PAPER • OPEN ACCESS

A Review on Hybrid Processes for Palm Oil Mill Effluent: Possible Approaches

To cite this article: S K Al-Amshawee et al 2020 IOP Conf. Ser.: Mater. Sci. Eng. 736 022036

View the article online for updates and enhancements.

Recent citations

- <u>Biocarriers for biofilm immobilization in</u> <u>wastewater treatments: a review</u> Sajjad Al-Amshawee *et al*

A Review on Hybrid Processes for Palm Oil Mill Effluent: Possible Approaches

S K Al-Amshawee¹, M Y Yunus^{1,2} and A A Azoddein¹

¹Faculty of Chemical and Natural Resources Engineering, Universiti Malaysia Pahang, Gambang, 26300 Gambang, Pahang, Malaysia.

²Earth Resource and Sustainability Centre (ERAS), Universiti Malaysia Pahang, Gambang, 26300 Gambang, Pahang, Malaysia.

Corresponding e-mail: yusri@ump.edu.my

Corresponding address: Faculty of Chemical and Natural Resources Engineering, Universiti Malaysia Pahang, Gambang, 26300 Gambang, Pahang, Malaysia.

Abstract. The aim of this review paper is to explore and examine hybrid processes and systems for polishing palm oil mill effluent (POME). Nitrification process, and nutrients removal are highly significant to process highly contaminated POME. Besides, quality of POME process is extremely important to solve fresh water shortage that has blocked millions of people from accessing a clean water. Hence, attentions have been made on water pollution to raise a global demand to improve POME processing and discharge unharmful effluent to the waterways. For decades, using a stand-alone technology to treat POME has faced fouling, and disability to deliver the promising quality. A new approach is termed as hybrid or combined system has the ability to deliver higher performance and more effective contamination removal than stand-alone technologies. Hybrid system is a novel technology can't accomplish. This review reports various hybrid systems and united technologies to treat POME including their advantages, disadvantages, and limitations.

1. Introduction

Annually, diarrhea problem causes death for two million people and 1.2 billion people suffer from water scarcity and can't find valid water for drinking purposes [1]. These consequences are still occurring because of careless wastewater discharge that have grown awareness towards fresh water lack, and wastewater treatment [2]. Wastewater contains various pollutants could be biological, chemical, and physical, which dangerously and severely impact the waterways [3]. Nutrients in palm oil mill effluent (POME), such as phosphorus (P), and nitrogen can cause groundwater contamination, and undesirable aquatic evolution, while physical pollution such as suspended solids (SS), and biodegradable matter can produce septic conditions, and oxygen depletion [4]. Therefore, polishing processes are made to deliver satisfying treatment quality, prevent diseases spread, secure aquatic life, and provide harmless environment [5][6]. Consequently, the concept of hybrid system has been introduced showing decent ability to produce energy and deliver treatment in one time for wastewater. However, hybrid system is still in their early stages because there are several unbeaten challenges yet, such as poor electricity generation, require expensive materials, and slow wastewater treatment.

Globally, Malaysia is the second major producer of the most traded cooking oil, named as palm oil. It produces massive discharge of palm oil mill effluent which leads to global pollution into the fresh

Content from this work may be used under the terms of the Creative Commons Attribution 3.0 licence. Any further distribution of this work must maintain attribution to the author(s) and the title of the work, journal citation and DOI.

Energy Security and Chemical Engineering Congress	IOP Publishing
IOP Conf. Series: Materials Science and Engineering 736 (2020) 022036	doi:10.1088/1757-899X/736/2/022036

water sources. The generated POME amount in 2011 was around 60 million ton, while it was around 30 million ton in year 2004 and 44 million ton in year 2008 [6][7][8]. Major demands to invent sustainable technologies having strong management system to protect and secure the waterways. Also, governments have decided to look for sustainable methods to polish POME [9]. Aerobic, anaerobic, and facultative operations have been advanced for POME treatment, but they are still costly, and requiring large surface area, long retention time, and gas capture facilities.

2. Hybrid System

Since POME is contaminated with multiple pollutants, such as metals, phosphorus, nitrogen, irons, degradable organics, volatile organics, oil and grease, and suspended solids, for that it requires a massive technology to remove all kinds of contamination, and it's impossible to make it done with a stand-alone technology. A system from various mechanisms like biological, chemical, and physical can be united in one system to defeat treatment limitations and disadvantages and deliver efficiency, performance, quality, and energy saving named as combined or hybrid system [10]. Also, combining two or more technologies unites their weaknesses and strengths which leads to major obtainable balance. Therefore, hybrid system can remove more than one sort of pollutants so that its more preferable. For instance, A physical-biological treatment like membrane bioreactor (MBR) can be employed to remove organic and inorganic matters, oil and grease, and high suspended solids from wastewater. In addition, MBR has many advantages such as stable nitrification, reusable water production, and good capability for handling large organic loading rates [11][12][13][14][15][16]. There are numerous possible combinations of POME hybrid systems, such as coagulation and flocculation, activated sludge and biofilm process, and hybrid membrane. Combined system owns many advantages such as stability, bioenergy generation, efficacy, and energy saving, while often, it requires costly materials, and this can be considered as a major disadvantage. There are several limitations restrict the hybrid system from getting developed like low energy production. Moreover, selection of a reliant combined system is very complex because it depends on kind and amount of POME pollutants. For instance, chemical treatment is used for heavy metals removal, physical treatment for suspended solids removal, and bioprocess for toxic organic, phosphorus, nitrogen, volatile organics, and degradable organics removal. Figure 1 presents the possible hybrid systems between biological, chemical, and physical treatments to treat wastewater. It's worth mentioning that there are differences between hybrid systems and group of processes employed to produce various polishing level named as preliminary, primary, secondary, and tertiary.



