# DEVELOPMENT OF DISH-STIRLING CONCENTRATING SOLAR THERMAL-ELECTRIC ENERGY CONVERSION SYSTEM

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### ABSTRACT

Sunlight is the world's largest renewable energy source. Using the existing technologies, this energy can provide the needs of all the people on Earth. By increasing the solar-to-electric energy conversion efficiency while maintaining the cost and lifespan of a machine, conventional photovoltaic technology is being progressively challenged by concentrated solar thermal engine technology especially in large scale power plant. For local research, the limitation of technological development between technical potential and practical utilisation of solar energy becomes one of the reasons behind the minimum growth of solar energy field. Owning a local renewable energy conversion system means decrease fossil fuel dependability, secure near to long term power supply chain and hence enhances economic development. In order to develop local expertise with low production cost, full scaled dish-Stirling CST based on DNI solar flux modules were prototyped. The development of the research began with a preliminary assessment on a 2m diameter manual operated ideal paraboloid concentrating dish prototype. Based on the important design parameters and followed by rigorous system design principles, an 8m diameter combined paraboloid-Fresnel concentrating dish with low focus height, low dish height and minimal wind resistance was designed and constructed. Using the hydraulic-electric two-axis solar tracking system, the proposed system was able to move  $0-90^{\circ}$  in Azimuth axis and  $+/-180^{\circ}$  in elevation axis for the full day solar tracking with the consideration of yearly solar path variation. For the thermal-to-mechanical energy conversion, a compact and superior combination of square configuration, four cylinders rhombic drive beta drive mechanism Stirling engine system was integrated with the concentrating dish and tracking mechanism. Throughout the research and development, detailed investigations were conducted to achieve correct operation of the actual prototype. Referring to the 3D model, these studies, including a 3D ray trace analysis on the dish's focal region solar flux concentration pattern, influent of Azimuth angle offset on the thermal receiver performance, air flow simulation on +/- 0 to 28m/s wind load, coefficient of drag comparison and stress distribution due to wind and structural loads. From the computational and operating analysis, the paraboloid-Fresnel dish showed 34.9 to 38.3% of wind load reduction compared with ideal paraboloid design, low  $C_D$  in between 0.077 to 0.76 depends on wind flow direction and rotating angle. Together with structural mass, stress simulation indicated maximum stress of 320.6MN/m<sup>2</sup> and was validated with six components failure. Meanwhile, practical model showed 51% of structural stress reduction after continuous design improvement. Next, focal region temperature readings were recorded under various circumferences, and maximum concentrated temperature of 357°C had agreed the research hypothesis that specific thermal receiver design can store the solar flux at higher intensity. After several cranking tests, the prototype Stirling engine was unable to start as designed due to scattered solar thermal distribution. Based on Schmidt's analysis, the predicted engine output power was 6.03kW. Considering the total energy consumption for PLC, electric motor, hydraulic system and auxiliary system, the net power output was predicted at 5.759kW. Based on 1000W/m<sup>2</sup> solar DNI, the energy conversion efficiency for 8m diameter concentrating dish was predicted at 11.52%.

### ABSTRAK

Cahaya matahari adalah sumber tenaga boleh diperbaharui yang terbesar di dunia. Dengan menggunakan teknologi yang sedia ada, tenaga ini boleh menyediakan keperluan semua manusia di Bumi. Dengan meningkatkan kecekapan penukaran tenaga solar untuk elektrik sementara mengekalkan kos dan jangka hayat mesin, teknologi photovoltaic konvensional sedang beransur-ansur dicabar oleh tertumpu solar enjin teknologi haba terutama di loji kuasa secara besar-besaran. Bagi penyelidikan tempatan, had pembangunan teknologi antara potensi teknikal dan praktikal penggunaan tenaga solar menjadi salah satu daripada sebab-sebab di sebalik pertumbuhan bertakung bidang tenaga solar. Memiliki sistem penukaran tenaga tempatan yang boleh diperbaharui ertinya mengurangkan pergantungan pada bahan api fosil, kekalkan rantaian bekalan kuasa jangka panjang dan dengan itu meningkatkan pembangunan ekonomi. Dalam usaha untuk membangunkan kepakaran tempatan dengan kos pengeluaran yang rendah, piring/Stirling CST berskala penuh berdasarkan modul fluks solar DNI telah dibangunkan. Pembangunan penyelidikan bermula dengan penilaian awal mengenai piring paraboloid diameter 2m. Berdasarkan parameter reka bentuk yang penting dan diikuti dengan prinsip-prinsip reka bentuk sistem ketat, piring diameter 8m hasil gabungan paraboloid-Fresnel dengan ketinggian tumpuan dan tinggi piring yang rendah, serta rintangan angin minimum telah ditakrifkan dan dibina. Menggunakan hidraulik elektrik dua paksi Penjejakan sistem solar, sistem yang dicadangkan mampu untuk bergerak 0-90° dalam Azimut paksi dan +/-180° dalam paksi ketinggian untuk Penjejakan hari solar penuh dengan mengambil kira perubahan laluan solar tahunan. Untuk penukaran tenaga terma kepada mekanikal, kombinasi yang padat dan atasan konfigurasi persegi, empat silinder berbentuk rhombic drive enjin Stirling jenis beta bersepadu dengan piring penggumpulan cahaya matahari serta mekanisme pengesan. Sepanjang penyelidikan dan pembangunan, siasatan terperinci dijalankan untuk mencapai pengendalian yang betul bagi prototaip sebenar. Merujuk kepada model 3D, kajian termasuk ray 3D surih analisis di rantau tumpuan pring kepekatan corak fluks. kesan sudut Azimut diimbangi prestasi penerima haba, udara simulasi aliran dari 0-28m/s angin beban, pekali perbandingan seret dan agihan tegasan yang disebabkan oleh angin dan beban struktur. Dari analisis pengiraan dan operasi, piring paraboloid-Fresnel menunjukkan 34.9-38.3% pengurangan beban angin berbanding dengan reka bentuk paraboloid yang ideal, C<sub>D</sub> rendah di antara 0.077-0.76 bergantung kepada arah aliran angin dan sudut berputar. Bersama-sama dengan jisim struktur, simulasi tekanan menunjukkan tegasan maksimum 320.6MN/m<sup>2</sup> dan disahkan dengan enam komponen kegagalan. Sementara itu, model praktikal menunjukkan 51% daripada pengurangan tekanan struktur selepas peningkatan reka bentuk yang berterusan. Seterusnya, fokus rantau bacaan suhu dicatatkan di bawah keadaan pelbagai, dan suhu maksimum pekat 357°C telah bersetuju hipotesis penyelidikan bahawa penerima reka bentuk haba tertentu boleh menyimpan fluks solar pada intensiti yang lebih tinggi. Selepas beberapa ujian cuba hidupkan enjin, prototaip Stirling enjin tidak dapat beroperasi seperti yang direka bentuk kerana rata berselerak panas matahari. Berdasarkan analisis Schmidt, kuasa enjin yang diramalkan adalah 6.03kW. Dengan mengambil kira jumlah penggunaan tenaga untuk PLC, motor elektrik, sistem hidraulik dan sistem bantu, kuasa keluaran bersih diramalkan pada 5.759kW. Berdasarkan 1000W/m<sup>2</sup> solar DNI, kecekapan penukaran tenaga bagi piring diameter 8m telah diramalkan pada 11.52%.

