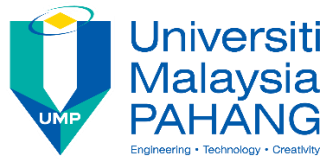


MATHEMATICAL MODELLING OF
PIPELINE COMPOSITE REPAIR DESIGN
USING FINITE ELEMENT ANALYSIS
INCORPORATING PUTTY'S
CONTRIBUTION

SIM YU LING

B. ENG (HONS.) CIVIL ENGINEERING

UNIVERSITI MALAYSIA PAHANG



SUPERVISOR'S DECLARATION

I hereby declare that I have checked this thesis and in my opinion, this thesis is adequate in terms of scope and quality for the award of the Bachelor Degree of Civil Engineering.

(Supervisor's Signature)

Full Name : DR. LIM KAR SING
Position : SENIOR LECTURER
Date :



STUDENT'S DECLARATION

I hereby declare that the work in this thesis is based on my original work except for quotations and citations which have been duly acknowledged. I also declare that it has not been previously or concurrently submitted for any other degree at Universiti Malaysia Pahang or any other institutions.

(Student's Signature)

Full Name : SIM YU LING

ID Number : AA15293

Date :

MATHEMATICAL MODELLING OF PIPELINE COMPOSITE REPAIR
DESIGN USING FINITE ELEMENT ANALYSIS INCORPORATING PUTTY'S
CONTRIBUTION

SIM YU LING

Thesis submitted in fulfillment of the requirements
for the award of the
Bachelor Degree in Civil Engineering

Faculty of Civil Engineering and Earth Resources
UNIVERSITI MALAYSIA PAHANG

JANUARY 2019

ACKNOWLEDGEMENTS

First and foremost, I would like to express my deepest sense of gratitude to my supervisor, Dr. Lim Kar Sing for his invaluable guidance, continuous encouragement and constant support throughout the period of my research work. I appreciate all the knowledge and guidance that have been shared, together with the support given to me to complete this research.

Secondly, my heartiest thanks goes to my parents for their love and sacrifice throughout my life. I acknowledge the sincerity of my parents, who have consistently encouraged me to pursue higher education which was crucial for the successful completion of this study.

Last but not least, I would like to highlight my thanks to my friends too. I am grateful for their continuous support and encouragement throughout my study life.

ABSTRAK

Sistem pembaikan komposit yang terdiri daripada penggunaan komposit polimer diperkuat gentian (*FRP*) dan isian pakal-pakal telah terbukti efektif dalam membaiki talian paip keluli yang mengalami kerosakan. Walau bagaimanapun, kajian terdahulu termasuk kod dan piawaian reka bentuk telah mengabaikan sumbangan daripada pakal kerana mereka menganggap pakal hanya berfungsi untuk mengisi bahagian yang berkarat dan memindahkan beban daripada paip ke pambalut komposit. Ini telah membataskan usaha untuk meneroka sumbangan pakal dan prestasi pambalut komposit telah menjadi tumpuan utama dalam kajian terdahulu. Satu kajian yang baru-baru ini telah menunjukkan bahawa pakal tidak hanya terhad untuk memindahkan beban, tetapi ia juga berpotensi sebagai komponen galas beban. Oleh itu, kajian ini bertujuan untuk memodelkan sumbangan pakal dari segi keupayaan galas beban melalui analisis unsur terhingga (*FEA*) dan pemodelan matematik. Dua model FE telah digunakan untuk mengkaji prestasi dua pakal yang berbeza sifat bahan yang digunakan untuk membaiki paip yang berkarat luaran diikuti dengan analisis regresi. Hubungan antara tekanan letus paip dan pengagihan beban antara paip keluli, pambalut komposit dan pakal telah dikaji. Keputusan ujian menunjukkan bahawa penggunaan pakal yang berbeza sifat mempunyai pengaruh yang besar terhadap sifat dan seterusnya prestasi keseluruhan paip pembaikan komposit. Bagi pakal yang mempunyai kekuatan tegangan yang tinggi, ia dapat meningkatkan kapasiti letus paip yang diperbaiki dengan memberikan pengukuhan tambahan manakala pakal yang mempunyai modulus tegangan yang tinggi dapat mengurangkan perubahan bentuk. Di samping itu, didapati bahawa dengan mengambilkira sumbangan kekuatan pakal, terdapat potensi untuk meningkatkan tekanan letus paip sebanyak 5%. Penemuan dalam kajian ini adalah penting kerana ia memberikan pemahaman yang komprehensif tentang sumbangan pakal dari segi keupayaan galas beban dalam paip pembaikan komposit di mana sumbangannya telah dikuantitikan dengan menggunakan dua jenis pakal yang berbeza sifat. Maka, kemasukan sumbangan kekuatan pakal harus diambil kira dalam penyelesaian tertutup reka bentuk pembaikan komposit. Ini boleh digunakan sebagai satu batu loncatan ke arah pengoptimuman reka bentuk pembaikan paip, seperti meminimumkan penggunaan pambalut komposit dan kemudiannya pembaikan tanpa pambalut komposit.