Figure 1. Possible combined systems for wastewater treatment [17]

Energy Security and Chemical Engineering Congress

IOP Publishing

IOP Conf. Series: Materials Science and Engineering 736 (2020) 022036 doi:10.1088/1757-899X/736/2/022036

2.1 Coagulation and Flocculation

When a coagulant and flocculant are streamed in a wastewater treatment tank, the operation is named as coagulation and flocculation process. Norulaini et al. (2013) defined coagulation-flocculation process as a physical-chemical hybrid system, which through this integration a reagent should be added and mixed thoroughly with the contaminated water to thicken solids layer into larger particles so its easily removed with physical means. This type of hybrid system is used to drop turbidity concentration in wastewater [18]. The most common coagulants for wastewater treatment are aluminum chlorohydrate, ferric sulfate, ferric chloride, and aluminum sulfate. Using poly aluminum as a coagulant can deliver 75, 88.8, and 99.9% reduction of chemical oxygen demand (COD), total nitrogen (TN), and total phosphorus (TP), respectively. Satyanarayan et al. (2005) examined wastewater coagulation-flocculation by using many coagulants materials such as alum, lime, ferrous sulfate, and anionic polyelectrolyte [19]. It removed 41.9, 36.1, and 38.9% of TSS, COD, and biochemical oxygen demand (BOD) concentrations, respectively by using lime, while using lime-ferrous sulfate combination produced 56.8% removal of COD. In addition, combining alum and lime had given 42.6% removal of COD. This empirical work proves that using a hybrid system produces efficacy and quality. Figure 2 shows simple scheme for coagulation and flocculation process.



Figure 2. Coagulation and Flocculation system

Non-renewable, and oil based raw materials are employed to synthesis polymers for the coagulationflocculation process. For decades, polymers have been used to reduce dosages of coagulants [20]. Since the world style is moving towards sustainable way, so a great interest to replace polymers with biopolymers which they are cellulose derivatives. Liimatainen et al. (2012) examined flocculation process by using cationic (CDAC) and anionic (ADAC) cellulose derivatives, and figured out using anionic cellulose produces higher flocculation efficacy, also Hok-kanen et al. (2013) confirmed Liimatainen's results [21][22]. Amuda and Alade (2006) conducted laboratory scale coagulationflocculation treatments for wastewater with utilizing many reagents. It eliminated 98, 34, and 65% of TSS, TP, and COD, respectively [23].

Coagulation-flocculation combination for POME processing can reduce turbidity, and COD concentrations, and utilizing ferric sulfate as coagulant, with employing high dicarboxylic acid nanocellulose nanofibril content gives tremendous polishing process for POME. Ho and Tan (1989) had examined POME treatment by using coagulation (aluminum sulphite)-flocculation (cationic polyacrylamide) and it removed 97% of the suspended solids [24].

2.2 Activated Sludge and Biofilm Process

Activated sludge process has been employed as a secondary polishing process for wastewater with using long time hydraulic. It can be improved by many ways but combing it with another process leads to impressive performances. For instance, additional clarifier is highly required from time to time to improve the activated sludge quality and defeat the high organic load. Besides, purchasing and installing another stand-alone process is costly, and may not produce the expected treatment. Hence, the hybrid

Energy Security and Chemical Engineering Congress IOP Publishing IOP Conf. Series: Materials Science and Engineering **736** (2020) 022036 doi:10.1088/1757-899X/736/2/022036

system got a huge attention by proposing to unite two different biomass processes through using suspended biofilm carriers, named as integrated fixed film activated sludge process (IFAS) [25][26][27][28]. It handles a higher dosage of the bio sludge and the final settling tank faces not a significant growth in the organic load. It occurs because biofilm have attached naturally by effective bacteria on the media elements and it is counted as a huge advantage for the IFAS hybrid system. In addition, the high retention time allows biofilm bacteria to acclimatize, develop, and mature [29][30]. Many studies conducted and investigated the quality of IFAS process with using different media elements for nitrogen and organic matter removal [31][32][33]. It confirmed that biofilm have the ability to attach on fixed or moving carrier media, for that these carriers can be fixed inside the reactor or freely moving [25][34][35][36].

There are advantages of using IFAS system, such as high surface area, low cost, low sludge production, doesn't need backwashing, doesn't require filter channeling, and can be operated in various temperatures and pH. On the other hand, uncontrollable biofilm growth, and longtime startup are major disadvantages for this hybrid system, and these are limiting the process efficiency. The below diagram presents IFAS system for wastewater treatment.



Figure 3. IFAS process

2.3 Hybrid Membrane

Hybrid membrane system refers to a combined system involving a biological, chemical, or physical process followed by ultrafiltration, reverse osmosis (RO), forward osmosis, nanofiltration, or microfiltration membrane. This integration empowers membrane process to defeat their limitations (e.g., membrane clog, fouling). Figure 4 shows a general hybrid membrane system for treating wastewater.



Figure 4. Flow process of general Hybrid membrane treatment

A lot of studies have showed that using a stand-alone membrane is pricy because it has many limitations, and it's unprofessional to neglect it (see table 1). Hence, membrane bioreactors (MBR) have been used broadly for wastewater treatment [37]. The selection process of a hybrid membrane system is quite sensitive because it should be constructed based on the wastewater characteristics, and depending on the wanted treatment quality [38][39]. The most common used membranes in MBR system is microfiltration (MF) and ultrafiltration (UF). Also, the combination between biological and membrane

Energy Security and Chemical Engineering Congress

IOP Conf. Series: Materials Science and Engineering 736 (2020) 022036 doi:10.1088/1757-899X/736/2/022036