# **TABLE OF CONTENTS**

.

|              |  | Page |
|--------------|--|------|
| SUPERVISOF   | <b>R'S DECLARATION</b>                       | ii   |
| CANDIDATE    | 'S DECLARATION                               | iii  |
| DEDICATION   | 1  | iv   |
| ACKNOWLE     | DGEMENTS                                     | v    |
| ABSTACT      |  | vi   |
| ABSTRAK      |  | vii  |
| TABLE OF CO  | ONTENTS                                      | viii |
| LIST OF TAB  | LES  | xii  |
| LIST OF FIGU | JRES   | xiii |
| LIST OF ABB  | REVIATIONS                                   | xix  |
| CHAPTER 1    | INTRODUCTION                                 | 1    |
| 1.1          | Background Study on Solar Power              | 1    |
| 1.2          | Problem Statement                            | 3    |
| 1.3          | Objectives                                   | 4    |
| 1.4          | Work Scope                                   | 5    |
| 1.5          | Hypothesis                                   | 5    |
| 1.6          | Flow Chart                                   | 6    |
| 1.7          | Schedule of Work                             | 7    |
| CHAPTER 2    | LITERATURE REVIEW                            | 8    |
| 2.1          | Sustainability and Energy from Nature        | 8    |
| 2.2          | Energy Transition to Renewable Resources     | 9    |
| 2.3          | Solar Irradiation Distribution and Potential | 11   |
| 2.4          | Worldwide and Local Renewable Energy on      | 12   |
|              | Demand                                       | 15   |
| 2.5          | Concentrating Solar Power                    | 15   |

viii

| 2.6   | <ul> <li>2.5.1 Concentrating Solar Thermal Energy</li> <li>2.5.2 Comparison of Various CST Systems</li> <li>2.5.3 Development of Concentrating Dish-<br/>Stirling</li> <li>Development of Stirling Engine</li> </ul>   | 18<br>20<br>24<br>28   |
|---|--|--|
| 2.0   | 2.6.1 Types of Stirling Engine   | 20<br>29   |
|   | 2.6.2 Stirling Engine for Solar Thermal Power  | 30   |
|   | 2.6.3 Ideal Stirling Cycle   | 31   |
|   | 2.6.4 Effect of Phase Angle and Practical Losses   | 30<br>40   |
|   | 2.6.6 Working Fluid Properties   | 42   |
|   | 2.6.7 Drive Mechanism  | 45   |
| 2.7   | Solar Concentrating System   | 47   |
|   | 2.7.1 Solar Flux Collector   | 47   |
|   | 2.7.2 Solar Thermal Receiver   | 50   |
|   | 2.7.3 Ray Trace of Focal Point Thermal   | - 52   |
|   | 2.7.4 Reflector and Receiver Material Properties   | 60   |
|   | 2.7.5 Mathematical Analysis  | 64   |
| 2.8   | Energy Storage and Hybridisation   | 69   |
| 2.9   | Solar Tracking   | 72   |
| CHAPTER 3   | METHODOLOGY  | 75   |
|   |  |  |
| 3.1   | Solar Irradiation Concentrator   | 76   |
| 3.1   | Solar Irradiation Concentrator<br>3.1.1 Feasibility Assessment of 2m Diameter<br>Concentrating Dish Technology   | 76<br>76   |
| 3.1   | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> </ul>  | 76<br>76<br>81   |
| 3.1   | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> <li>3.1.3 Solar Concentrating Dish Working Model<br/>Development</li> </ul>  | 76<br>76<br>81<br>89   |
| 3.1   | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> <li>3.1.3 Solar Concentrating Dish Working Model<br/>Development</li> <li>Two-axis Intermediate Solar Tracking System</li> </ul>   | 76<br>76<br>81<br>89<br>96   |
| 3.1<br>3.2  | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> <li>3.1.3 Solar Concentrating Dish Working Model<br/>Development</li> <li>Two-axis Intermediate Solar Tracking System</li> <li>3.2.1 System Operation Design</li> </ul>  | 76<br>76<br>81<br>89<br>96<br>97   |
| 3.1<br>3.2  | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> <li>3.1.3 Solar Concentrating Dish Working Model<br/>Development</li> <li>Two-axis Intermediate Solar Tracking System</li> <li>3.2.1 System Operation Design</li> <li>3.2.2 Working Model Development</li> </ul>   | 76<br>76<br>81<br>89<br>96<br>97<br>100                                    |
| 3.1<br>3.2<br>3.3   | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> <li>3.1.3 Solar Concentrating Dish Working Model<br/>Development</li> <li>Two-axis Intermediate Solar Tracking System</li> <li>3.2.1 System Operation Design</li> <li>3.2.2 Working Model Development</li> <li>Solar Thermal Receiver</li> </ul>   | 76<br>76<br>81<br>89<br>96<br>97<br>100<br>107                             |
| <ul> <li>3.1</li> <li>3.2</li> <li>3.3</li> <li>3.4</li> </ul>  | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> <li>3.1.3 Solar Concentrating Dish Working Model<br/>Development</li> <li>Two-axis Intermediate Solar Tracking System</li> <li>3.2.1 System Operation Design</li> <li>3.2.2 Working Model Development</li> <li>Solar Thermal Receiver</li> <li>Square Rhombic Drive Multi Cylinders Stirling</li> </ul>  | 76<br>76<br>81<br>89<br>96<br>97<br>100<br>107                             |
| <ul> <li>3.1</li> <li>3.2</li> <li>3.3</li> <li>3.4</li> </ul>  | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> <li>3.1.3 Solar Concentrating Dish Working Model<br/>Development</li> <li>Two-axis Intermediate Solar Tracking System</li> <li>3.2.1 System Operation Design</li> <li>3.2.2 Working Model Development</li> <li>Solar Thermal Receiver</li> <li>Square Rhombic Drive Multi Cylinders Stirling</li> <li>Engine Development</li> </ul>  | 76<br>76<br>81<br>89<br>96<br>97<br>100<br>107<br>112                      |
| <ul> <li>3.1</li> <li>3.2</li> <li>3.3</li> <li>3.4</li> <li>3.5</li> </ul>                           | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> <li>3.1.3 Solar Concentrating Dish Working Model<br/>Development</li> <li>Two-axis Intermediate Solar Tracking System</li> <li>3.2.1 System Operation Design</li> <li>3.2.2 Working Model Development</li> <li>Solar Thermal Receiver</li> <li>Square Rhombic Drive Multi Cylinders Stirling</li> <li>Engine Development</li> <li>Overall System Integration</li> </ul>  | 76<br>76<br>81<br>89<br>96<br>97<br>100<br>107<br>112                      |
| <ul> <li>3.1</li> <li>3.2</li> <li>3.3</li> <li>3.4</li> <li>3.5</li> <li>3.6</li> </ul>              | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> <li>3.1.3 Solar Concentrating Dish Working Model<br/>Development</li> <li>Two-axis Intermediate Solar Tracking System</li> <li>3.2.1 System Operation Design</li> <li>3.2.2 Working Model Development</li> <li>Solar Thermal Receiver</li> <li>Square Rhombic Drive Multi Cylinders Stirling</li> <li>Engine Development</li> <li>Overall System Integration</li> <li>Dish-Stirling Monitoring and Data Acquisition</li> </ul>   | 76<br>76<br>81<br>89<br>96<br>97<br>100<br>107<br>112<br>123<br>125        |
| <ul> <li>3.1</li> <li>3.2</li> <li>3.3</li> <li>3.4</li> <li>3.5</li> <li>3.6</li> </ul>              | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> <li>3.1.3 Solar Concentrating Dish Working Model<br/>Development</li> <li>Two-axis Intermediate Solar Tracking System</li> <li>3.2.1 System Operation Design</li> <li>3.2.2 Working Model Development</li> <li>Solar Thermal Receiver</li> <li>Square Rhombic Drive Multi Cylinders Stirling</li> <li>Engine Development</li> <li>Overall System Integration</li> <li>Dish-Stirling Monitoring and Data Acquisition</li> <li>System</li> </ul>   | 76<br>76<br>81<br>89<br>96<br>97<br>100<br>107<br>112<br>123<br>125        |
| <ul> <li>3.1</li> <li>3.2</li> <li>3.3</li> <li>3.4</li> <li>3.5</li> <li>3.6</li> <li>3.7</li> </ul> | <ul> <li>Solar Irradiation Concentrator</li> <li>3.1.1 Feasibility Assessment of 2m Diameter<br/>Concentrating Dish Technology</li> <li>3.1.2 Conceptual Design of 8m Diameter Solar<br/>Flux Concentrating Dish</li> <li>3.1.3 Solar Concentrating Dish Working Model<br/>Development</li> <li>Two-axis Intermediate Solar Tracking System</li> <li>3.2.1 System Operation Design</li> <li>3.2.2 Working Model Development</li> <li>Solar Thermal Receiver</li> <li>Square Rhombic Drive Multi Cylinders Stirling</li> <li>Engine Development</li> <li>Overall System Integration</li> <li>Dish-Stirling Monitoring and Data Acquisition</li> <li>System</li> <li>Computational Analysis of Dish-Stirling System</li> </ul> | 76<br>76<br>81<br>89<br>96<br>97<br>100<br>107<br>112<br>123<br>125<br>128 |

