic simulator. Figure 3 (a)-(d) present the relative permittivity, permeability, refractive index and impedance of the unit cell of DNG-SRR. This unit cell array have been applied on top of circular patch antenna in 5 mm distance.

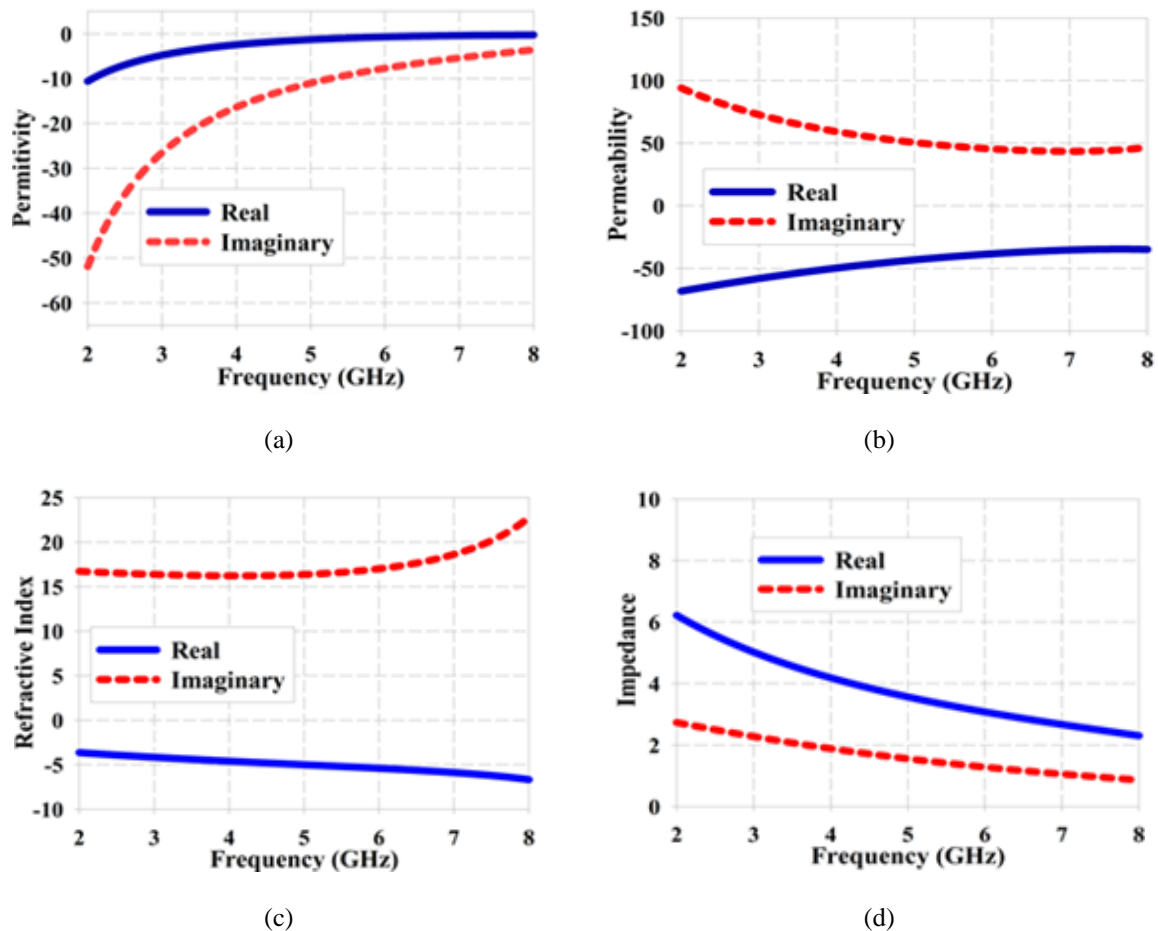


Figure 3. Characterization of DNG-SRR unit cell, (a) Permittivity, (b) Permeability, (c) Refractive index, (d) Impedance

Figure 3(a) and (b) proven that the SRR-based unit cell of SRR is a double negative (DNG) unit cell since both negative permittivity and negative permeability are stated in a negative Y-axis for both parameters. These figures give substantiation results of a negative behavior of the periodic structure, which simulation of negative permittivity and permeability shows good compliance. Meanwhile negative refractive index and positive impedance is shown in Figure 3(c) and (d). The resulting bandwidth and gain of the final antenna is illustrated in Figure 4 and 5 respectively. The enhancement of bandwidth is observed to be 210 MHz while gain is observed to be 3.9 dB at 5.8GHz.

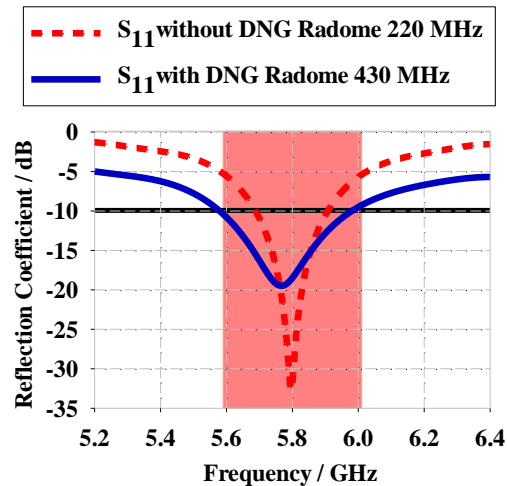


Figure 4. Effects of DNG-SRRs S11 comparison between with and without radome

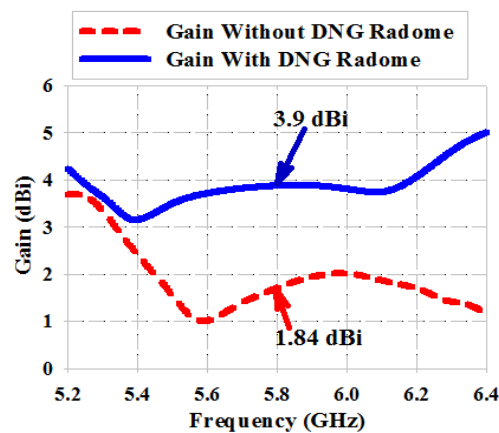


Figure 5. The effects of Gain comparison between with and without radome

#### 4. CONCLUSION

Provide The paper concludes that DNG-SRRs could increase the antenna gain and bandwidth, which could be useful for antenna radome applications. The features of negative permeability, permittivity and refractive index, in which produced using MATLAB from Transmission Reflection (T/R) technique using direct retrieval method from simulated S11 and S21 is contributed by the DNG-SRRs, which placed on the top of circular patch microstrip antenna. The S11 shows a 7.43% of bandwidth with DNG metamaterial radome. Gain of 3.9 dB has been realized by the presence of DNG-SRRs radome compared to 1.84 dB of without the radome.

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