System	Table 1. Hybrid Memb Membrane type	Results	Limitations	Ref
MBR	Chlorinated polyethylene nano	Good efficiency in	TN/TP removal	[43
MBK	filtration (NF) + conventional activated sludge	removing polar pollutants	11N/1P Temovai	[43]
Hybrid membrane bioreactor (HMBR)/ conventional membrane bioreactor (CMBR)	Aerobic reactor + hollow fiber membrane (MF)	Eliminating organic contaminants and lowering COD concentration	-	[44
Nonwoven fabric filter bag (NFFB)+MBR	Nonwoven polyester fabric + conventional activated sludge	Good performance in removing TSS, and sludge	-	[37
ANMBR	Polyvinylidene difluoride (PVDF) flat sheet membrane/ PES tubular membrane	Great discharge quality with low sludge production	High organic strength, pore size, and membrane operational properties	[45
Hybrid membrane anaerobic membrane bioreactors (ANMBRs)	Polyethylene (PE) flat sheet membrane + CSTR	Efficiency in removing TSS, and COD concentrations	Flux, and pore size	[46
Submerged anaerobic membrane bioreactor (SANMBR)/HANMBR	PE flat sheet membrane	High COD, and SCOD removal with low energy consumption but it is easy to foul.	Restricted at limited temperatures	[47
Submerged membrane bioreactors (SMBRs)	Conventional activated sludge + hollow fiber MF membrane	Fouling	Membrane fouling with Bio sludge generation	[48
SMBR with chorine	PVDF hollow fiber	Good performance in reducing TSS concentration	Low efficiency for dissolved organics removal	[49
Nitrogen loading rate (NLR)+SMBR	Acrylic hollow fiber	Efficiency in reducing TN, and COD amounts	Low ability to remove phosphorus in high polluted wastewater	[50
Staged anaerobic fluidized membrane bioreactor (SAF-MBR)	Anaerobic fluidized-bed reactor (AFBR) + anaerobic fluidized bed membrane bioreactor (AFMBR) +PVDF hollow fiber	Low fouling, with low energy consumption	-	[51
NF+MBR	NF flat sheets +PVDF MF membrane hollow fiber + activated sludge	Good quality in removing organic matter	-	[52
Dynamic membrane reactor (DMR)	Activated sludge, diatomite, kaolin clay and powder activated carbon (PAC) + nylon membrane flat sheet	Short treatment time, easy backwash, and high filtration flux.	Microbial layer formation	[53
Bio-enhanced powder activated carbon dynamic membrane (BPDM)	Asymmetrical PAC +mesh support	Good performance in removing organic and inorganic matters	-	[11
ANMBR-psychrophilic condition	Flat-sheet MF polyether sulfone membranes	Flux managing, with efficiency in decreasing BOD, and COD levels	-	[54

treatment produces high declining in ammonia nitrogen (NH3-N), biochemical oxygen demand (BOD), and chemical oxygen demand (COD).

In the pharmaceutical treatment, Dolar et al. (2012) investigated RO and MBR hybrid system for polishing wastewater and it delivered 95-99% of total reduction [40]. Moreover, Chon et al. (2013)

Energy Security and Chemical Engineering Congress	IOP Publishing
IOP Conf. Series: Materials Science and Engineering 736 (2020) 022036	doi:10.1088/1757-899X/736/2/022036

tested MBR and Nanofiltration membrane for municipal wastewater treatment [41]. The laboratory scale hybrid system declined fouling and flux occurring probability. Therefore, hybrid membrane produces great quality of wastewater treatment with cost-effectiveness, and eco-friendliness, and it's expected to be employed in industrial and domestic scale.

POME is highly polluted, and it needs a massive treatment with high quality to stream reusable discharge. Hybrid membrane system is quite suitable for POME treatment to deliver high polishing process but there are concerns regarding unexpected membrane fouling [42]. The successful treatment of membrane is constructed on the previous treatment performance which determines the overall treatment quality.

2.4 Hybrid Up-Flow Anaerobic Sludge Bed (HUASB) Reactor

Often, wastewater industry uses anaerobic conditions to process POME like HUASB reactor. HUASB is a combination of up-flow anaerobic sludge bed (UASB) and anaerobic filter [55]. HUASB reactor has several benefits such as stability, and well ability to remove organics, and it can process high organic load POME processing. Shivayogimath and Ramanujam (1999) achieved 80% reduction of COD concentration by using HUASB reactor for 6 hours of HRT and the organic load rate was 36 kg COD.m⁻ ³.d⁻¹ [56]. In addition, 80% of the produced gas was methane. Lew (2004) had conducted empirical work on Hybrid UASB reactor for domestic wastewater treatment at different temperatures [57]. The treatment efficiency was found stable by 80% at temperatures range 28 to 20 °C, but COD removal performance declined by 60% at temperatures less than 20 °C. Another report by Rajakumar and Meenambal (2008) found that HUASB reactor has short-start time around 120 days, with 80% efficiency of organic removal. Other researchers, reported that HUASB is very effective to process dilute to medium strength contaminated water [58]. Microorganisms have shown fast developing in HUASB reactor because POME is quite fitting with their biological activities. It produces biomass, which accumulates in major range around 86% at the sludge section, while the rest amount 14% of the total biomass settles at the biofilter layer, according to Tur and Huang (1997) [59]. Figure 5 presents HUASB structure diagram which is involving packing media, influent distributor, sludge bed, and weirs for industrial scale, while laboratory scale involves filter media, sludge blanket, sludge bed, and gas displacement system.



Figure 5. HUASB reactor schematic diagram

IOP Publishing

IOP Conf. Series: Materials Science and Engineering 736 (2020) 022036 doi:10.1088/1757-899X/736/2/022036

2.5 Ultraviolet and Fenton Oxidation (UV-Fenton)

Fenton oxidation process is the most common process for eliminating organic pollutants among advanced oxidation processes (AOPs). It requires high chemical amounts, and high operating costs and leads to excessive sludge production. Hence, a hybrid system termed as UV-Fenton has been introduced to decrease operating cost and improve the treatment quality. UV-Fenton system oxidizes and breaks down large organic matters into smaller size. Hydrogen peroxide (H₂O₂) can be photolysis by using UV lights, which leads to oxidation process by radical addition, electron transfer, or hydrogen abstraction and generates powerful fundamental of HO [60][61][62]. In comparing to all AOPs, UV-Fenton can deliver wastewater treatment in short time, without sludge production at the end of the reaction [63][64]. UV-Fenton system can remove 91.2% of COD concentration, while using stand-alone Fenton process removes 81.4% of COD concentration. It shows that using UV-Fenton for high polluted discharges such as POME, can produce well treated effluent with major reduction in COD, color, and total organic carbon (TOC) concentrations with ranges 91.2, 99.9, and 78.5%, respectively. In below, combined pictures to illustrate UV-Fenton process.



Figure 6. UV-Fenton process

There are parameters affect UV-Fenton process quality, such as pH, pollutants, H_2O_2 concentration, light intensity, catalyst, and temperature [65][66][67][68][69]. Muruganandham et al. (2006) and Shu et al. (2005) reported that pH level is a major factor determining UV-Fenton degradation performance [70][71]. Another report by Schrank et al. (2007) and Shu et al. (2005) declared that high pH level increases the degradation efficiency [72][73]. Some advantages of UV-Fenton are effective destruction of hazardous organic pollutants, and organic matter mineralization [74].