ABSTRACT

A composite repair system which consists of Fibre Reinforced Polymer (FRP) and putty as infill material has been proven effective in repairing pipeline system. However, previous studies including the design codes and standards are neglecting the contribution of putty as they assume putty is only functioned to fill the corroded section and to transfer loads from damaged pipeline to composite wrap. This has restricted the efforts to explore the contribution of putty that performance of wrapper became the main focus in the past research works. A recent study has pointed out that putty is not only limited to transfer the load, but it has the potential to serve as a load bearing component. Therefore, this research is aimed to model the contribution of putty in terms of load bearing capacity through finite element analysis (FEA) and mathematical modelling. Two finite elements models were utilized to study the performance of two different material properties of putties used to repair externally corroded pipeline followed by regression analysis. The relationship between burst pressure and stress distribution of steel, composite wrap and putty are investigated. Results revealed that different properties of putty have great influence upon the behaviour and subsequently the overall performance of a composite repaired pipe. A high tensile strength putty can increase the burst capacity that a repaired pipe can withstand by providing additional reinforcement while high tensile modulus of putty can help to reduce the deformation. In addition, it was found that by incorporating the strength contribution of putty, there are potential to increase the burst pressure by about 5%. The finding of this research is significant as it provides comprehensive understanding on the contribution of putty in terms of load bearing capacity in composite repaired pipeline where its contribution has been quantified with two different properties of putties. Hence, the inclusion of strength contribution of putty should be taken into account in the closed-form solution of composite repair design. This can serve as a stepping stone towards design optimization of pipeline rehabilitation, such as minimizing the usage of composite wrap and subsequently repair without composite wrap.

TABLE OF CONTENT

DECLARATION	
TITLE PAGE	
ACKNOWLEDGEMENTS	ii
ABSTRAK	iii
ABSTRACT	iv
TABLE OF CONTENT	v
LIST OF TABLES	viii
LIST OF FIGURES	ix
LIST OF SYMBOLS	x
LIST OF ABBREVIATIONS	xi
CHAPTER 1 INTRODUCTION	1
1.1 Overview	1
1.2 Research Background	2
1.3 Problem Statement	3
1.4 Research Objectives	5
1.5 Scope of Study	6
1.6 Significance of Study	6
CHAPTER 2 LITERATURE REVIEW	8
2.1 Introduction	8
2.2 Overview	8
2.3 Conventional Pipeline Repair Technique	10

2.4	Pipeline Repair Systems Using Composite	12
2.4.1	Composite Repair System	13
2.5	Infill materials	17
2.6	FRP Repair Design Codes and Practices	18
2.7	Future Trends in Composite Repair	21
2.8	Current Gaps in FRP Composite Pipeline Repair	23
2.9	Concluding Remark	27
CHAPTER 3 RESEARCH METHODOLOGY		29
3.1	Introduction	29
3.2	Overview of Overall Research Methodology	29
3.3	Stage 1: Finite Element Modelling Data Collection	32
3.4	Stage 2: Mathematical Modelling of Closed-form Equation	33
3.4.1	Design of Base Model: Establishment of Mathematical Model of Composite Repair Design	34
3.4.2	Design of Validation Model: Validation of Established Matheamtical Model	37
3.5	Concluding Remark	39
CHAPTER 4 RESULTS AND DISCUSSIONS		41
4.1	Introduction	41
4.2	Relationship between Hydrostatic Burst Pressure and Stress Distribution of Steel, Composite Wrap and Putty	41
4.3	Design of Base Model	43
4.4	Result of Base Model with Contribution of Putty	44
4.4.1	Model 1: Full Range	44
4.4.2	Model 2: Yield Strength of Steel	46