X

|           | 3.7.1   | Air Flow Analysis on Concentrating Dish                                   | 129 |
|-----------|---------|---|-----|
|           | 3.7.2   | Structural Analysis on Solar Concentrator<br>and Solar Tracking Mechanism | 130 |
|           | 3.7.3   | 3D Ray Trace Analysis on Concentrating Dish                               | 132 |
|           | 3.7.4   | Thermodynamic Analysis on Rhombic<br>Drive Beta Stirling Engine           | 135 |
| CHAPTER 4 | RESU    | LTS AND DISCUSSIONS   | 138 |
| 4.1       | Parabo  | oloid-Fresnel Concentrating Dish Design                                   | 138 |
|           | Param   | eters   |     |
| 4.2       | Solar I | rradiation Distribution on Focal Region                                   | 141 |
|           | 4.2.1   | DNI Distribution and Boundary Setting                                     | 142 |
|           | 4.2.2   | Solar Points Distribution   | 144 |
|           | 4.2.3   | Feasibility on Receiver/Secondary   | 147 |
|           |         | Reflector Design  |     |
| 4.3       | Dish-S  | tirling Working Model Development   | 151 |
|           | 4.3.1   | Concentrating Dish  | 151 |
|           | 4.3.2   | Two-axis Solar Tracking System  | 155 |
|           | 4.3.3   | Solar Thermal Receiver and Secondary<br>Reflector                         | 157 |
|           | 4.3.4   | Square Rhombic Drive Beta Stirling Engine                                 | 161 |
|           | 4.3.5   | Dish-Stirling System Integration and On-<br>Site Installation             | 169 |
| 4.4       | Air Flo | ow Simulation on Concentrating Dish                                       | 171 |
|           | 4.4.1   | Boundary Condition Setting  | 171 |
|           | 4.4.2   | Air Flow Distribution   | 173 |
|           | 4.4.3   | Force Effect for Focus Height and Dish<br>Height Variation                | 177 |
|           | 4.4.4   | Wind Drag Analysis  | 180 |
|           | 4.4.5   | Resultant Force on Hydraulic System                                       | 181 |
| 4.5       | Structu | ural Load Analysis  | 186 |
|           | 4.5.1   | Boundary Condition Setting  | 186 |
|           | 4.5.2   | Case 1 : Failure Analysis on Original<br>Prototype                        | 189 |
|           | 4.5.3   | Case 2: Design Refinement for Second<br>Prototype                         | 195 |
| 4.6       | Worki   | ng Model Analysis   | 202 |
|           | 4.6.1   | Solar Receiver and Secondary Reflector<br>Analysis                        | 202 |
|           | 4.6.2   | Concentrating Dish Operation  | 211 |
|           |         |   | 014 |
|           | 4.6.3   | Thermal Engine Operational Analysis                                       | 214 |

| CHAPTER 5  | CONCLUSION AND RECOMMENDATION                     | 238 |
|------------|---|-----|
|            |   |     |
| 5.1        | Research Summary                                  | 238 |
| 5.2        | Conclusions                                       | 239 |
| 5.3        | Recommendations                                   | 241 |
|            |   |     |
| REFERENCES |   | 243 |
| APPENDICES |   | 251 |
| А          | Research Gantt Chart                              | 252 |
| В          | Development of 2m Diameter Paraboloid             | 253 |
|            | Concentrating Dish                                |     |
| С          | Optimisation Calculation on Reflecting Angle and  | 256 |
|            | Dish Height Based on Paraboloid-Fresnel Principle |     |
| D          | Thermocouple Dimension and Installation           | 259 |
| E          | Direct Normal Irradiation Reading                 | 262 |
| F          | Solar Flux Distribution                           | 263 |
| G          | Dish-Stirling System Development                  | 273 |
| Н          | Air Flow Simulation                               | 284 |
| Ι          | Static and Wind Load Analysis                     | 288 |
| J          | Schmidt Cycle Analysis                            | 295 |
|            |   |     |