2.6 Ultrasound and H_2O_2

Ultrasound and H_2O_2 combination produce higher quantity of radicals than using a stand-alone oxidation process like Fenton oxidation. The attach of the free radicals against wastewater pollutants over time period determines the process quality. Several parameters can advance process performance such as influent composition, pollutants concentration, temperature, Fenton's reagent dosage and pH. A report by Olson and Barbier (1994) found that increasing ultrasound intensity raised the rate of degradation process [75]. Another researcher reported that ozone amount rapidly declined from 620 μ M to 40 μ M when ultrasound was applied during 3 minutes of time period [76]. The generated acoustic streaming by ultrasound leads to turbulence which terminates mass transfer limitations with the ozonation process. Hence, combined system comprising of ultrasound and H_2O_2 can give impressive treatment due high degradation rate [77][78][79]. Moreover, it shows a great promise for wastewater treatment because it possesses simple design and easy operation.

There are two kinds of pollutants in the wastewater, known as hydrophobic and hydrophilic. The degradation rate is determined by the pollutants kind and amount. Also, Ultrasound and H2O2 hybrid system causes pyrolysis followed by high temperature and pressure [80]. In addition, there are two kinds

Energy Security and Chemical Engineering Congress

IOP Conf. Series: Materials Science and Engineering 736 (2020) 022036 doi:10.1088/1757-899X/736/2/022036

of cavitation or sonication process which they are hydrodynamic and acoustic cavitation. Several reports declared that it's hard to use acoustic cavitation process for wastewater treatment in industrial scale because its associated with issues and high costs, but it's a quite successful process at the lab scale [81]. Venturi, valve, or orifice passages are capable to produce hydrodynamic cavitation when the liquid is streamed and constricted through it. In comparing to acoustic cavitation process, hydrodynamic method produces less destruction rate within same pressure and temperature [82]. Ma (2010) conducted experimental work to compare the performance of individual Fenton process against Ultrasound and Fenton (US-Fenton) system [83]. The stand-alone system reduced 15% of TOC, and 40% of carbofuran within 120 minutes, while the hybrid system gave more than 99% of carbofuran removal with 40% mineralization for 30 minutes.

2.7 Sequential Batch Reactor and Forward Osmosis (SBR–FO)

Forward osmosis is a novel technology of membrane separation family which can be used to save energy. FO membrane has been combined with various technologies such as electro dialysis (ED), and membrane distillation (MD). This combined system of Sequential Batch Reactor and Forward Osmosis (SBR–FO) involves a two flat sheets of FO membrane submerged inside SBR. Sequential batch reactor and forward osmosis (SBR–FO) can achieve 100, 88.4, 96.2, 58.4, 62.4, and 98.55% reduction of phosphate, ammonia, nitrite, nitrate, total nitrogen, and dissolved organic carbon concentrations. Two different liquid concentrations are separated by FO membrane, water moves from the low concentration liquid (FO influent) to the high concentration side (Draw solution) to get equilibrium state. While SBR process involves various stages of treatment like filling, aeration, settling, decantation, and idling, with great ability to remove COD and phosphor concentration [84]. Fouling is still a major issue with all the kind of membrane because of organic molecules, colloids, and particles, and when a clog occurs because of extracellular polymer substance (EPS) it is named as biofouling.

2.8 Other Combinations

Majority of other combinations are expensive, hard to be operated at the industrial scale, and not quite effective for POME treatment. Hence, at the present, researches and developments are conducted to come out with high performance, and appropriate hybrid system for large quantities, and highly polluted wastewater like POME. Some researches occurred on uniting electrocoagulation with electro dialysis system for wastewater. It can deliver 100, 100, 100, 92-87% of color, Cr, NH₃-N, and COD removal, respectively. Mahtab et al. (2009) evaluated combined system of coagulation and adsorption for wastewater processing with using different coagulants like lime, ferric chloride, ferrous sulfate, and alum. The process delivered optimum reduction up to 92% removal of COD by using alum. Table 2 shows researches results on combined or hybrid systems for the last five years. In addition, figure 7 presents the achievement of stand-alone technologies versus their hybrid systems.



Stand-alone vs. Hybrid system

Figure 7. stand-alone technologies versus their hybrid systems. Where FL is flocculation, AD is adsorption, and ED is electrodialysis