4.4.3	Model 3: Yield Stress Composite Repaired Pipe	48
4.4.4	Comparison between Model 1, Model 2 and Model 3	50
4.5	Result of Base Model without Contribution of Putty	51
4.5.1	Model 4: Full Range	51
4.5.2	Model 5: Yield Strength of Steel	53
4.5.3	Model 6: Yield Stress Composite Repaired Pipe	55
4.6	Comparison between Base Models of with and without Putty	57
4.7	Design of Validation Model	59
4.8	Result of Validation Model with Contribution of Putty	60
4.8.1	Model 7: Full Range	60
4.8.2	Model 8: Yield Strength of Steel	61
4.8.3	Model 9: Yield Stress Composite Repaired Pipe	62
4.9	Result of Validation Model without Contribution of Putty	63
4.9.1	Model 10: Full Range	63
4.9.2	Model 11: Yield Strength of Steel	64
4.9.3	Model 12: Yield Stress Composite Repaired Pipe	65
4.10	Comparison between Validation Models of with and without Putty	66
4.11	Understanding the Contribution of Putty	68
4.12	Concluding Remark	69
CHAPTER 5 CONCLUSION AND RECOMMENDATIONS		71
5.1	Overview	71
5.2	Conclusions	72
5.3	Significance of Research Contribution	72
5.4	Recommendations	73
REFERENCES		75

LIST OF TABLES

Table 2.1	Typical properties of epoxy grout for repair and rehabilitation (Source: Mendis, 1985)	22
Table 3.1	Material properties of steel, composite wrap and putties	33
Table 3.2	Input of modelling of base model	36
Table 4.1	Regression output part 1 of Model 1	45
Table 4.2	Regression output part 2 of Model 1	45
Table 4.3	Regression output part 1 of Model 2	47
Table 4.4	Regression output part 2 of Model 2	47
Table 4.5	Regression output part 1 of Model 3	49
Table 4.6	Regression output part 2 of Model 3	49
Table 4.7	Comparison between Model 1, Model 2 and Model 3	51
Table 4.8	Regression output part 1 of Model 4	52
Table 4.9	Regression output part 2 of Model 4	52
Table 4.10	Regression output part 1 of Model 5	54
Table 4.11	Regression output part 2 of Model 5	54
Table 4.12	Regression output part 1 of Model 6	56
Table 4.13	Regression output part 2 of Model 6	56
Table 4.14	Comparison between base models of with and without putty	59
Table 4.15	Percentage difference between base models of with and without putty	59
Table 4.16	Comparison between validation models of with and without putty	67
Table 4.17	Percentage difference between validation models of with and without putty	67

LIST OF FIGURES

Figure 2.1	Full encirclement steel sleeve	10
Figure 2.2	Type A steel sleeve (left) and Type B steel sleeve (right)	11
Figure 2.3	Typical mechanical bolt on clamp	11
Figure 2.4	Clock Spring® FRP composite repair system (Source: The Clock Spring Company, 2012)	14
Figure 2.5	ProAssure™ Wrap (Source: Index Pioneer Technologies Sdn Bhd, 2018)	15
Figure 2.6	ProAssure™ Clamp (Source: Merit Technologies Sdn Bhd, 2018)	16
Figure 2.7	Wrapping process of Kevlar tape repair system (Source: 3X Engineering, 2018)	17
Figure 2.8	Load transfer mechanism (Source: Freire <i>et al.</i> , 2007)	18
Figure 3.1	Flowchart of overall research methodology	31
Figure 3.2	Schematic drawing of corroded pipe specimen	33
Figure 3.3	Flowchart of design for base model	37
Figure 3.4	Flowchart of design for validation model	39
Figure 4.1	Stress versus applied pressure of finite element analysis base model	43
Figure 4.2	Actual versus predicted pressure of Model 1	46
Figure 4.3	Actual versus predicted pressure of Model 2	48
Figure 4.4	Actual versus predicted pressure of Model 3	50
Figure 4.5	Actual versus predicted pressure of Model 4	53
Figure 4.6	Actual versus predicted pressure of Model 5	55
Figure 4.7	Actual versus predicted pressure of Model 6	57
Figure 4.8	Actual versus predicted pressure of Model 7	61
Figure 4.9	Actual versus predicted pressure of Model 8	62
Figure 4.10	Actual versus predicted pressure of Model 9	63
Figure 4.11	Actual versus predicted pressure of Model 10	64
Figure 4.12	Actual versus predicted pressure of Model 11	65
Figure 4.13	Actual versus predicted pressure of Model 12	66

LIST OF SYMBOLS

D	Diameter of pipe
E	Young's modulus
E_c	Tensile modulus of composite laminate (in circumferential direction)
E_s	Tensile modulus of pipe
P	Pressure
P_{live}	Live pressure
P_s	Maximum allowable operating pressure
P_{yield}	Internal pressure of the substrate pipe at yield
R^2	R Square
S	Yield strength in substrate pipe
t	Thickness of pipe, composite wrap and putty
t_{min}	Minimum repair thickness
t_s	Minimum remaining wall thickness
x_i, x_{ii}, x_{iii}	Independent variables
y	Dependent variable
ε	Strain
ε_c	Design allowable strain of composite
$\varepsilon_{elastic}$	Elastic strain
$\varepsilon_{plastic}$	Plastic strain
σ	Stress
σ_c	Composite wrap stress
σ_h	Hoop stress
σ_p	Putty stress
σ_s	Steel stress