## LIST OF TABLES

| Table No. | Title   | Page |
|-----------|---|------|
| 2.1       | Comparison between various CST system                           | 23   |
| 2.2       | Development of dish-Stirling CST and technical                  | 25   |
|           | viability of this technology for generating power               |      |
| 2.3       | Parasitic losses in Stirling engine                             | 37   |
| 2.4       | Effect of regenerator on Stirling engine performance            | 39   |
|           | referred to GPU-3 model   |      |
| 2.5       | Working fluid properties comparison at 1 atm, 300K              | 43   |
| 2.6       | Specular reflectance values for different reflector             | 62   |
|           | materials   |      |
| 3.1       | Preliminary assessment on paraboloid concentrating              | 80   |
|           | dish with two-axis control mechanisms                           |      |
| 3.2       | Comparison of different reflecting shape                        | 83   |
| 3.3       | Various operation modes for concentrating dish                  | 100  |
| 3.4       | Dimension definitions for rhombic drive mechanism               | 114  |
| 3.5       | Static stress analysis solar concentrating system               | 134  |
| 4.1       | Boundary condition setting on 3D sun ray tracing and            | 143  |
| •         | focal region distribution                                       |      |
| 4.2       | Concentrating dish model dimension for air flow                 | 173  |
|           | simulation  |      |
| 4.3       | Air Flow result of Ideal Paraboloid I Design                    | 174  |
| 4.4       | Air Flow result of Ideal Paraboloid II Design                   | 175  |
| 4.5       | Air Flow result of Paraboloid-Fresnel Design                    | 176  |
| 4.6       | TDC and BDC for 44° phase angle rhombic drive system            | 216  |
| 4.7       | Engine volumetric displacement at TDC and BDC                   | 217  |
| 4.8       | Engine dynamic test conditions                                  | 218  |
| 4.9       | Summary of single cylinder thermodynamic                        | 228  |
|           | parameters  |      |
| 4.10      | Single and four cylinders configuration power output at 2000rpm | 230  |
| 4.11      | Total energy consumption analysis                               | 237  |

## LIST OF FIGURES

| Figure No. | Title  | Page |
|------------|--|------|
| 1.1        | Annual solar irradiance on Earth                               | 2    |
| 2.1        | Definition of sustainability                                   | 8    |
| 2.2        | Energy conversion scheme                                       | 9    |
| 2.3        | Solar irradiation versus established global energy             | 12   |
|            | resources  |      |
| 2.4        | Solar irradiation and yearly variations of the solar           | 12   |
|            | constant at outer atmosphere                                   |      |
| 2.5        | Sunbelt countries  | 13   |
| 2.6        | Estimate of the number of days where DNI falls below           | 16   |
|            | 3000kWh/m <sup>2</sup>   |      |
| 2.7        | Simplified analytic CSP solar output profile by time of        | 17   |
|            | the day  |      |
| 2.8        | Various concentrating solar power technologies                 | 18   |
| 2.9        | Performance of different solar systems                         | 19   |
| 2.10       | Dish engine system block diagram                               | 22   |
| 2.11       | Three basic mechanical configurations for Stirling             | 29   |
|            | engine   |      |
| 2.12       | Stirling cycle   | 32   |
| 2.13       | Ideal Stirling engine thermodynamic cycle                      | 33   |
| 2.14       | PV diagram for phase angle range between 0 to 175°             | 36   |
| 2.15       | Performance of different regenerator matrix porosity           | 40   |
|            | on various phase angle   |      |
| 2.16       | Variation of brake power with heat source temperature          | 42   |
| 2.17       | Possible concentrating collector configurations                | 48   |
|            | a. tubular absorbers with diffuse back reflector, b.           |      |
|            | tubular absorbers with specular cusp reflectors, c.            |      |
|            | plane receiver with plane reflectors, d. parabolic             |      |
|            | concentrator, e. Fresnel reflector, f. Linear Fresnel          | ÷.   |
|            | reflector with central receiver                                |      |
| 2.18       | Schematic diagram of relationship between Earth and            | 53   |
|            | Sun  |      |
| 2.19       | The thermal efficiency of a receiver $\eta_{th}$ as a function | 54   |
|            | of the fluid temperature $T_F$ and concentration factor C      |      |
|            | based on 800 $W/m^2$ solar irradiation                         |      |
| 2.20       | The laws of reflection and refraction                          | 55   |
| 2.21       | Modelling and sampled ray display generated from the           | 56   |
|            | ray tracing results  |      |
| 2.22       | Comparison of the radiative flux distribution between          | 57   |
|            | the real concentrator and the ideal paraboloidal               |      |
|            | concentrator for the real sun case                             |      |
| 2.23       | Effect of the receiver position on the radiation flux          | 58   |
|            | distribution and radiation collecting efficiency               |      |
| 2.24       | Variations in temperature for various radii                    | 59   |