		Hybrid systems for wastew		
Hybrid System	Wastewater	Characteristics	Results	Ref.
Anaerobic Hybrid	Slaughter	pH (6.9-7.1), COD	COD (86.0%-93.58%), BOD	[85]
Reactor Packed with	House	(27800), BOD	(88.9%-95.71%), HRT (1)	
Special Floating	Wastewater	(16680), Oil and grease		
Media Hybrid anaerobic	Doim	(246) Organic loading rate	COD (87.86±2.12%), biogas yield	[86]
baffled reactors	Dairy wastewater	$(OLR) (3.33 \pm 0.03),$	(155.80 ± 7.02) , sludge yield (0.067)	[00]
burned reactors	wastewater	packed with sponge	(155.00 ± 1.02) , studge yield (0.007)	
		media characterized by		
		specific surface area		
		(157), density (65), and		
		voids ratio (0.65)		
SBR–FO	Synthetic	COD (439.47), TN	Dissolved organic carbon (DOC)	[87]
	domestic	(60.23), P (9.42)	(98.55%), TN (62.4%), nitrate	
	wastewater		(58.4%), nitrite (96.2%) ammonium	
		U (7.01) NO. (0.050)	(88.4%), phosphate (100%)	1001
Hybrid Constructed Wetland	Domestic Wastewater	pH (7.91), NO ₂ (0.059), NO ₃ (2.83),	HRT (20), COD (97.55%), BOD5 (97.5%), PO ₄ (89.35%), SO ₄	[88]
wettallu	w aste water	PO_4 (0.197), SO_4 (0.095),	$(97.5\%), FO_4 (89.55\%), SO_4$ $(80.75\%), NO_3 (96.04\%), NO_2$	
		total dissolved solids	(91.52%), fecal coliforms $(98.6%)$	
		(TDS) (480), electrical	() 110 2 /0), 100 21 00 110 () 010 /0)	
		conductivity (EC) (510),		
		Cl (35.87), TSS (478),		
		DO (2.5), BOD5		
		(134.83), COD (199.23)		
Hybrid moving bed	Municipal	Hydraulic load (2208),	TSS (63%), COD (56%), BOD	[89]
biofilm reactor	wastewater	TSS (28), COD (214),	(74%), TKN (85%), TN (20%)	
(MBBR)		BOD (111), total kjeldahl		
		nitrogen (TKN) (41.3), TN (41.3)		
Adsorption-	Biologically	TOC (1.6–3.8), Turbidity	TOC (99.7%), PO ₄ -3 (94%)	[90]
Flocculation-MF	treated	$(0.8-6), PO_4^{-3} (0.5-12),$		[> 0]
	wastewater	SS (2–15)		
EC- electro dialysis	Tannery	pH (4.10) at T (6.5),	COD (92%), NH ₃ -N (100%), Cr	[91]
(ED)	wastewater	Conductivity (11.71),	(100%) and color (100%) were	
		COD (2200-3000), SS	based on conductivity value (0.371)	
		(912), Color (824), NH ₃ -	at 45 minutes, and by using	
	D	N (180)	aluminum electrodes	[0 0]
UF-osmotic	Raw	-	COD (96%), TN (82%), P (99%)	[92]
membrane bioreactors Ultrasonic-Membrane	wastewater POME	BOD (437.31), COD	HRT (11), sonication operation	[93]
Anaerobic System	TOME	(42800), total solid (TS)	$(2 \text{ hr.}), \text{COD} (98.75\%), \text{CH}_4$	[א]
(UMAS)		(11740), volatile	generation (32,595)	
()		suspended solid (VSS)	8	
		(13270), T (55), pH		
		(3.97)		
Fenton and	Petroleum	BOD5 (173), COD	COD (76.5%), BOD (37.6%), TOC	[94]
sequencing batch	refinery	(1259), TOC (186), DO	(45.0%), oil and grease (100%)	
reactor (FE-SBR)	wastewater	(3), pH (9.4), TSS (124),		
	DOME	Oil and grease (233)		[0.67
HUASB reactor	POME	COD (47750), TN (817.5), TD (272.5), TSS	COD (82%), TSS (80%), turbidity	[95]
		(817.5), TP (272.5), TSS (9225), Color (5975)	(45%), HRT (57)	
		(9225), Color (5975), turbidity (5887), pH		
		(4.45)		

Table 2. Hybrid systems for wastewater treatment

OLR (g-COD/L.d), Hydraulic load (m³/d), Turbidity (NTU), T (°C), Conductivity (mS.cm⁻¹), biogas yield (mL.CH₄/g. COD_r), sludge yield (g.VSS/g.COD), HRT (day), gas size (ml), specific surface area (m²/m³), density (kg/m³), the rest is in mg/l, except pH.

3. Acknowledgment

S. K. Al-Amshawee introduced and wrote the paper. M. Y. Yunus supervised the paper to ensure the quality. This research work is financially supported by the Fundamental Research Grant Scheme (FRGS/UMP.05/25.12/04/01/1) with the RDU number RDU190160 which is awarded by the Ministry of Higher Education Malaysia (MOHE) via Research and Innovation Department, Universiti Malaysia Pahang (UMP) Malaysia.

4. Conclusion and Future trends

Majority of the reviewed hybrid systems show great capability to lead wastewater treatment. For instance, Mahmoud et al. (2014) proved that using a hybrid system involving anaerobic baffled reactor is highly efficient than using the conventional method [86]. In addition, the hybrid system had reduced $87.86\pm2.12\%$ of COD, while the conventional anaerobic baffled reactor had delivered $72.50\pm2.40\%$ of COD for dairy wastewater treatment.

Hybrid system empowers and raises the treatment quality, and possibly able to eliminate several core weaknesses. On the other hand, there are disadvantage like limited energy generation, slow treatment, costly, and vast dosage of wastes.

It is important to knock out the negative aspects and produce a concrete hybrid system involving quality, performance, low operation and maintenance requirement, ecofriendly, cost-effective, and energy productive. In addition, a lot of R&D are occurring on different combinations. Lastly, Global warming, pollution, and contamination, won't stop and wait us till we achieve the optimistic operation, it's quite depressed to notice pollution rises in vast amounts over the planet, and between us, while we are highly powered to defeat it.

5. References

- [1] Jury W A and Vaux H J 2007 The Emerging Global Water Crisis: Managing Scarcity and Conflict Between Water Users. *Adv. Agron.* **95** 1–76.
- [2] Yang H and Abbaspour K C 2007 Analysis of wastewater reuse potential in Beijing. *Desalination* **212** 238–50.
- [3] Sajjad A-A, Yunus M Y B M, Azoddein A A M, Hassell D G, Dakhil I H and Hasan H A 2019 Electrodialysis Desalination for Water and Wastewater: A Review. *Chem. Eng. J.* **380** 122231.
- [4] Shyue Koong Chang and Schonfeld P M 1991 Multiple period optimization of bus transit systems. *Transp. Res. Part B* **25** 453–78.
- [5] Vymazal J 2005 Horizontal sub-surface flow and hybrid constructed wetlands systems for wastewater treatment. *Ecol. Eng.* **25** 478–90.
- [6] Awalludin M F, Sulaiman O, Hashim R and Nadhari W N A W 2015 An overview of the oil palm industry in Malaysia and its waste utilization through thermochemical conversion, specifically via liquefaction. *Renew. Sustain. Energy Rev.* **50** 1469–84.
- [7] Bala J D, Lalung J and Ismail N 2014 Palm Oil Mill Effluent (POME) Treatment "Microbial Communities in an Anaerobic Digester": A Review. *Int. J. Sci. Res. Publ.* **4** 1–24.
- [8] Wu T Y, Mohammad A W, Jahim J M and Anuar N 2010 Pollution control technologies for the treatment of palm oil mill effluent (POME) through end-of-pipe processes. J. Environ. Manage. 91 1467–90.
- [9] Ahmed Y, Yaakob Z, Akhtar P and Sopian K 2015 Production of biogas and performance evaluation of existing treatment processes in palm oil mill effluent (POME). *Renew. Sustain. Energy Rev.* **42** 1260–78.
- [10] Udo de Haes H A and Heijungs R 2007 Life-cycle assessment for energy analysis and management. *Appl. Energy* **84** 817–27.
- [11] Chu H qiang, Cao D wen, Jin W and Dong B zhi 2008 Characteristics of bio-diatomite dynamic membrane process for municipal wastewater treatment. *J. Memb. Sci.* **325** 271–6.