LIST OF ABBREVIATIONS

DGEBA	Diglycidyl ether of bisphenol-A
Eq.	Equation
FEA	Finite element analysis
FRP	Fibre reinforced polymer
HES	Helicoid epoxy sleeve
IMPACT	International Measures of Prevention, Application and Economics of Corrosion Technology
MAOP	Maximum allowable operating pressure
MLR	Multiple linear regression
RGTSU	Regasification Terminal Sungai Udang
SMYS	Specific Minimum Yield Strength
USDOT PHMSA	U.S. Department of Transportation Pipeline and Hazardous Materials Safety Administration
VSD	Volumetric Surface defects

CHAPTER 1

INTRODUCTION

1.1 Overview

In the oil and gas industry, steel pipelines are regarded as the most effective, economic and safest way of transporting crude oil, natural gas and liquid petroleum products over a long distance (Kishawy & Gabbar, 2010; Shamsuddoha *et al.*, 2013a; Abdul Jalil *et al.*, 2016). Owing to this reason, provision of their continuous work and accident-free operation is utmost essential (Barkanov *et al.*, 2018). However, these pipelines are subjected to damage and deterioration throughout their service life. These damages are generally caused by several factors, which include material and construction defects, natural forces, corrosion and also third parties' excavation (Kishawy & Gabbar, 2010; Azraai *et al.*, 2015). Referring to the U.S. Department of Transportation Pipeline and Hazardous Materials Safety Administration (USDOT PHMSA), it can be summarized that about 21% of recent oil pipeline failures in the United States are caused by corrosion (Haladuick & Dann, 2018). Hence, a damaged pipeline can be very dangerous as it tends to reduce the strength of the steel pipelines and eventually its intended service life. This issue has become a big headache for the oil and gas industry since it can lead to pipeline failures such as loss of structural integrity, fire, explosion and leakage. All these failures require a significant amount of cost while bringing much inconvenience towards the industry and public as well.

As reported by NACE International in their two years of global study, International Measures of Prevention, Application, and Economics of Corrosion Technology (IMPACT), the global cost of corrosion is approximated at \$2.5 trillion (NACE International, 2016). In addition, the average annual corrosion-related cost is estimated at \$7 billion to monitor, replace, and maintain these gas and liquid transmission pipelines. The corrosion-related cost of operation and maintenance makes up 80% of this

cost (Koch *et al.*, 2002). In 2013, an explosion of an underground pipeline in Qingdao in eastern China killed at least 62 people and injured 136 which was caused by an ignition of vapours produced from oil leakage from a corroded underground pipeline (NACE International, 2014). Saeed *et al.* (2014) revealed that more than 60% of the pipelines from all over the world have been in service for more than 40 years. Even in our own country, Malaysia, Petronas Gas Berhad (2014) reported that more than 35% of the local onshore pipelines are more than 30 years old. In short, it can be concluded that there is an urge to repair all these pipelines so as to recover their desired operating capacity and to restore their in service performance. Hence, pipeline failure due to corrosion that can have large social, economic, and environmental consequences has gained attention from researchers worldwide and so its repair technique is kind of their main interest to ensure the pipelines are in good working condition (Shamsuddoha *et al.*, 2013a; Alexander, 2014).

1.2 Research Background

Nowadays, there are a wide variety of pipeline rehabilitation techniques that are available for the offshore platform and onshore processing plant. Traditionally, the most common repair method is done by replacing a new steel pipe entirely for the damaged pipe or by removing the localized damaged section and covered it with a welded steel patch. Alternatively, the repair method can be done by the installation of full encirclement steel clamp or steel sleeve. These conventional repair system use either bolting or welding method to join both external steel sleeve and damaged pipe. Nevertheless, there are several limitations of these kinds of techniques, which are pricey, time-consuming and bulky especially for underground pipelines (Shamsuddoha *et al.*, 2012). It is an obvious fact that heavy machinery is required to perform this cumbersome work. Additionally, welding poses a potential risk of explosion as it involves hot work. Besides, these techniques are mostly not applicable for joints or bends but more suitable for a straight section of pipe. Therefore, it is an urge for the researchers to find an alternative way of repairing that is relatively lightweight, cheaper, appropriate yet effective (Shamsuddoha *et al.*, 2013a; Lim *et al.*, 2016a).