| 2.25 | Types of reflection from surfaces  | 61  |
|------|--|-----|
| 2.26 | Solar Flux Map in the focal plane normalized to $1000 \text{W/m}^2$  | 64  |
| 2.27 | Schematic diagram for parabolic dish concentrating system  | 65  |
| 2.28 | Combination of storage and hybridisation in a solar plant  | 70  |
| 2.29 | Concept of Hydrogen internal combustion Stirling engine  | 72  |
| 2.30 | Definition of solar altitude and azimuth angles  | 73  |
| 2.31 | Various two-axis solar tracking system   | 74  |
| 3.1  | Solar thermal dish-Stirling development block diagram  | 75  |
| 3.2  | 2m diameter concentrating dish with manual tracking  | 77  |
| 2.2  | System<br>Dranged exerction for solar tracking   | 70  |
| 3.3  | Proposed operation for solar tracking  | 70  |
| 3.4  | Design detail of 211 diameter concentrating dish   | 79  |
| 3.5  | Variation of total wind force on the collector for   | 85  |
| 3.6  | variation of total wind force on the conector for<br>various collector orientations and wind velocities        | 83  |
| 27   | Mathematical definition of Paraboloid-Fresnel Design   | 86  |
| 3.8  | Concentrating dish segment division  | 90  |
| 3.0  | 3D design of centre block  | 91  |
| 3.10 | 3D design of dish supporting structure   | 92  |
| 3.10 | Design of nolv-frame for different dish segments   | 93  |
| 3.17 | Design of poly nume for uniform dish segments  | 93  |
| 3.12 | Design of reflecting surface   | 94  |
| 3.14 | Sub-assembly of solar concentrating dish – load  | 95  |
| 3.15 | supporting structure<br>Sub-assembly of solar concentrating dish – segment<br>assembly with reflecting mirrors | 95  |
| 3.16 | Assembly view of the solar concentrating dish design   | 96  |
| 3.17 | Typical Malaysia's annual variation of sun path diagram  | 97  |
| 3.18 | Solar tracking system – Integration between mechanism and control units  | 98  |
| 3.19 | Solar wind and rain sensor   | 99  |
| 3.20 | Design of azimuth angle control unit   | 101 |
| 3.21 | Working principle of the azimuth angle control unit  | 102 |
| 3.22 | Design of elevation angle control unit and dish  | 103 |
| 3 23 | Integration of two-axis solar tracking mechanism   | 104 |
| 3.24 | Alignment of the concentrator and solar sensor using a   | 105 |
| 3.25 | compass<br>Full accombly view of color concentrating dish  | 106 |
| 3.26 | Basic operation mode of solar tracking system based  | 106 |
| 2.0- | on solar time  |     |
| 3.27 | Conceptual design of solar concentrator focal region   | 107 |
| 3.28 | Design of solar thermal receiver   | 109 |
| 3.29 | Design of solar thermal absorber coil  | 110 |

,

| 3.30 | Design of secondary reflector model 1  | 111  |
|------|--|------|
| 3.31 | Design of secondary reflector model 2  | 112  |
| 3.32 | 2D sketch of a Beta Stirling engine with rhombic drive mechanism                                       | 113  |
| 3.33 | 3D design of identical set of Beta Stirling engine with rhombic drive mechanism                        | 115  |
| 3.34 | Power multiplication module design   | -116 |
| 3.35 | 3D illustration of square rhombic drive Stirling engine assembly                                       | 117  |
| 3.36 | Displacer and power cylinder design and assembly   | 118  |
| 3.37 | Regenerator material selection   | 119  |
| 3.38 | Complete design of square rhombic drive beta Stirling engine system                                    | 120  |
| 3.39 | Water cooling system operation   | 121  |
| 3.40 | Lubricating system operation   | 122  |
| 3.41 | Engine starting motor and power output drive mechanism   | 123  |
| 3.42 | Completed assembly of engine, receiver and power generator   | 124  |
| 3.43 | Full integration of dish-Stirling concentrating solar thermal system                                   | 125  |
| 3.44 | Dish-Stirling monitoring System  | 126  |
| 3.45 | Dish-Stirling monitoring sensors   | 126  |
| 3.46 | Thermocouple variation for different application   | 127  |
| 3.47 | DAO unit and calibration procedures  | 128  |
| 3.48 | Modelling of simplified 3D cone mirror arrays concentrator   | 129  |
| 3.49 | Solar flux meter   | 130  |
| 3.50 | Annual frequency distribution of wind speeds in<br>Mersing   | 131  |
| 3.51 | Daily mean wind speed for Subang Malaysia<br>throughout a typical year                                 | 131  |
| 3.52 | Weight distribution for solar concentrator with and without engine assembly                            | 133  |
| 3.53 | Engine efficiencies as a function of phase angle for various losses                                    | 136  |
| 4.1  | Intersection of $Y_a$ and $Y_b$ for the reflecting angle definitions                                   | 139  |
| 4.2  | Optimised reflecting angle for various layer of reflecting mirrors                                     | 140  |
| 4.3  | Corresponding mirror height, $Y_s$ referred to each layer reflecting angle                             | 140  |
| 4.4  | Comparison between Paraboloid-Fresnel and ideal parabolic dish   | 141  |
| 4.5  | DNI result from 8:00am to 6:00pm for measured days   | 142  |
| 4.6  | Modelling of paraboloid-Fresnel solar concentrators  | 143  |
| 4.7  | Solar flux input and reflection to focus plane   | 144  |
| 4.8  | Solar flux distribution on 2m height focus point range $200-1200$ W/m <sup>2</sup> (0° azimuth offset) | 145  |

| 4.9                  | Focal region shape and size variation in different azimuth offset angle ( $H_c=2000$ mm) | 146 |
|----------------------|--|-----|
| 1 10                 | Focal region area distribution for different azimuth                                     | 147 |
| 4.10                 | angle offset (referred to various focus height)  | 117 |
| 4 1 1                | Palationship between receiver assembly and focus   | 148 |
| 4.11                 | plane  | 140 |
| 1 12                 | Percentage of overlap between external receiver and                                      | 149 |
| 4.12                 | focal region for various focus height  |     |
| 1 13                 | Percentage of overlap between cavity receiver model 1                                    | 150 |
| <b>4.</b> 1 <i>J</i> | and focal region for various focus height  | 100 |
| A 1A                 | Percentage of overlap between cavity receiver model 2                                    | 150 |
| 4.14                 | and focal region for various focus height  |     |
| 4 15                 | Fabrication of centre block  | 152 |
| 4.15                 | Fabrication of dish supporting structure   | 152 |
| 4.17                 | Fabrication of poly-frame structure for segment A. B.                                    | 153 |
| 7.17                 | C and D  |     |
| 4 18                 | Completed poly-frame structure and reflecting mirrors                                    | 154 |
| 4.10                 | Assembly of 8m paraboloid-Fresnel concentrating dish                                     | 155 |
| 4 20                 | Elevation control mechanism  | 156 |
| 4 21                 | Azimuth control mechanism  | 156 |
| 4 22                 | Load supporting structures   | 156 |
| 4.22                 | Assembly of two-axis solar tracking system   | 157 |
| 4.23                 | Assembly of solar thermal receiver   | 158 |
| 4.25                 | Integration of external receiver   | 159 |
| 4.26                 | Integration of secondary reflector model 1   | 160 |
| 4 27                 | Integration of secondary reflector model 2   | 160 |
| 4 28                 | Stirling engine interior components  | 161 |
| 4.29                 | Stirling engine exterior engine blocks   | 162 |
| 4.30                 | Assembly of power cylinder and upper voke  | 163 |
| 4.31                 | Assembly of engine main moving components  | 163 |
| 4.32                 | Assembly of power multiplication module  | 164 |
| 4.33                 | Assembly of power cylinders, water jacket and  | 165 |
|                      | regenerator  |     |
| 4.34                 | Assembly of power cylinders, water jacket and  | 166 |
|                      | regenerator  |     |
| 4.35                 | Completion of multi cylinders square rhombic drive                                       | 167 |
|                      | beta engine  |     |
| 4.36                 | Installation of auxiliary components   | 168 |
| 4.37                 | Completed integration between engine, receiver and                                       | 169 |
|                      | absorber   |     |
| 4.38                 | Sub integration of dish-Stirling system  | 170 |
| 4.39                 | Integration of dish-Stirling system  | 171 |
| 4.40                 | Air flow computational simulation boundary condition                                     | 172 |
|                      | setting  |     |
| 4.4]                 | Wind load on 8m diameter ideal Paraboloid I vs wind                                      | 177 |
| 4                    | speed for 0-90° dish rotation  |     |
| 4.42                 | Wind load on 8m diameter ideal Paraboloid II vs wind                                     | 178 |
| 4 4 5                | speed for 0-90° dish rotation  |     |
| 4.43                 | Wind load on 8m diameter Paraboloid-Fresnel dish vs                                      | 179 |