- [12] Ben Aim R M and Semmens M J 2003 Membrane bioreactors for wastewater treatment and reuse: a success story. *Water Sci. Technol.* **47** 1–5.
- [13] Rosenberger S, Krüger U, Witzig R, Manz W, Szewzyk U and Kraume M 2002 Performance of a bioreactor with submerged membranes for aerobic treatment of municipal waste water. *Water Res.* 36 413–20.
- [14] Krauth K and Staab K F 1993 Pressurized bioreactor with membrane filtration for wastewater treatment. *Water Res.* **27** 405–11.
- [15] Davies W J, Le M S and Heath C R 1998 Intensified activated sludge process with submerged membrane microfiltration. *Water Sci. Technol.* **38** 421–8.
- [16] Li H, Yang M, Zhang Y, Yu T and Kamagata Y 2006 Nitrification performance and microbial community dynamics in a submerged membrane bioreactor with complete sludge retention. J. *Biotechnol.* 123 60–70.
- [17] Tee P F, Abdullah M O, Tan I A W, Rashid N K A, Amin M A M, Nolasco-Hipolito C and Bujang K 2016 Review on hybrid energy systems for wastewater treatment and bio-energy production. *Renew. Sustain. Energy Rev.* 54 235–46.
- [18] K. Wang L, Hung Y-T and K. Shammas N 2005 *Physicochemical Treatment Processes*. **3** (Humana Press).
- [19] Satyanarayan S, Ramakant and Vanerkar A P 2005 Conventional approach for abattoir wastewater treatment. *Environ. Technol.* **26** 441–7.
- [20] Bolto B and Gregory J 2007 Organic polyelectrolytes in water treatment. *Water Res.* **41** 2301–24.
- [21] Liimatainen H, Sirviö J, Sundman O, Hormi O and Niinimäki J 2012 Use of nanoparticular and soluble anionic celluloses in coagulation-flocculation treatment of kaolin suspension. *Water Res.* 46 2159–66.
- [22] Hokkanen S, Repo E and Sillanpää M 2013 Removal of heavy metals from aqueous solutions by succinic anhydride modified mercerized nanocellulose. *Chem. Eng. J.* **223** 40–7.
- [23] Amuda O S and Alade A 2006 Coagulation/flocculation process in the treatment of abattoir wastewater. *Desalination* **196** 22–31.
- [24] Pogaku R, Bono A and Chu C 2013 Developments in sustainable chemical and bioprocess technology. (Springer US).
- [25] Randall C W and Sen D 1996 Full-scale evaluation of an integrated fixed-film activated sludge (IFAS) process for enhanced nitrogen removal. *Water Sci. Technol.* **33** 155–62.
- [26] Sriwiriyarat T and Randall C W 2005 Evaluation of integrated fixed film activated sludge wastewater treatment processes at high mean cells residence time and low temperatures. *J. Environ. Eng.* **131** 1550–6.
- [27] Boltz J P, Johnson B R, Daigger G T and Sandino J 2009 Modeling integrated fixed-film activated sludge and moving-bed biofilm reactor systems I: mathematical treatment and model development. *Water Environ. Res.* **81** 555–75.
- [28] Di Trapani D, Christensson M, Torregrossa M, Viviani G and Ødegaard H 2013 Performance of a hybrid activated sludge/biofilm process for wastewater treatment in a cold climate region: Influence of operating conditions. *Biochem. Eng. J.* 77 214–9.
- [29] Kim H su, Gellner J W, Boltz J P, Freudenberg R G, Gunsch C K and Schuler A J 2010 Effects of integrated fixed film activated sludge media on activated sludge settling in biological nutrient removal systems. *Water Res.* **44** 1553–61.
- [30] Mahendran B, Lishman L and Liss S N 2012 Structural, physicochemical and microbial properties of flocs and biofilms in integrated fixed-film activated sludge (IFFAS) systems. *Water Res.* **46** 5085–101.
- [31] Hamoda M F and Al-Sharekh H A 2000 Performance of a combined biofilm-suspended growth system for wastewater treatment. *Water Sci. Technol.* **41** 167–75.
- [32] Christensson M and Welander T 2004 Treatment of municipal wastewater in a hybrid process using a new suspended carrier with large surface area. *Water Sci. Technol.* **49** 207–14.