In most recent years, Fibre Reinforced Polymer (FRP) composite has been justified as a useful approach in steel pipeline rehabilitation (Duell *et al.*, 2008; Alexander,

2014). One of the reasons may be due to its capability in repairing steel pipelines which has been proven both experimentally and analytically. It is widely practiced in the industrial projects. Also, it does not require a stop of pipeline operation while eliminating the risk of fire or explosion due to welding during the repair that makes it a better choice (Duell *et al.*, 2008). Composite repair also prevented the growth of newer corrosion risk and it can be considered as a life time repair (Shouman & Taheri, 2011). Basically, FRP composite method can be categorized into few groups, which are pre-cured layered, pre-impregnated with the aid of resin, clamping, flexible tape and wet lay-up, which is similar to the concept of a bandage. Even though numerous companies have produced their own composite repair systems around the world which might have various performances, a composite material repair system generally consists of three parts: (i) a high strength of FRP composite wrap, (ii) a high curing speed of adhesive and (iii) an infill material with high compressive strength which transfers the load. Owing to the capability of restraining high pressure of pipeline from yielding, FRP composite wrap, together with putty have been selected in repairing steel pipeline (Trifonov & Cherniy, 2014).

Generally, a composite wrap is installed by wrapping few layers of a composite material over the defected location (Ariff *et al.*, 2014). An increase in wrapping thickness can help to prevent the premature yielding of pipeline especially at the damaged area and so it is rather important that a minimum thickness is done according to the existing design codes (Osella *et al.*, 1998). However, there is a trend to reduce the usage of composite wrapping as composite wrapper is more expensive than the infill material itself. Besides, some damaged pipes are situated in congested areas such as piping on offshore platforms, piping of boiler tank and underground pipelines that have only limited working space for the wrapping process to be done. This makes the only possible solution is to replace the whole damaged pipe to maintain its service life (Abdul Jalil *et al.*, 2016).

1.3 Problem Statement

In composite repair system, putty is generally used as an infill material. Most of the researchers assume that the function of putty is only to fill the defected area and creating a smooth surface rather than sharing the load with an additional protection layer. In other words, putty or grout acts as a load transfer agent between a corroded pipe and composite wrap. It is essential for minimizing the outward distortion of the corroded part

REFERENCES

- 3X Engineering. (2018). REINFORCEKiT[®] 4D, accessed on 26 December 2018, <http://www.3xeng.com/pdf/plaquette/pl-R4D-UK.pdf>
- Air Logistics Corporation. (2018). Aquawrap[®], accessed on 26 December 2018, <http://www.airlog.com/FACS/FACS%20Aquawrap.htm>
- Abdul Jalil, M.H., Valipour, A., Lim, K.S., Azraai, S.N.A., Zardasti, L., Yahaya, N., & Noor, N.M. (2016). Effect of putty properties in repairing corroded pipeline: a finite element analysis. *Malaysian Journal of Civil Engineering*, 28(2), 65–72.
- Alexander, C. (2014). The role of composite repair technology in rehabilitating piping and pipelines. *Proceedings of the ASME 2014 Pressure Vessels & Piping Conference (PVP 2014)*. 20-24 July 2014. Anaheim, California, USA. Paper No.: PVP2014-28257
- Alexander, C., Vyvial, B., & Wilson, F. (2014). Pipeline repair of corrosion and dents: a comparison of composite repairs and steel sleeves. *Proceedings of the 2014 10th International Pipeline Conference (IPC 2014)*. 29th September – 3rd October, 2014. Clagary, Alberta, Canada. Paper No.: IPC2014-33410. <https://doi.org/10.1115/IPC201433410>
- Ariff, T.F., Azmi, M.A., & Bahar, R. (2014). Economic analysis of using E-glass composite wrap repair system for pipelines in Malaysia. *Australian Journal of Basic and Applied Sciences*, 8(15), 241–245.
- Armor Plate Inc. (2018). Armor Plate[®], accessed on 26 December 2018, <https://www.armorplateinc.com/what-is-armor-plate/>
- ASME International. (2006). *ASME PCC-2-2006. Repair of Pressure Equipment and Piping*. New York, USA: The American Society of Mechanical Engineers.
- ASME International. (2011). *ASME PCC-2-2011. Repair of Pressure Equipment and Piping*. New York, USA: The American Society of Mechanical Engineers.
- Azraai, S.N.A., Lim, K.S., Yahaya, N., & Noor, N.M. (2015). Infill materials of epoxy grout for pipeline rehabilitation and repair. *Malaysian Journal of Civil Engineering*, 27(1), 162–167.
- Azraai, S.N.A., Lim, K.S., Yahaya, N., & Noor, N.M. (2016). Characterization of mechanical properties of graphene-modified epoxy resin for pipeline repair. *International Journal of Chemical, Molecular, Nuclear, Materials and Metallurgical Engineering*, 10(1), 15–18.

