



# Quantifying Tensile Properties of Bamboo Silicone Biocomposite using Yeoh Model

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## Abstract

The utilisation of bamboo has the potential of improving the properties of silicone. However, a thorough investigation has yet to be reported on the mechanical properties of bamboo silicone biocomposite. This study was carried out with the aim to quantify the tensile properties and assess the tensile behaviour of bamboo silicone biocomposite using Yeoh hyperelastic constitutive function. The specimens were prepared from the mix of bamboo particulate and pure silicone at various fibre composition ratio (0wt%, 1wt%, 3wt% and 5wt%) cured overnight at room temperature. A uniaxial tensile test was carried out by adopting the ASTM D412 testing standard. The Coefficient of Variation, CV, and the Coefficient of Determination,  $r^2$ , were determined to assess the reliability of the experimental data and fitting model. The results of the determined Yeoh material constants for 5wt% specimen is found to be  $C_1 = 12.0603 \times 10^{-3}$  MPa,  $C_2 = 8.7353 \times 10^{-5}$  MPa and  $C_3 = -11.6165 \times 10^{-8}$  MPa, compared to pure silicone (0wt%)  $C_1 = 5.6087 \times 10^{-3}$  MPa,  $C_2 = 8.6639 \times 10^{-5}$  MPa and  $C_3 = -7.6510 \times 10^{-8}$  MPa. The results indicate that the bamboo fibre improves the stiffness of the silicone rubber by 115 percent. A low variance was exhibited by the experimental data with a CV value of less than 8 percent. The Yeoh Model demonstrated an excellent prediction of the elastic behaviour of bamboo silicone biocomposite with a fitting accuracy of more than 99.93 percent.

**Keywords:** Bamboo fibres; Hyperelastic; Tensile properties; Yeoh Model; Coefficient of Variation

## 1. Introduction

The exploitation of natural fibers as reinforcement material has led to a massive development of biocomposite for various applications. The transition towards sustainable products is in tandem with one of the seventeen United Nation's Sustainable Development Goals that contribute towards a sustainable future. Lignocellulosic fibres possess an advantage over other natural fibres due to its massive annual production which reflected from substantial agriculture activities across the tropical continents especially in China, India and South East Asia [1-3]. These materials are favoured for their notable strength-to-density ratio and have been extensively utilised in the production of high-elastic-resistance and weight-reduced components for automobiles, aircraft, marines and buildings [4-11]. The integration can also be seen in the exploratory works of rubberlike composites, although the employment greatly accentuated on high-strength fibres such as jute and hemp [12-14]. The limitation, however, resulted in the diversity towards the exploration of alternative resources with comparable properties and yet, provide facile accessibility and less costly [15].

In Malaysia, bamboo offers considerable potential, primarily due to its large cultivation area and relatively cost-effective [16, 17]. It is worth to note that bamboo has identical performance to major timber species [18] and have been exploited in numerous form to cater for different industrial applications [19, 20]. Bamboo fibres are mostly incorporated into polymeric composites i.e. polyvinyl chloride (PVC) and high-density polyethylene (HDPE) where the addition enhances the stiffness and flexural strength of the ma-

trixes [21, 22]. The integration was also found to improve the tensile modulus of natural rubber in [23, 24]. It is worth noting that the amount of fibre used was between 2.5 to 45 weight percent of the matrix. Though, the effect from the embedded fibre on elastomeric response has yet to be thoroughly reported in the previous work of rubber composites.

The characteristics of rubber, in contrary to bamboo fibre, are induced by the elastic behaviour of the material [25], hence, the need for nonlinear elastic models to quantify their properties is essential. Hyperelastic polynomial relations such as Neo-Hookean and Mooney-Rivlin are among the commonly used quantification models [26-30] owing to their lower degree of intricacy to be assessed as compared to exponential prediction models [31, 32]. However, the precision of the invariant-based models is limited by the presence of insufficient terms thus brought to the establishment of the extended polynomial hyperelastic models such as Yeoh and third order deformation approximation [33]. Yeoh model has been employed in many studies to quantify tensile [34], compressive [35] and shear [36] properties of rubberlike materials. The model was found to provide a reasonably accurate prediction of the experimental values with a relatively low error [37].