- [33] Wang S, Chandrasekhara Rao N, Qiu R and Moletta R 2009 Performance and kinetic evaluation of anaerobic moving bed biofilm reactor for treating milk permeate from dairy industry. *Bioresour. Technol.* **100** 5641–7.
- [34] Seetha N, Bhargava R and Kumar P 2010 Effect of organic shock loads on a two-stage activated sludge-biofilm reactor. *Bioresour. Technol.* **101** 3060–6.
- [35] Bassin J P, Dezotti M and Sant'Anna G L 2011 Nitrification of industrial and domestic saline wastewaters in moving bed biofilm reactor and sequencing batch reactor. J. Hazard. Mater. 185 242–8.
- [36] Falås P, Baillon-Dhumez A, Andersen H R, Ledin A and La Cour Jansen J 2012 Suspended biofilm carrier and activated sludge removal of acidic pharmaceuticals. *Water Res.* **46** 1167–75.
- [37] Meng F, Yang F, Xiao J, Zhang H and Gong Z 2006 A new insight into membrane fouling mechanism during membrane filtration of bulking and normal sludge suspension. J. Memb. Sci. 285 159–65.
- [38] Lim A L and Bai R 2003 Membrane fouling and cleaning in microfiltration of activated sludge wastewater. *J. Memb. Sci.* **216** 279–90.
- [39] Liu Q, Wang X C, Liu Y, Yuan H and Du Y 2010 Performance of a hybrid membrane bioreactor in municipal wastewater treatment. *Desalination* **258** 143–7.
- [40] Dolar D, Gros M, Rodriguez-Mozaz S, Moreno J, Comas J, Rodriguez-Roda I and Barceló D 2012 Removal of emerging contaminants from municipal wastewater with an integrated membrane system, MBR-RO. J. Hazard. Mater. 239–240 64–9.
- [41] Chon K, Cho J and Shon H K 2013 Fouling characteristics of a membrane bioreactor and nanofiltration hybrid system for municipal wastewater reclamation. *Bioresour. Technol.* 130 239–47.
- [42] Damayanti A, Ujang Z and Salim M R 2011 The influenced of PAC, zeolite, and Moringa oleifera as biofouling reducer (BFR) on hybrid membrane bioreactor of palm oil mill effluent (POME). *Bioresour. Technol.* **102** 4341–6.
- [43] Rashidi H R, Sulaiman N M N and Hashim N A 2012 Batik Industry Synthetic Wastewater Treatment Using Nanofiltration Membrane. *Procedia Eng.* **44** 2010–2.
- [44] Rautenbach R and Gröschl A 1990 Separation potential of nanofiltration membranes. *Desalination* **77** 73–84.
- [45] Stoquart C, Servais P, Bérubé P R and Barbeau B 2012 Hybrid Membrane Processes using activated carbon treatment for drinking water: A review. *J. Memb. Sci.* **411–412** 1–12.
- [46] Nguyen T T, Ngo H H and Guo W 2013 Pilot scale study on a new membrane bioreactor hybrid system in municipal wastewater treatment. *Bioresour. Technol.* **141** 8–12.
- [47] Rodríguez-Hernández L, Esteban-García A L and Tejero I 2014 Comparison between a fixed bed hybrid membrane bioreactor and a conventional membrane bioreactor for municipal wastewater treatment: A pilot-scale study. *Bioresour. Technol.* **152** 212–9.
- [48] Ellouze E, Tahri N and Amar R Ben 2012 Enhancement of textile wastewater treatment process using Nanofiltration. *Desalination* **286** 16–23.
- [49] Yang T, Ma Z F and Yang Q Y 2011 Formation and performance of Kaolin/MnO2 bi-layer composite dynamic membrane for oily wastewater treatment: Effect of solution conditions. *Desalination* 270 50–6.
- [50] Smith A L, Skerlos S J and Raskin L 2013 Psychrophilic anaerobic membrane bioreactor treatment of domestic wastewater. *Water Res.* **47** 1655–65.
- [51] Ma D, Gao B, Hou D, Wang Y, Yue Q and Li Q 2013 Evaluation of a submerged membrane bioreactor (SMBR) coupled with chlorine disinfection for municipal wastewater treatment and reuse. *Desalination* **313** 134–9.
- [52] Zeng Y, Yang C, Zhang J and Pu W 2007 Feasibility investigation of oily wastewater treatment by combination of zinc and PAM in coagulation/flocculation. *J. Hazard. Mater.* **147** 991–6.
- [53] Kim J, Kim K, Ye H, Lee E, Shin C, McCarty P L and Bae J 2011 Anaerobic fluidized bed membrane bioreactor for wastewater treatment. *Environ. Sci. Technol.* **45** 576–81.

- [54] Verstraete W and Vandevivere P 1999 New and broader applications of anaerobic digestion. *Crit. Rev. Environ. Sci. Technol.* **29** 151–73.
- [55] Lo C H, Onstott T C, Chen C H and Lee T 1994 An assessment of 40Ar39Ar dating for the wholerock volcanic samples from the Luzon Arc near Taiwan. *Chem. Geol.* **114** 157–78.
- [56] Shivayogimath C B and Ramanujam T K 1999 Treatment of distillery spentwash by hybrid UASB reactor. *Bioprocess Eng.* **21** 255–9.
- [57] Lew B, Tarre S, Belavski M and Green M 2004 UASB reactor for domestic wastewater treatment at low temperatures: A comparison between a classical UASB and hybrid UASB-filter reactor. *Water Sci. Technol.* **49** 295–301.
- [58] Ozturk I, Eroglu V, Ubay G and Demir I 1993 Hybrid upflow anaerobic sludge blanket reactor (HUASBR) treatment of dairy effluents. *Water Sci. Technol.* **28** 77–85.
- [59] Tur M Y and Huang J C 1997 Treatment of phthalic waste by anaerobic hybrid reactor. J. *Environ. Eng.* **123** 1093–9.
- [60] Xu H, Xu W and Wang J 2011 Degradation kinetics of azo dye reactive Red SBE wastewater by complex ultraviolet and hydrogen peroxide process. *Environ. Prog. Sustain. Energy* **30** 208–15.
- [61] Zuorro A and Lavecchia R 2014 Evaluation of UV/H2O2 advanced oxidation process (AOP) for the degradation of diazo dye Reactive Green 19 in aqueous solution. *Desalin. Water Treat.* 52 1571–7.
- [62] Zuorro A, Fidaleo M and Lavecchia R 2013 Response surface methodology (RSM) analysis of photodegradation of sulfonated diazo dye Reactive Green 19 by UV/H2O2 process. J. Environ. Manage. 127 28–35.
- [63] Aleboyeh A, Moussa Y and Aleboyeh H 2005 The effect of operational parameters on UV/H2O2 decolourisation of Acid Blue 74. *Dye. Pigment.* **66** 129–34.
- [64] Autin O, Hart J, Jarvis P, MacAdam J, Parsons S A and Jefferson B 2012 Comparison of UV/H2O2 and UV/TiO2 for the degradation of metaldehyde: Kinetics and the impact of background organics. *Water Res.* 46 5655–62.
- [65] Banat F, Al-Asheh S, Al-Rawashdeh M and Nusair M 2005 Photodegradation of methylene blue dye by the UV/H2 O2 and UV/acetone oxidation processes. *Desalination* **181** 225–32.
- [66] Li W, Lu S, Qiu Z and Lin K 2011 UV and VUV photolysis vs. UV/H2O2 and VUV/H2O2 treatment for removal of clofibric acid from aqueous solution. *Environ. Technol.* **32** 1063–71.
- [67] Malik P K and Sanyal S K 2004 Kinetics of decolourisation of azo dyes in wastewater by UV/H2O2 process. *Sep. Purif. Technol.* **36** 167–75.
- [68] Shu H Y, Fan H J, Chang M C and Hsieh W P 2006 Treatment of MSW landfill leachate by a thin gap annular UV/H 2O2 photoreactor with multi-UV lamps. *J. Hazard. Mater.* **129** 73–9.
- [69] Yonar T, Kestioglu K and Azbar N 2006 Treatability studies on domestic wastewater using UV/H2O2 process. *Appl. Catal. B Environ.* **67** 223–8.
- [70] Muruganandham M and Swaminathan M 2006 Advanced oxidative decolourisation of Reactive Yellow 14 azo dye by UV/TiO2, UV/H2O2, UV/H2O2/Fe2+ processes - A comparative study. *Sep. Purif. Technol.* 48 297–303.
- [71] Shu H Y and Chang M C 2005 Decolorization and mineralization of a phthalocyanine dye C.I. Direct Blue 199 using UV/H2O2 process. *J. Hazard. Mater.* **125** 96–101.
- [72] Schrank S G, Santos J N R dos, Souza D S and Souza E E S 2007 Decolourisation effects of Vat Green 01 textile dye and textile wastewater using H2O2/UV process. J. Photochem. Photobiol. A Chem. 186 125–9.
- [73] Shu H Y and Chang M C 2005 Pilot scale annular plug flow photoreactor by UV/H2O2 for the decolorization of azo dye wastewater. *J. Hazard. Mater.* **125** 244–51.
- [74] Hartmann M, Kullmann S and Keller H 2010 Wastewater treatment with heterogeneous Fentontype catalysts based on porous materials. *J. Mater. Chem.* **20** 9002–17.
- [75] Olson T M and Barbier P F 1994 Oxidation kinetics of natural organic matter by sonolysis and ozone. *Water Res.* **28** 1383–91.
- [76] Larsen N W, Sehested T and Pedersen J 1991 Isotopic study of the mechanism of ozone