|        | wind speed for 0-90° dish rotation   |     |
|--------|--|-----|
| 4.44   | Coefficient of drag $(C_D)$ vs dish rotating angle for                                     | 180 |
|        | different case study   |     |
| 4.45   | Structural load distribution of hydraulic system for                                       | 182 |
|        | zero wind load   |     |
| 4.46   | Structural load distribution on hydraulic cylinder for                                     | 182 |
|        | zero wind load   |     |
| 4.47   | Total load on hydraulic system vs dish rotating angle                                      | 184 |
| 4.48   | Total load on hydraulic cylinder vs dish rotating angle                                    | 185 |
| 4.49   | Static load analysis boundary condition setting  | 187 |
| 4.50   | Input load setting for static load analysis  | 188 |
| 4.51   | Von Mises stress distribution for dish structure (zero                                     | 189 |
|        | wind load without engine)  |     |
| 4.52   | Von Mises stress distribution for dish structure (zero                                     | 190 |
|        | wind load with engine)   |     |
| 4.53   | Critical component minimum Factor of safety  | 191 |
|        | comparison   |     |
| 4.54   | Factor of Safety for dish structure  | 192 |
| 4.55   | Structural failure on proposed dish-Stirling system  | 193 |
| 4.56   | Bearing failure validation   | 194 |
| 4.57   | Shaft failure due to overloading   | 195 |
| 4.58   | Structural displacement plot   | 195 |
| 4.59   | Development of second model  | 196 |
| 4.60   | Stress distribution plot for dish with engine system                                       | 197 |
|        | under maximum wind load condition  |     |
| 4.61   | FOS distribution plot for dish with engine system  | 198 |
|        | under maximum wind load condition  | 100 |
| 4.62   | Maximum stress distribution under different  | 199 |
|        | circumferences   | 200 |
| 4.63   | Maximum strain distribution under different  | 200 |
|        | circumferences   | 201 |
| 4.64   | Maximum displacement plot under different  | 201 |
|        | circumterences   | 001 |
| 4.65   | Minimum FOS plot under different circumferences  | 201 |
| 4.66   | Second model working prototype   | 202 |
| 4.67   | Temperature distribution for external receiver on 14                                       | 204 |
| 1 (9   | Oct 2011   | 205 |
| 4.68   | Temperature distribution for secondary reflector model                                     | 205 |
| 4.60   | I without lenses on 28 Oct 2011  | 206 |
| 4.09   | l emperature distribution for secondary reflector model                                    | 206 |
| 4 70   | 1 with lenses on 31 Oct 2011   | 200 |
| 4.70   | 2 cm 01 New 2011   | 208 |
| 4 71   | 2 ON UT NOV 2011   | 200 |
| 4 72   | Deficiency due to mirror defeats<br>Tomporature distribution for accordance affector model | 209 |
| •••• 4 | I emperature distribution for secondary reflector model                                    | 210 |
| 4.73   | In alter mirror luning on 10 Nov 2011<br>On site color variation from 10 and to 7mm        | 211 |
| 4.74   | On site solar variation from 10 am to /pm<br>Definition of single acting and double acting | 211 |
| 4.75   | Solar tracking system operation  | 212 |
|        | Solar tracking system operation  | 213 |

| 4.76 | Scopes of engine operational analysis                  | 214   |
|------|--|-------|
| 4.77 | Engine components reciprocating displacement plot      | 215   |
|      | for 44° phase angle                                    |       |
| 4.78 | Periodic volumetric displacement (cylinder 1) for      | 217   |
|      | proposed engine model                                  |       |
| 4.79 | Temperature result under condition A                   | 219   |
| 4.80 | Temperature result under condition B                   | 220   |
| 4.81 | Temperature result under condition C                   | 221   |
| 4.82 | Temperature result under condition D                   | 222   |
| 4.83 | Temperature result under condition E                   | 223   |
| 4.84 | Inertial constraint due to original setting            | 224   |
| 4.85 | Refined engine timing setting                          | 225   |
| 4.86 | Temperature result under condition F                   | 226   |
| 4.87 | P-V diagram for different phase angle setting          | 227   |
| 4.88 | Multi cylinders total effective volume variation for a | 228   |
|      | complete engine cycle                                  |       |
| 4.89 | Multi cylinders pressure distribution for a complete   | 229   |
|      | engine cycle   |       |
| 4.90 | Power output prediction under various engine speed     | 230   |
|      | calculation  |       |
| 4.91 | Power output variation under various engine speed      | 231   |
|      | calculation  |       |
| 4.92 | Hydraulic system voltage and current distribution      | 232   |
| 4.93 | Electric motor voltage and current distribution        | 233   |
| 4.94 | Two-axis control system voltage and current            | 234   |
|      | distribution   |       |
| 4.95 | Auxiliary system voltage and current distribution      | 235   |
| 4.96 | Hydraulic system and electric motor power              | 236   |
|      | consumption  | • • - |
| 4.97 | Overall system power consumption                       | 237   |
|      |  |       |