Therefore, this work attempts to quantify and assess the tensile properties of a novel bamboo silicone biocomposite using Yeoh hyperelastic constitutive equation. Low fibre loading was used to prevent the tendency for large size agglomerates to develop in the mixture [38]. The study also employed two different statistical indicators, namely, Coefficient of Variation, CV, and Coefficient of Determination,  $r^2$  to assess the reliability of the attained experimental results and the prediction model respectively. Moreover, since silicone rubber is favoured in many applications, i.e.

biomedical and automotive, amongst others for its excellent material properties [30, 39, 40], thus interpreting its elastic response is of critical importance for design optimization.

## 2. Methodology

### 2.1. Specimen Formulation and Compounding

Bamboo acquired is of *Dendrocalamus pendulus* species with an initial moisture content of 36.5 percent. The culm was cut into sections before peeled and dried in an oven at 80<sup>0</sup> C for 24 h. Dried mid culm was then crushed using ball mill at a speed of 300 rpm for 2 h. The produced powder was ground using a 100 μm screen. Next, bamboo particulate and pure silicone (Ecoflex 0030) were mixed at a fibre composition ratio of 0, 1, 3 and 5 weight percentage to the matrix and left to cure overnight at room temperature. Specimens were labelled as BS00, BS01, BS03 and BS05 where the number represents the respective fibre composition. Composed specimens were considered to be homogeneous throughout the structure.

### 2.2. Tensile Test

The uniaxial tensile test was carried out using Shimadzu Auto-graph AG-X 5kN (Fig. 1), by employing the ASTM D412 testing standard [41]. A total of 20 specimens was tested; 5 specimens for every composition of bamboo particulate. Attained results were presented in the form of mean engineering stress–stretch relation.



Fig. 1: Tensile test in progress

### 2.3. Determining the Yeoh Material Constants

Mechanical properties of the composed material were determined numerically through the manipulation of Yeoh hyperelastic constitutive model to the experimental data. The general form of strain energy function is given by [33]:

$$W = C_{10}(I_1 - 3) + C_{20}(I_1 - 3)^2 + C_{30}(I_1 - 3)^3 \quad (1)$$

where  $C_{10}$ ,  $C_{20}$  and  $C_{30}$  are the material constants of the tested specimen. For the case of incompressible material, the Green deformation tensor relation,  $I_1$ , reduces to:

$$I_1 = \lambda^2 + 2\lambda^{-1} \quad (2)$$

where  $\lambda$  is the principle extension ratio. Considering Piola Kirchhoff stress theory, engineering stress–stretch relation can be derived from Eq. (1):

$$\sigma_e = 2(\lambda - \lambda^{-2})(C_{10} + 2C_{20}(\lambda^2 + 2\lambda^{-1} - 3) + 3C_{30}(\lambda^2 + 2\lambda^{-1} - 3)^2) \quad (3)$$

Material constants were computed using the derivative of the polynomial regression method, which is represented by the following relation [42]:

$$S_r = \Sigma(\sigma(\lambda)_{i, \text{exp}} - \sigma(\lambda)_{i, \text{model}})^2 \quad (4)$$

This method has been employed in various studies due to its effectiveness in solving multiple–constant polynomial equation [43, 44].

### 2.4. Statistical Analysis

The precision of the experimental results was measured by the evaluation of data extendibility using Coefficient of Variation relation [45]:

$$CV = [\Sigma(\lambda_i - \lambda_{\text{mean}})^2 / (n - 1)]^{1/2} / |\lambda_{\text{mean}}| \quad (5)$$

where  $n$  is the number of specimens. In general, the value of CV represents the ratio of sample standard deviation relative to its absolute mean,  $\lambda_{\text{mean}}$  at predetermined stress magnitude. A dataset of high precision scattered at low variance, contributed to the small CV value vice versa [46, 47].