- Barkanov, E.N., Lvov, G.I., & Akishin, P. (2018). Optimal design of composite repair systems of transmission pipelines. *Engineering Materials*, 387–398. <https://doi.org/10.1007/978-3-319-56579-8>
- Buyukozturk, O., Gunes, O., & Karaca, E. (2004). Progress on understanding debonding problems in reinforced concrete and steel members strengthened using FRP composites. *Construction and Building Materials*, 18(1), 9–19. [https://doi.org/10.1016/S0950-0618\(03\)00094-1](https://doi.org/10.1016/S0950-0618(03)00094-1)
- Central Intelligence Agency. (2018). *The World Factbook Field Listing: Pipelines*. Retrieved from the Central Intelligence Agency. Accessed on 1 May 2018. <https://www.cia.gov/library/publications/the-world-factbook/fields/2117.html>.
- Chan, P.H., Tshai, K.Y., Johnson, M., Choo, H.L., Li, S., & Zakaria, K. (2015). Burst strength of carbon fibre reinforced polyethylene strip pipeline repair system - a numerical and experimental approach. *Journal of Composite Materials*, 49(6), 749–756. <https://doi.org/10.1177/0021998314525652>
- Chen, C.H., Sheen, Y.N., & Wang, H.Y. (2016). Case analysis of catastrophic underground pipeline gas explosion in Taiwan. *Engineering Failure Analysis*, 65(3), 39–47. <https://doi.org/10.1016/j.engfailanal.2016.03.013>
- Cosham, A., & Hopkins, P. (2011). The assessment of corrosion in pipelines – guidance in the pipeline defect assessment manual (PDAM). *Symposium A Quarterly Journal in Modern Foreign Literatures*, 44(0), 0–22.
- Cunha, S.B., & Netto, T.A. (2012). Analytical solution for stress, strain and plastic instability of pressurized pipes with volumetric flaws. *International Journal of Pressure Vessels and Piping*, 89, 187–202. <https://doi.org/10.1016/j.ijpvp.2011.11.002>
- Diniță, A., Lambrescu, I., Chebakov, M.I., & Dumitru, G. (2018). Finite element stress analysis of pipelines with advanced composite repair. *Engineering Materials*, 289–309. <https://doi.org/10.1007/978-3-319-56579-8>
- Duell, J.M., Wilson, J.M., & Kessler, M.R. (2008). Analysis of a carbon composite overwrap pipeline repair system. *International Journal of Pressure Vessels and Piping*, 85(11), 782–788. <https://doi.org/10.1016/j.ijpvp.2008.08.001>
- Farrag, K. (2013). *Selection of Pipe Repair Methods*. Final Report GTI – Project Number 21087, Gas Technology Institute.

- Frankel, G.S. (1998). Pitting corrosion of metals a review of the critical factors. *Journal of The Electrochemical Society*, 145(6), 2186–2198.
<https://doi.org/10.1149/1.1838615>
- Freire, J.L.F., Vieira, R.D., Diniz, J.L.C., & Meniconi, L.C. (2007). Effectiveness of composite repairs applied to damaged pipeline. *Experimental Techniques*, September/October, 59-66.
- Haladuick, S., & Dann, M.R. (2018). Decision making for long-term pipeline system repair or replacement. *ASCE-ASME Journal of Risk and Uncertainty in Engineering Systems, Part A: Civil Engineering*, 4(2), 04018009.
<https://doi.org/10.1061/AJRUA6.0000956>
- Hopkins, P. (2007). *Pipelines: Past, Present, and Future*, 44(0), 1–27.
- Index Pioneer Technologies Sdn Bhd. (2018). ProAssure™ Wrap product, accessed on 26 December 2018,
<https://ipt.com.my/products-pipeline-repair-reinforcement-system-proassure-technology.php>
- ISO. (2006). *ISO/TS24817. Petroleum, Petrochemical and Natural Gas Industries – Composite Repairs of Pipework – Qualification and Design, Installation, Testing and Inspection*. Switzerland: International Organization for Standardization.
- Jaske, C.E., Hart, B.O., & Bruce, W.A. (2006). *Pipeline repair manual*.
- Kishawy, H.A., & Gabbar, H.A. (2010). Review of pipeline integrity management practices. *International Journal of Pressure Vessels and Piping*, 87(7), 373–380.
<https://doi.org/10.1016/j.ijpvp.2010.04.003>
- Koch, G.H., Brongers, M.P., Tompson, N.G., Virmani, Y.P., & Payer, J.H. (2001). *Corrosion Cost and Preventative Strategies in the United States*. Federal Highway Administration, Office of Infrastructure Research and Development. pp. 260-311.
- Koch, G.H., Brongers, M.P.H., Thompson, N.G., Virmani, Y.P., & Payer, J.H. (2002). *Corrosion costs and preventive strategies in the United States*. Federal Highway Administration, Office of Infrastructure Research and Development. 1–12.
- Kou, J. & Yang, W. (2011). Application progress of oil and gas pipeline rehabilitation technology. *Proceeding of the International Conference on Pipelines and Trenchless Technology (ICPTT)*. 26-29 October 2011. Beijing, China. 1285–1292.