formation. Chem. Informationsd. 23 331-43.

- [77] Gogate P R 2002 Cavitation: An auxiliary technique in wastewater treatment schemes. *Adv. Environ. Res.* **6** 335–58.
- [78] Kumar A, Gogate P R and Pandit A B 2007 Mapping of acoustic streaming in sonochemical reactors. *Ind. Eng. Chem. Res.* **46** 4368–73.
- [79] Pang Y L, Abdullah A Z and Bhatia S 2011 Review on sonochemical methods in the presence of catalysts and chemical additives for treatment of organic pollutants in wastewater. *Desalination* 277 1–14.
- [80] Mahamuni N N and Adewuyi Y G 2010 Advanced oxidation processes (AOPs) involving ultrasound for waste water treatment: A review with emphasis on cost estimation. *Ultrason. Sonochem.* **17** 990–1003.
- [81] Mason T J 2000 Large scale sonochemical processing: Aspiration and actuality. *Ultrason.* Sonochem. **7** 145–9.
- [82] Moholkar V S, Senthil Kumar P and Pandit A B 1999 Hydrodynamic cavitation for sonochemical effects. *Ultrason. Sonochem.* **6** 53–65.
- [83] Ma Y S and Sung C F 2010 Investigation of carbofuran decomposition by a combination of ultrasound and Fenton process. *Sustain. Environ. Res.* **20** 213–9.
- [84] Zou S, Gu Y, Xiao D and Tang C Y 2011 The role of physical and chemical parameters on forward osmosis membrane fouling during algae separation. *J. Memb. Sci.* **366** 356–62.
- [85] Sunder G C and Satyanarayan S 2013 Efficient Treatment of Slaughter House Wastewater by Anaerobic Hybrid Reactor Packed with Special Floating Media. Int. J. Chem. Phys. Sci. 2 73– 81.
- [86] Nasr M, Khalil A, Abdel-Kader A, Elbarki W and Moustafa M 2014 Comparative performance between conventional and hybrid anaerobic baffled reactors for treating dairy wastewater. *Int. J. Chem. Environ. Eng.* **5**.
- [87] Linares R V, Li Z, Yangali-Quintanilla V, Li Q, Vrouwenvelder J S, Amy G L and Ghaffour N 2016 Hybrid SBR–FO system for wastewater treatment and reuse: Operation, fouling and cleaning. *Desalination* 393 31–8.
- [88] Sehar S, Aamir R, Naz I, Ali N and Ahmed S 2013 Reduction of Contaminants (Physical, Chemical, and Microbial) in Domestic Wastewater through Hybrid Constructed Wetland. *ISRN Microbiol.* 2013 1–9.
- [89] Falletti L, Conte L and Maestri A 2014 Upgrading of a wastewater treatment plant with a hybrid moving bed biofilm reactor (MBBR). *AIMS Environ. Sci.* **1** 45–52.
- [90] Guo W S, Vigneswaran S, Ngo H H and Chapman H 2004 Experimental investigation of adsorption-flocculation-microfiltration hybrid system in wastewater reuse. J. Memb. Sci. 242 27– 35.
- [91] Deghles A and Kurt U 2016 Treatment of tannery wastewater by a hybrid electrocoagulation/electrodialysis process. *Chem. Eng. Process. Process Intensif.* **104** 43–50.
- [92] Holloway R W, Wait A S, Fernandes da Silva A, Herron J, Schutter M D, Lampi K and Cath T Y 2015 Long-term pilot scale investigation of novel hybrid ultrafiltration-osmotic membrane bioreactors. *Desalination* 363 64–74.
- [93] Abdurahman N H, Rosli Y M and Azhari N H 2011 Development of a membrane anaerobic system (MAS) for palm oil mill effluent (POME) treatment. *Desalination* **266** 208–12.
- [94] Diya'uddeen B H, Rahim Pouran S, Abdul Aziz A R, Nashwan S M, Wan Daud W M A and Shaaban M G 2015 Hybrid of Fenton and sequencing batch reactor for petroleum refinery wastewater treatment. *J. Ind. Eng. Chem.* **25** 186–91.
- [95] Habeeb S A, Aziz A B, Latiff A, Daud Z and Ahmad Z 2011 A biodegradation and treatment of palm oil mill effluent (POME) using a hybrid up-flow anaerobic sludge bed (HUASB) reactor. *Int. J. Energy Environmental* 2 653–60.