Moreover, the accuracy of the fitted curves was determined using the Coefficient of Determination (COD) relation [42]:

$$r^2 = 1 - \Sigma(\sigma(\lambda)_{i, \text{exp}} - \sigma(\lambda)_{i, \text{model}})^2 / \Sigma(\sigma(\lambda)_{i, \text{exp}} - \sigma(\lambda)_{\text{mean}})^2 \quad (6)$$

Mainly, the higher coefficient value indicates higher accuracy is achieved by the prediction model to the original uncertainties of experimental data [48, 49].

## 3. Results and Discussion

Fig. 2 shows the uniaxial elastic behaviour of bamboo silicone biocomposite at various fibre–to–matrix ratio. All curves display nonlinear characteristic in which similar to the profile of silicone rubber composites reported in [30, 50].

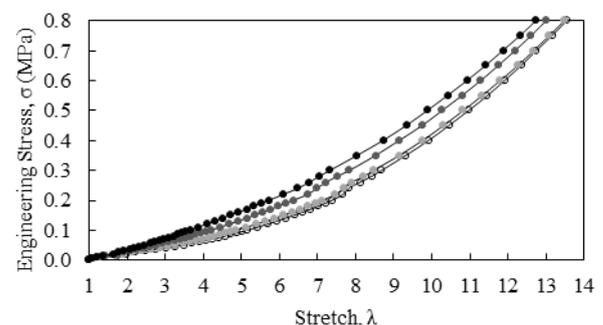


Fig. 2: Mean stress–stretch behaviour of specimens BS00 (○); BS01 (●); BS03 (■); and BS05 (◆).

It is interesting to note the transition of the curvilinear trend across the axes. It could be observed that the addition of bamboo filler into the silicone rubber matrix affects the elasticity properties of

the developed biocomposite. This is apparent with the decrease in the elongation of 6 percent. A similar trend was also portrayed in [50] where the relative strain reduces with the increase of fibre content. The poor elasticity behaviour is resulted from the progression of strain energy, which leads to a higher degree of resistance of the structure towards large deformation state.

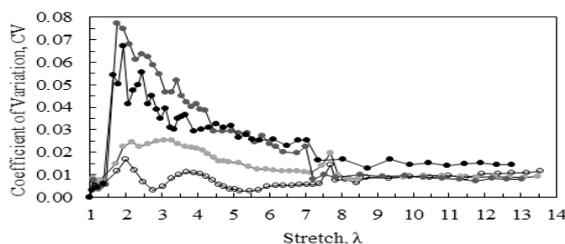
Furthermore, it could also be observed that along the deformation range  $2 \leq \lambda \leq 7$ , gradual increment transpired to the slope of the curves which suggested that stiffening effect is highly intensified at lower stress range ( $20 \text{ kPa} \leq \sigma \leq 300 \text{ kPa}$ ). The presence of more fillers provides a larger surface area, allowing higher load transfer to take place due to the significant interaction occurs between matrix and fibres [39, 51]. The increase in stiffness is reflected by the upsurge trend of constant  $C_1$  in Table 1. The stiffness of the silicone rubber was found to enhance by 115 percent with the incorporation of 5 wt% bamboo fibres. The elongation profile also tends to be less nonlinear in which conveyed by the decreasing value of constant  $C_3$ . However, no changes transpired to the behaviour of the stress–stretch curve beyond the aforesaid range, probably due to the greater matrix crosslinking effect as compared to the fibre reinforcing [24]. Such occurrence can be related to the unvarying trend of the constant  $C_2$  in the presented table.

**Table 1:** Yeoh material constants determined at various composition

Specimens	Fibre Addition (wt%)	Material Constants (MPa)			COD, $r^2$
		$C_1 (10^{-3})$	$C_2 (10^{-5})$	$C_3 (10^{-8})$	
BS00	0	5.6087	8.6639	-7.6510	0.9998
BS01	1	6.6271	8.6510	-8.3200	0.9999
BS03	3	9.3171	9.0450	-10.7941	0.9997
BS05	5	12.0603	8.7353	-11.6165	0.9993