- Lee, A. & Meng, A. (2018). *Owners never inspected Taiwan gas pipeline that exploded because they 'didn't have the keys'*. Retrieved from the South China Morning Post. Accessed on 29 September 2018.
<https://www.scmp.com/news/china/article/1566101/owners-never-inspected-taiwan-gas-pipeline-exploded-because-they-didnt>.
- Lim, K.S. (2017). *Behaviour of repaired composite steel pipeline using epoxy grout as infill material*. Ph.D. Thesis. Universiti Teknologi Malaysia, Malaysia.
- Lim, K.S., Azraai, S.N.A., Noor, N.M., & Yahaya, N. (2016a). An overview of corroded pipe repair techniques using composite materials. *World Academy of Science, Engineering and Technology, International Journal of Chemical, Molecular, Nuclear, Materials and Metallurgical Engineering*, 10(1), 19–25.
- Lim, K.S., Azraai, S.N.A., Noor, N.M., & Yahaya, N. (2016b). *Systems for repair and rehabilitation of corroded oil & gas pipelines*. November 2016. 13–16.
- Madhujit, M. (2004). *Mechanics of Composite Materials*, Universities Press (India) Private Limited: India.
- Mendis, P. (1985). Commercial applications and property requirements for epoxies in construction. *SP. ACI Special*, 127–140.
- Merit Technologies Sdn Bhd. (2018). ProAssure™ Clamp (Composite) product, accessed on 26 December 2018, <http://merit.net.my/proassurance-clamp/>
- NACE International. (2014). *CORROSION FAILURES: Sinopec Gas Pipeline Explosion*. Retrieved from the NACE International. Accessed on 30 March 2018.
<https://www.nace.org/CORROSION-FAILURES-Sinopec-GAS-Pipeline-Explosion.aspx>.
- NACE International. (2016). *NACE study estimates global corrosion cost at \$2.5 trillion annually*. Retrieved from the NACE International. Accessed on 30 March 2018.
<https://inspectioneering.com/news/2016-03-08/5202/nace-study-estimates-global-cost-of-corrosion-at-25-trillion-ann>.
- Neptune Research Incorporation. (2018a). Syntho-Glass® XT products, accessed on 26 December 2018, <https://neptuneresearch.com/product/syntho-glass-xt/>
- Neptune Research Incorporation. (2018b). Viper Skin™ products, accessed on 26 December 2018, <https://neptuneresearch.com/product/viper-skin/>

- Nixus International. (2018). StrongBack® products, accessed on 26 December 2018, <http://nixusinternational.com/products/strongback/>
- Noor, N.M., Lim, K.S., Yahaya, N., & Abdullah, A. (2011). Corrosion study on X70-carbon steel material influenced by soil engineering properties. *Advanced Materials Research*, 311–313, 875–880. <https://doi.org/10.4028/www.scientific.net/AMR.311-313.875>
- Osella, A., Favetto, A., & López, E. (1998). Currents induced by geomagnetic storms on buried pipelines as a cause of corrosion. *Journal of Applied Geophysics*, 38(3), 219–233. [https://doi.org/10.1016/S0926-9851\(97\)00019-0](https://doi.org/10.1016/S0926-9851(97)00019-0)
- Palmar-Jones, R., & Paisley. (2000). Repairing internal corrosion defects in pipelines – a case study. *The Proceedings of the 4th International Pipeline Rehabilitation and Maintenance Conference*. September 2000, Prague.
- Peck, J.A., Li, G., Pang, S-S., & Stubblefield, M.A. (2004). Light intensity effect on UV cured FRP coupled composite pipe joints. *Composite Structures*, 64, 539–546.
- Peck, J.A., Jones, R.A., Pang, S-S., Li, G., & Smith, B.H. (2007). UV-Cured FRP joint thickness effect on coupled composite pipes. *Composite Structures*, 80, 290–297.
- Petronas Gas Berhad. (2014). *Pipeline System Listing*. Transmission Operation Division.
- Petronas Gas Berhad. (2015). *Annual Report 2015 – Transform to perform: results matter*.
- Pipe Line Development Company. (2018). PLIDCO Split+Sleeve, accessed on 26 December 2018, <http://www.plidco.com/product-line/split-sleeve>
- Saeed, N. (2015). *Composite overwrap repair system for pipelines – onshore and offshore application*. Ph.D. Thesis. The University of Queensland, Australia.
- Saeed, N., Ronagh, H., & Virk, A. (2014). Composite repair of pipelines, considering the effect of live pressure – analytical and numerical models with respect to ISO/TS 24817 and ASME PCC-2. *Composites Part B: Engineering*, 58, 605–610. <https://doi.org/10.1016/j.compositesb.2013.10.035>
- Shamsuddoha, M. (2014). *Behaviour of infilled rehabilitation system with composites for steel pipe*. Ph.D. Thesis. University of Southern Queensland, Australia.