## LIST OF ABBREVIATIONS

# **Capital Letters**

| Aa               | Reflector area  |
|------------------|---|
| Ar               | Receiver area   |
| A <sub>w</sub>   | Cavity internal area of receiver  |
| A <sub>c</sub>   | Entrance aperture area of receiver  |
| BDC              | Bottom Dead Centre  |
| CSP              | Concentrating solar power   |
| CST              | Concentrating solar thermal   |
| C <sub>D</sub>   | Coefficient of drag   |
| C <sub>p</sub>   | Specific heat capacity at constant pressure                               |
| $C_{v}$          | Specific heat capacity at constant volume                                 |
| CR               | Geometric concentration ratio   |
| $CR_o$           | concentration ratio   |
| DNI              | Direct Normal Irradiation   |
| Ε                | Total emissive power  |
| E <sub>b</sub>   | Total emissive power of a blackbody                                       |
| F                | Force   |
| FOS              | Factor of safety  |
| $H_f$            | Focus height  |
| $H_d$            | Dish height   |
| Ia               | Reflector solar flux  |
| Ir               | Receiver solar flux   |
| $L_{0}$          | Distance between the Sun and the Earth = $1.496 \times 10^{11} \text{ m}$ |
| М                | Moment  |
| Mtoe             | Million Tonnes of Oil Equivalent  |
| Р                | Working gas pressure  |
| PLC              | Programmable logic control  |
| P <sub>min</sub> | Minimum working pressure  |
| P <sub>max</sub> | Maximum working pressure  |

| P <sub>mean</sub> | Mean working pressure                              |
|-------------------|--|
| PV                | Photovoltaic                                       |
| Q                 | Heat transfer                                      |
| $Q_H$             | Heat source or sink per unit volume                |
| $Q_s$             | Solar energy incident on the concentrating dish    |
| $Q_r$             | Radiant solar energy falling on the receiver       |
| $Q_l$             | Heat losses from the receiver to the surroundings  |
| $Q_u$             | Useful energy collected                            |
| $Q_{lo}$          | Optical loss from the collector                    |
| $Q_{lk}$          | Conductive heat loss from receiver                 |
| $Q_{lc}$          | Convective heat loss through the receiver aperture |
| $Q_{lr}$          | Radiative heat loss through the receiver aperture  |
|                   | the focusing device                                |
| R                 | Gas constant                                       |
| R <sub>sn</sub>   | Dish front radius for mirror in section n          |
| $R_{cn}$          | Dish centre radius for mirror in section n         |
| R <sub>en</sub>   | Dish end radius for mirror in section n            |
| S <sub>i</sub>    | Mass distributed external force per unit mass      |
| Т                 | Working gas temperature                            |
| TDC               | Top Dead Centre                                    |
| TW                | Terawatts  |
| TWh               | Terawatts hour                                     |
| $T_{min}$         | Working fluid minimum temperature                  |
| $T_{max}$         | Working fluid maximum temperature                  |
| $T_w$             | Average operating wall temperature in the cavity   |
| Ta                | Ambient temperature                                |
| V                 | Working gas volume                                 |
| W                 | Work done  |
| W <sub>c</sub>    | Compression work done                              |
| We                | Expansion work done                                |
| Wnet              | Net-work done                                      |

# Small Letters

| <i>d</i> <sub>r</sub> | Concentrating dish diameter                        |
|-----------------------|--|
| $d_f$                 | Focus area diameter                                |
| d <sub>sun</sub>      | Diameter of the Sun= $1.392 \times 10^9 \text{ m}$ |
| dearth                | Diameter of the Earth= $d_{sun}/10^9$              |
| h                     | Thermal enthalpy                                   |
| h <sub>c</sub>        | Convective heat transfer coefficient               |
| $l_n$                 | Reflected sun ray length                           |
| l <sub>m</sub>        | Faceted mirror length                              |
| m                     | Mass of working gas                                |
| п                     | Mirror section                                     |
| <i>p</i> <sub>f</sub> | Paraboloid focus point                             |
| $q_i$                 | Diffusive heat flux                                |
| $r_i$                 | Sun ray incoming vector                            |
| $r_t$                 | Sun ray refraction vector                          |
| rpm                   | revolution per minute                              |
| $r_v$                 | Compression ratio                                  |
| S                     | Entropy  |
| x                     | X-axis coordinate                                  |
| У                     | Y-axis coordinate                                  |
| Y <sub>s n</sub>      | Front height for mirror in section n               |
| y <sub>cn</sub>       | Centre height for mirror in section n              |
| Y <sub>en</sub>       | End height for mirror in section n                 |
| y' <sub>sn</sub>      | Front height for ideal parabolic in section n      |
| y'cn                  | Centre height for ideal parabolic in section n     |
| y' <sub>en</sub>      | End height for ideal parabolic in section n        |

# **Greek Symbols**

| α              | Absorptivity   |
|----------------|--|
| $\alpha_t$     | Thermal diffusivity  |
| γ              | Ratio of the energy intercepted by the receiver to the energy reflected by |
| 3              | Emissitivity   |
| ε <sub>c</sub> | Cavity surface emittance   |

| E <sub>eff</sub>          | Effective infrared emittance of cavity   |
|---------------------------|--|
| $\eta_t$                  | Thermal efficiency   |
| $\eta_{plant}$            | Plant efficiency   |
| $\eta_{col}$              | Solar collector efficiency   |
| $\eta_{ref}$              | Reflector efficiency   |
| $\eta_{eng}$              | Engine efficiency  |
| $\eta_o$                  | Optical efficiency   |
| n <sub>i</sub>            | Sun ray incoming ratio   |
| <i>n</i> <sub>t</sub>     | Sun ray refraction ratio   |
| θ                         | Solar incidence angle  |
| $\theta_n$                | Faceted mirror angle   |
| $	heta_i$                 | Sun ray incoming angle   |
| $\theta_r$                | Sun ray reflecting angle   |
| $\theta_t$                | Sun ray refraction angle   |
| $	heta_a$                 | Sun's radiation cone maximum half angle  |
| $	heta_{lpha}$            | Solar altitude angle   |
| $	heta_eta$               | Solar azimuth angle  |
| $	heta_\delta$            | X-axis angle   |
| $	heta_L$                 | Y-axis angle   |
| $\theta_{H}$              | Z-axis angle   |
| $	heta_{rim}$             | Half angle subtended by the arc of the parabola                                |
| k                         | Thermal diffusivity  |
| λ                         | Factor of un-shading   |
| σ                         | Stress   |
| $\sigma_{_{ m vonMises}}$ | Von misses stress  |
| $\sigma_{ m limit}$       | Maximum stress   |
| $\sigma_{S}$              | Stefan-Boltzmann constant, 5.67 x $10^{-8}$ W/(m <sup>2</sup> K <sup>4</sup> ) |
| ρ                         | Fluid density  |
| $ ho_r$                   | Reflectivity   |
| $ ho_{gas}$               | Working gas density  |
| τ                         | Transmissivity   |
| $	au_{ik}$                | Viscous shear stress tensor  |

| $	au_t$ | Temperature ratio |
|---------|-------------------|
| Ω       | Angular velocity. |

### **CHAPTER 1**

### INTRODUCTION

### 1.1 Background Study on Solar Power

Due to environmental issues as well as increasing demand for renewable resource, the conversion of solar power into useful energy is receiving more and more attention in recent years. Sunlight is the world's largest energy source. The amount that can be readily accessed with existing technology greatly exceeds the world's primary energy consumption. Furthermore, sunlight is free, clean, renewable and technically exploitable in most part of the inhabited earth (Angkee and Chana, 2011).