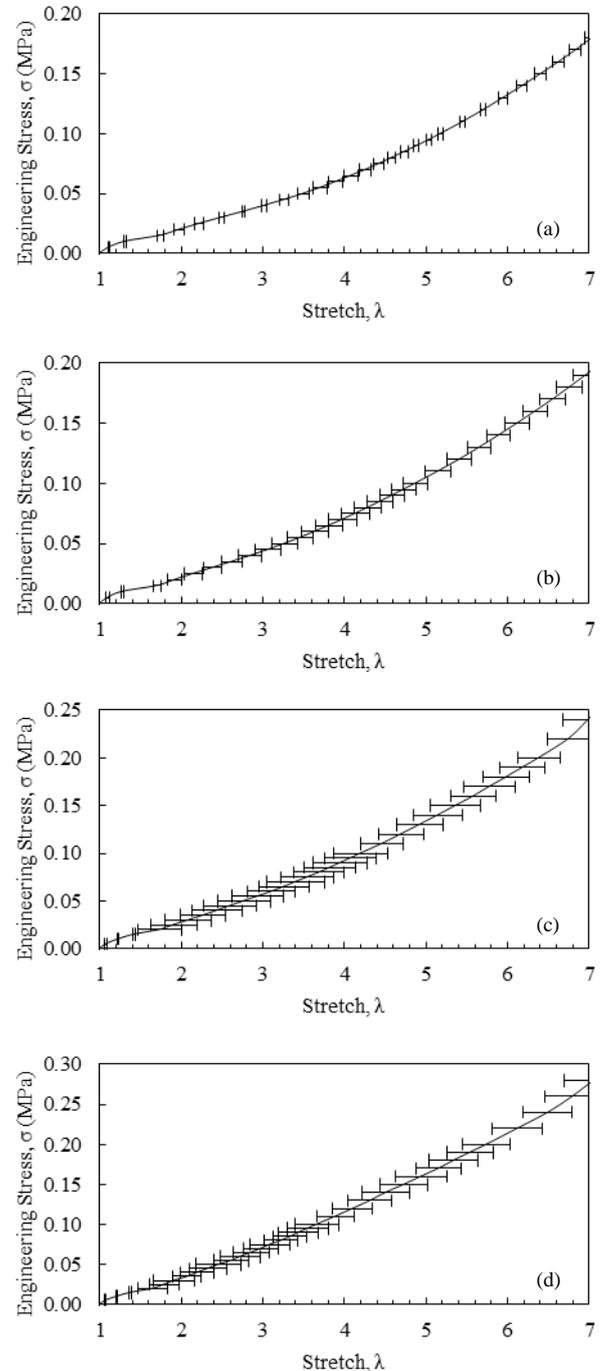
Fig. 3 shows the CV value of the experimental data at various mean stretch. High CV value was found to appear in the range of  $2 \leq \lambda \leq 7$  which concentrated at 200 percent stretch for all specimens. The emergence of the peak value is brought by the abrupt data distribution exhibited by the specimens within the stress value of 0.02 to 0.03 MPa (refer Fig. 4). However, as the exerted load increases, the transpired elongation becomes closer to the sample mean, that in turn resulted in the less deviation of the error bar. Despite the broad data distribution exhibited in Fig. 4(c) and 4(d), low variance data appeared in the stress–stretch diagram of specimens BS00 and BS01 with a CV value of less than 3 percent (Fig. 4(a) and 4(b)).

In terms of reinforcing mechanism, such development might be associated to the disproportionate tensile strength exhibited by the distinctive specimens as a result from the presence of the large and poor dispersion of agglomerates throughout the matrix [52-54]. The development of the filler network during low deformation is highly related to the higher surface interaction between fibre and matrix [55]. However, as the concentration of filler increases, the matrix–filler interaction tends to become weaker due to the reduction of specific surface area transpired from the agglomeration of fibres [56]. Large agglomerates act as a stress concentrator in a matrix [56] and it is unfavoured for its low transverse stiffness [48]. Agglomerates with a size larger than the flaw size of matrix contribute to poor dispersion [57, 58] and deteriorate the mechanical properties [54].



**Fig. 3:** Coefficient of variation of dataset attribute to specimens BS00 (○); BS01 (●); BS03 (■); and BS05 (▲) at various mean stretch

Though, less variation was found to appear to the data set beyond 700 percent stretch range with a CV value of less than 2 percent. At large strain, filler network tends to be weak due to amplification of local strain which causes rubber chains between crosslinks to greatly extend [55]. The development of rubber crosslinking reduces the inconsistency of reinforcing effect thus resulted in the homogeneous deformation of the specimens. All the data attained from the experiment are distributed within 95 percent of the normal distribution.