- Shamsuddoha, M., Islam, M.M., Aravinthan, T., Manalo, A., & Lau, K.T. (2012). Fibre composites for high pressure pipeline repairs, in-air and subsea – an overview. *Proceedings of The Third Asia-Pacific Conference on FRP in Structures (APPFIS 2012)*. 2nd – 4th February 2012, Hokkaido University, Japan.
- Shamsuddoha, M., Islam, M.M., Aravinthan, T., Manalo, A., & Lau, K.T. (2013a). Effectiveness of using fibre-reinforced polymer composites for underwater steel pipeline repairs. *Composite Structures*, 100, 40–54.
<https://doi.org/10.1016/j.compstruct.2012.12.019>
- Shamsuddoha, M., Islam, M.M., Aravinthan, T., Manalo, A., & Lau, K.T. (2013b). Characterisation of mechanical and thermal properties of epoxy grouts for composite repair of steel pipelines. *Materials and Design*, 52, 315–327.
<https://doi.org/10.1016/j.matdes.2013.05.068>
- Shamsuddoha, M., Islam, M.M., Aravinthan, T., Manalo, A., & P. Djukic, L. (2016). Effect of hygrothermal conditioning on the mechanical and thermal properties of epoxy grouts for offshore pipeline rehabilitation. *AIMS Materials Science*, 3(3), 832–850. <https://doi.org/10.3934/matersci.2016.3.832>
- Shouman, A., & Taheri, F. (2011). Compressive strain limits of composite repaired pipelines under combined loading states. *Composite Structures*, 93(6), 1538–1548. <https://doi.org/10.1016/j.compstruct.2010.12.001>
- Sindt, O., Perez, J., & Gerard, J.F. (1996). Molecular architecture-mechanical behaviour relationships in epoxy networks. *Polymer*, 37(14), 2989–2997.
[https://doi.org/10.1016/0032-3861\(96\)89396-7](https://doi.org/10.1016/0032-3861(96)89396-7)
- Thacker, B.B.H., Light, G.M., Dante, J.F., Trillo, E., Song, F., Popelar, C.F., Coulter, K.E., Page, R.A. (2010). *Corrosion control in oil and gas pipelines*, 7 March, 62–67.
- The Clock Spring Company. (2012). Clock Spring[®] product brochure.
- Trifonov, O.V., & Cherniy, V.P. (2014). Analysis of stress-strain state in a steel pipe strengthened with a composite wrap. *Journal of Pressure Vessel technology*, 136(5), 051202. <https://doi.org/10.1115/1.4027229>
- T.D. Williamson Inc. (2018). RES-Q[®] composite wrap product, accessed on 26 December 2018,
<http://www.tdwilliamson.com/content/Bulletins/RES-Q%20Composit%20Wrap.pdf>
- Wrapmaster. (2018a). PermaWrap[™] product brochure, accessed on 26 December 2018,
https://www.wrapmasterinc.com/wp-content/uploads/permawrap_brochure.pdf

- Wrapmaster. (2018b). WeldWrap™ product brochure, accessed on 26 December 2018,
https://www.wrapmasterinc.com/wp-content/uploads/weldwrap_brochure.pdf
- Zecheru, G., Dumitrescu, A., Diniță, A., & Yukhymets, P. (2018). Design of composite repair system, *Engineering Materials*, 269–285.
<https://doi.org/10.1007/978-3-319-56579-8>