Taking the Sun as the spectrum of a blackbody at 5800K, the amount of solar energy falling on a surface per unit area and per unit time is illustrated in Figure 1.1. Currently, the Sun radiates energy at  $3.9 \times 10^{26}$ W or  $64 \times 10^{6}$ W/m<sup>2</sup> but energy received by the Earth and its atmosphere is 1368W/m<sup>2</sup> or  $1.7 \times 10^{17}$ W of radiation yearly from the sun. This value varies in +/-1.7% due to changes in the Earth-Sun distance (Salsabila, Ab Kadir and Suhaidi, 2011). Assuming that the world population is 10 billion with a total power need per person of 10kW would require about  $10^{11}$ kW of energy (Goswami, Frank and Jan, 2000). This is equal to 1000km x 1000km solar powered land area plotted in the middle of the Atlantic Ocean (Anton and Christian, 2009). Apparently, solar irradiance on only 1% of the earth's surface with 10% efficiency useful energy conversion could provide the needs of all the people on Earth (Goswami, Frank and Jan, 2000).



Figure 1.1 : Annual solar irradiance on Earth

#### Source : Anton and Christian (2009)

A tropical country such as Malaysia is generally hot all year-round and experiences its rainy season during the end of the year. Within an average of 12 hours of sunshine daily, the average solar energy received is between 1400 and 1900kWh/m<sup>2</sup> annually. The maximum radiation is received during a sunny day, where 90% of the extraterrestrial radiation becomes direct radiation while the rests are being deflected as diffuse radiation, while conversely, on a cloudy day, nearly all the solar radiation is diffused (Salsabila, Ab Kadir and Suhaidi, 2011). The weather condition in Malaysia is suitable for solar power implementation. This is because the weather condition is almost predictable and the availability of about 6h of direct sunlight with irradiation of between  $800W/m^2$  and  $1000W/m^2$  (Nowshad, Chin and Kamaruzzaman, 2009).

Today, two technologies are being actively developed to transform solar irradiation into electricity. One technology is photovoltaic or solar voltaic which uses photovoltaic materials to convert solar radiation directly into electricity. The other technology is solar thermal power or concentrating solar power converts the solar radiation into heat and then electricity through various thermodynamic cycles. For photovoltaic cells, efficiency up to 18% are reported while the efficiency of heat engine conversion systems can be as high as 33% depending on the quality of the technology used (Karabulut, Yucesu and Cinar, 2006). Restricted by the capital cost of solar panels

and other issues, the photovoltaic technology is being increasingly challenged by solar thermal power technology. In recent years, some practical solar thermal power plants have been installed in countries such as the US, Europe, India and China (Wu, Xiao, Cao and Li, 2010).

### 1.2 Problem Statement

Compared with the heavily subsidised fossil fuel, renewable energy such as solar power often labeled as expensive and will never be price-competitive. In addition, solar technology has been always stereotyped as not technically feasible for electricity generation due to the high cost. Although solar power has an enormous potential to reduce the global emissions of greenhouse gasses, the current use of this energy resource represents less than 1% of the total electricity production from renewable sources (Goswami, Frank and Jan, 2000). Particularly in Malaysia, the present initiatives and efforts are lower than the country's actual potential. Currently, the solar status in Malaysia is 1MW, but its estimated potential can reach more than 6500MW (Salsabila, Ab Kadir and Suhaidi, 2011). The limitation of technological development between technical potential and practical utilisation of solar energy becomes one of the reasons behind the minimum growth of solar-energy field.

The total solar energy reaching the earth is made up of two parts; energy from direct irradiation and energy from diffused irradiation. Although power-plants can use direct and diffuse solar energy, most of the man-made solar-electric conversion system can convert only direct energy efficiently (Goswami, Frank and Jan, 2000). With the solar concentration system, high intensity solar thermal engine operation is much more efficient than the diffuse solar technology.

In the recent development, one of the most viable technologies is the concentrating solar thermal (CST) which is able to convert solar electric for both distributed and remote area applications. However, each energy conversion has efficiency, cost and an environmental footprint depending on the worthiness of the process. From a scientific and technical viewpoint, the development of new technologies with higher conversion efficiencies and low production costs become the

key requirement for enabling the deployment of solar energy at a large scale (Goswami, Frank and Jan, 2000).

For the dish-Stirling CST technology as instance, it has good potential in power modulation and possess high concentration ratio. However, the solar-to-electric efficiency varies largely depending upon the solar flux density, concentration factor, the temperature of the thermal intermediary and the thermal cycle efficiency for the production of mechanical work and electricity. In order to maximise the solar fraction, intense search for effective and economic methods to capture, store and convert solar energy into useful energy should not be neglected (Mekhilef, Saidur and Safari, 2011).

In order to do that, one of the crucial steps is the introduction of specific solar thermal-electric energy conversion technology. In the case of dish-Stirling system, the technology development includes concentrator, receiver, absorber, thermodynamic cycle and tracking system. The technology must be further developed and proven to be technically and economically feasible with the consideration of environmental impact such as material degradation and climate constraints.

### 1.3 Objectives

Research objectives for the development of solar thermal energy conversion system are listed as follows:

- i. To prototype 8m diameter innovative solar thermal concentrating dish with twoaxis solar tracking system
- ii. To develop compact multi cylinders solar Stirling engine with thermal receiver unit for concentrated solar flux operation
- iii. To analyse the operation feasibility of integrated full scale solar dish-Stirling prototype model.

### 1.4 Work Scope

The work scope is specified as follows:

- i. Development of solar thermal concentrator based on combined paraboloid-Fresnel principle
- ii. Development of azimuth-elevation control unit, load supporting structures and direct normal irradiation tracking system
- iii. Development of a square rhombic drive Stirling engine incorporated with the solar-thermal receiver
- iv. Integration of working prototype dish-Stirling system
- v. Installation of data acquisition and monitoring sensors
- vi. Dish-Stirling working model operational analysis.

### 1.5 Hypothesis

Large concentrating dish development based on innovated paraboloid-Fresnel concept could minimise wind and rain load which indeed applicable for modular or distributed tropical application. Consistent solar tracking system could be developed using PLC principle and accumulation of high intensity solar direct normal irradiation. Consequently, it could increase the temperature of thermal flux in the specific receiver-absorber to drive the four-cylinder square type rhombic drive beta Stirling engine. For the solar power conversion, solar thermal is an alternate solution instead of the photochemical process.