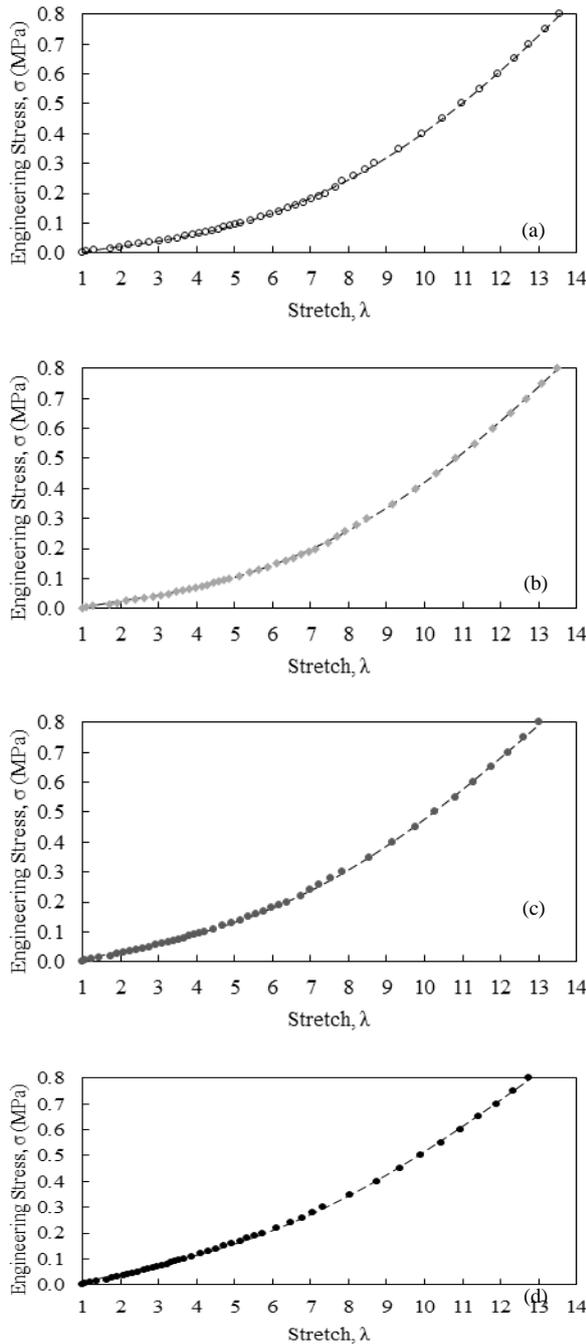


**Fig. 4:** Mean stress–stretch behaviour of specimens (a) BS00; (b) BS01; (c) BS03; and (d) BS05 focusing specifically on deformation region of  $1 \leq \lambda \leq 7$  with 2 standard deviation error bar.

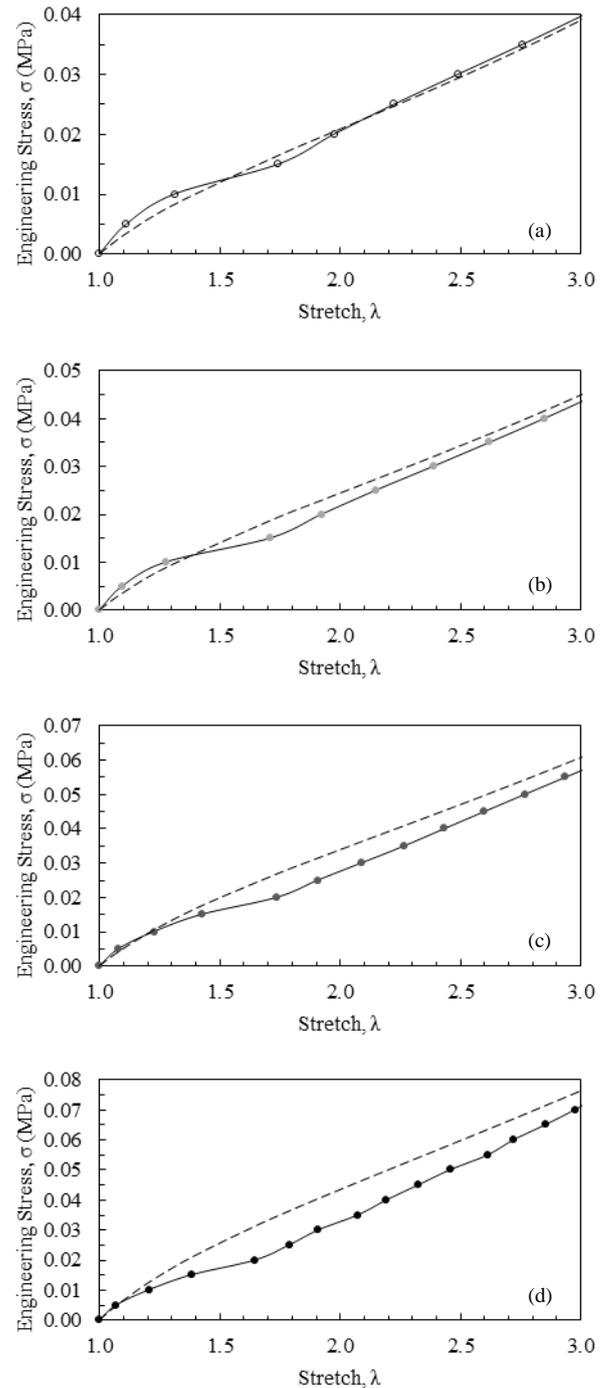
The stress–stretch curve for each variation is separated into Fig. 5(a), Fig. 5(b), Fig. 5(c) and Fig. 5(d) to explicitly highlight the behaviour of the prediction curve (Yeoh Model) with respect to the experimental value. Predicted hyperelastic profiles are depicted by the dashed curve lines. The fitted curves are almost consistent with the experimental data value (denoted by markers) with

a standard error of less than 1 percent. The high value of  $r^2$  obtained indicates the adequacy of the Yeoh Model on representing the experimental results. The outcome shows that there is a real relation between stretch,  $\lambda$ , and stress,  $\sigma$ , [43] for all tested specimens in present work.

Nevertheless, at lower stretch range ( $1 \leq \lambda \leq 3.25$ ), a high discrepancy occurs to the projections (Fig. 6(a) to 6(d)) due to the inherent limitation of the model on depicting small strain behaviour of large deformation material [33]. Disassociation of invariant tensor  $I_2$  has brought to such drawback [33]. A relative error within the range was found to be 31.38, 30.27, 34.09 and 56.42 percent which attribute to the prediction model of specimen BS00, BS01, BS03 and BS05 respectively. An inverse relation can be seen between relative error and coefficient of determination value – the higher the error transpired, the lower the value of the coefficient attained. At higher stretch range ( $3.25 < \lambda \leq 14$ ), transpired relative error is below 5 percent for all predicted value.



**Fig. 5:** Mean stress–stretch behaviour of specimens (a) BS00; (b) BS01; (c) BS03; and (d) BS05 and respective Yeoh Model prediction curves.



**Fig. 6:** Mean stress–stretch behaviour of specimens (a) BS00; (b) BS01; (c) BS03; and (d) BS05 in deformation region of  $1 \leq \lambda \leq 3$ . The dashed line represents the Yeoh Model prediction curve.

### 4. Conclusion

This paper reports the work related to the quantification of the tensile properties of bamboo silicone biocomposite. The variation of experimental data was found to be acceptable with the distribution of less than 8 percent. It was observed that the stiffness of bamboo silicone biocomposite is improved by 115 percent through the reinforcement of 5 weight percent ratio of bamboo fibres into silicone rubber. Moreover, an excellent prediction of the elastic behaviour of tested specimens was demonstrated by the Yeoh Model, suggesting its efficacy in predicting the behaviour of the proposed biocomposite. Future works will involve the investigation and the quantification of the compressive behaviour of

bamboo reinforced silicone biocomposite to provide further insight on its potentiality and practical implications.

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